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CORONA J

PERFORMANCE EVALUATION REPORT

MISSION 1010-1 and 1010-2

FTV 1178; J-11

28 May 1965

Approved: [REDACTED]

Mgr.

Advanced Projects

Approved: [REDACTED]

Mgr.

Program [REDACTED]

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FOREWORD

This report details the performance of the payload system during the operational phase of the Program [REDACTED] Flight Test Vehicle 1178.

Lockheed Missiles and Space Company has the responsibility for evaluating payload performance under the Systems Integration and "J" System contracts.

This document is the final payload test and performance evaluation report for Missions 1010-1 and 1010-2 which was launched on 14 September 1964.

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INTRODUCTION

This report presents the final performance evaluation of Missions 1010-1 and 1010-2 of the Corona Program. The purpose of this report is to define the performance characteristics of the J-1 payload system, to identify the source of in-flight anomalies and recommend the appropriate corrective action.

The performance evaluation was jointly conducted by representatives of Lockheed Missiles and Space Company (LMSC) and ITEK at the facilities of NPIC and AFSPPL. The off-line evaluation using Corona engineering photography acquired over the United States was performed at the individual contractors plants.

The quantitative data used for this report is obtained from government organizations. The diffuse density data, visual RES values and MTF/AIM resolution are produced by AFSPPL. The vehicle attitude error values, frame correlation times are made at NPIC who also supply the Processing Summary and MTF/AIM resolution reports published by

Computer programs developed by A/P are utilized to calculate and plot the frequency distribution of the various contributors to image smear to permit analysis and correlation of the conditions of photography to the information content and quality of the acquired pictures. Computer analysis of the exposure, processing and illumination data provides the necessary data to analyze the exposure criteria selected for the mission.

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SECTION 1

SYSTEM PERFORMANCE

A. MISSION OBJECTIVES

The payload section of Mission 1010, placed into orbit by Flight Test Vehicle #1178 and SLV-2A booster #405, consisted of two panoramic cameras, two Stellar-Index cameras, two Mark 5A recovery capsules and a space structure to enclose the cameras and provide mounting surfaces for all equipments. Figure 1-1 presents an inboard profile of the J-11 payload system. This Corona "J" system is designed to acquire search and reconnaissance photography of selected areas of the earth from orbital altitudes. The planned mission was two, four day photographic periods separated by a seven day inactive period.

B. MISSION DESCRIPTION

The payload was launched from Vandenberg Air Force Base (VAFB) at 2253:43 Z (3:53:43 PDT) on 14 September 1964. Ascent and injection were normal and the achieved orbit within nominal tolerances. Tracking and command support was effected by the Air Force Satellite Control Facility consisting of tracking and command stations at [REDACTED] under central control of the Satellite Test Center at Sunnyvale, California. Mission 1010-1 consisted of four days operation and was completed by air recovery on 18 September 1964. Mission 1010-2 was completed with an air recovery on 23 September 1964 following five days of photographic operations. Mission 1010 was the first nine day Corona operation.

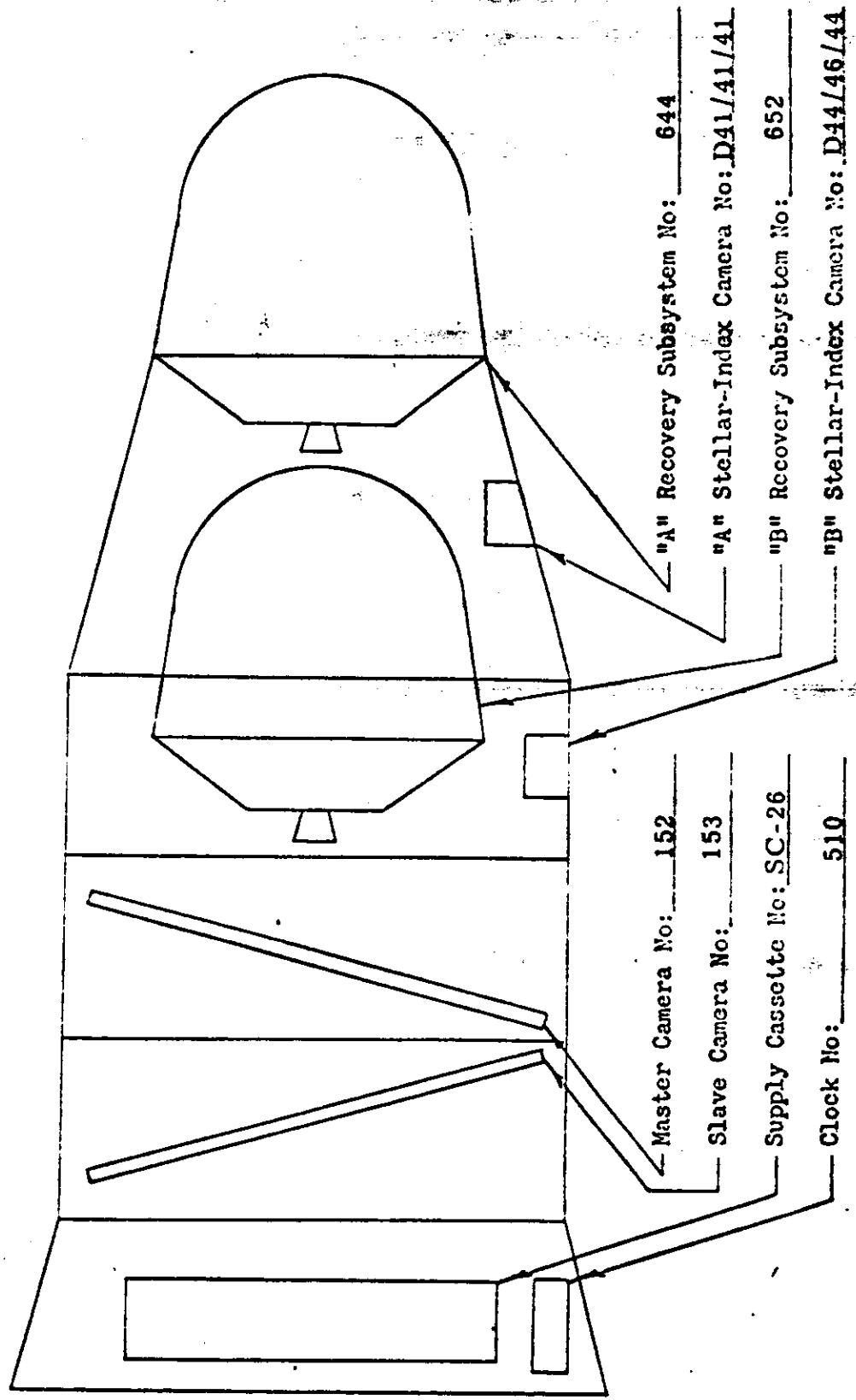
The comparison of the planned and actual orbit parameters is tabulated as follows:

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SCHEMATIC PRESSURE PROFILE - CORONA J SYSTEM

MISSION 1010



Yaw Programmer No: N/A

FIGURE 1-1

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ORBIT PARAMETERS

<u>Parameter</u>	<u>Predicted</u>	<u>Orbit 1 Actuals</u>
Period (Min.)	91.06	90.97
Perigee (N. M.)	99.98	97.45
Apogee (N. M.)	206.29	259.19
Inclination (Deg.)	84.99	84.96
Perigee Latitude (Deg. N.)	39.99	42.58
Eccentricity	0.02221	0.02236

The achieved orbit was within the 3 sigma dispersions from nominal. The Agena vehicle was not deactivated after the completion of Mission 1010-2. VHF command exercises were conducted until the vehicle power was depleted. All contact was lost by orbit 166.

C. PANORAMIC CAMERAS

The Master and Slave panoramic cameras operated throughout both missions with no significant problems and produced excellent photographic coverage. The cloud cover and atmospheric haze observed in the photography was high. A small area on the Master camera formats of Mission 1010-1 contained a small soft focus area which was not present during Mission 1010-2.

D. STELLAR-INDEX CAMERAS

The Stellar-Index cameras operated properly through both missions. Double star images were observed intermittently during both missions. This anomaly has been traced to the unbalance of the panoramic cameras during non-synchronous operation. The unbalance imparts a small roll motion to the satellite.

E. OTHER SUB-SYSTEMS

The clock, instrumentation, pressure make-up, command and thermal control sub-systems performed satisfactorily through both missions.

F. CONCLUSIONS

Mission 1010-1 and 1010-2 achieved the objective of acquiring high quality search and reconnaissance photography from orbital altitudes.

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G. RECOMMENDATIONS

The evaluation and analysis of the data produced by both missions has resulted in the following recommendations:

1. Continue the analysis of the cause of soft focus areas in the panoramic photography.
2. Utilize the higher level exposure criteria on future Corona missions.

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SECTION 2

PRE-FLIGHT SYSTEMS TESTS

A. ENVIRONMENTAL TESTING

1. Test Objective

As a standard procedure, the J payload systems are subjected to thermal/altitude environmental testing which simulates orbital environment. One of the purposes of this test is to demonstrate the system susceptibility to corona discharge. Such discharge fogs the film thus degrading the operational photography.

2. Test Summary

The J-11 payload system was tested for pressure, thermal and corona discharge effects in the TASC chamber starting May 20, 1964. The test consisted of three days active operation with the "A" bucket; one day of de-active soak and three days of active operation with the "B" bucket. The J-11 system contained the first flight type pressure make-up system and corona markings were reported to be acceptable for flight.

Several abnormalities in system performance were evident during the test. Component replacement after the completion of the environmental test corrected all observed problems.

3. Thermal Environment

The TASC chamber thermal environment was programmed to simulate the on-orbital temperature conditions that the J-11 payload system would experience in flight. Typical instrument temperatures recorded through the test are as follows:

<u>Orbit</u>	<u>Master Camera</u>	<u>Slave Camera</u>
6	78°	81°
17	83°	86°
33	84°	87°
48	82°	87°
59	67°	67°
69	61°	62°
79	51°	52°

Two self-heating tests were conducted during the soak period. One test was deemed invalid due to a change in the steady state temperature in the chamber, but the other test was valid and the results are included in Figure 2-1.

4. Pressure Environment

The pressure environment of the instruments was less than 0.5 micron in a non-operating condition. The pressure would increase to a nominal 1 micron during operation when the pressure make-up system was not used. The pressure make-up system would cause the pressure to increase to a nominal 40 microns during an operate. The pressure make-up system was active only during the "B" mode operations.

5. Panoramic Camera Performance

Evaluation of the test film showed that both the Master and Slave cameras produced intermittent start-up corona discharge. The resulting fogging was well within the acceptance criteria hence the J-11 system was recommended for flight.

The panoramic cameras operated normally during the test phase with the exception that the cycle rate errors were excessive. Component replacement and adjustment corrected this anomaly.

6. Stellar-Index Camera Performance

The Stellar-Index Cameras installed in the J-11 system during

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the environmental test were replaced prior to flight. The flight cameras were environmentally tested as components and found acceptable for flight.

B. RESOLUTION TEST

The dynamic resolution test of the J-11 payload system was performed at the A/P facility on 5 June 1964. Each panoramic camera photographed high and low contrast resolution targets. The resulting through focus resolution data is shown in Figure 2-2 for the Master camera and in Figure 2-3 for the Slave camera.

C. LIGHT LEAK TEST

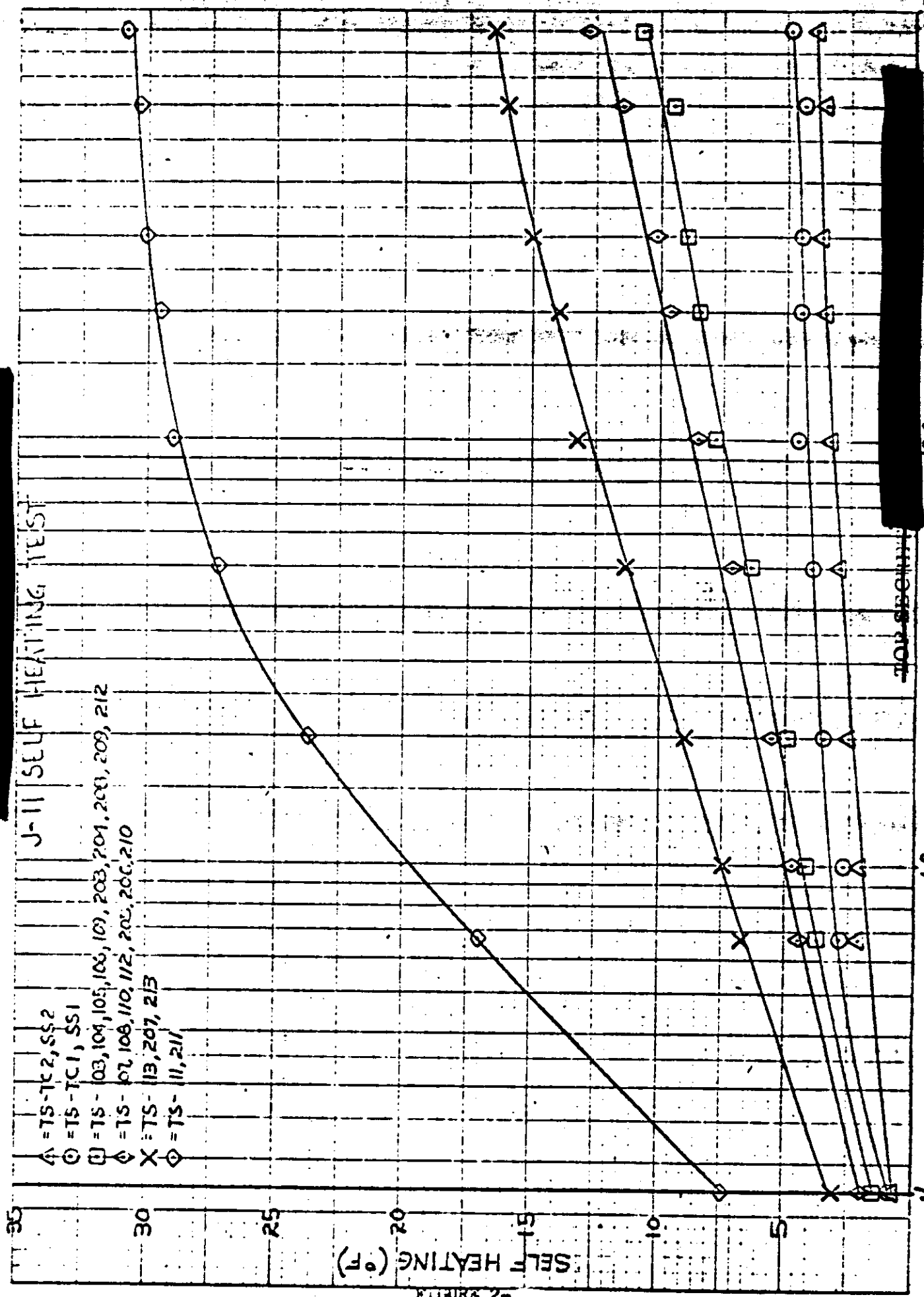
The examination of the film threaded in the J-11 system during the light leak test determined that no film fogging was present. The light tight integrity of the system was considered acceptable for flight.

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J-II SELF HEATING TEST

- △ = TS-TC2, SS2
- = TS-TC1, SS1
- = TS-103, 104, 105, 106, 107, 203, 204, 208, 209, 212
- ◇ = TS-102, 108, 110, 112, 205, 206, 210
- X = TS-113, 207, 213
- ◇ = TS-11, 211



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TIME FROM TURN ON (MIN)

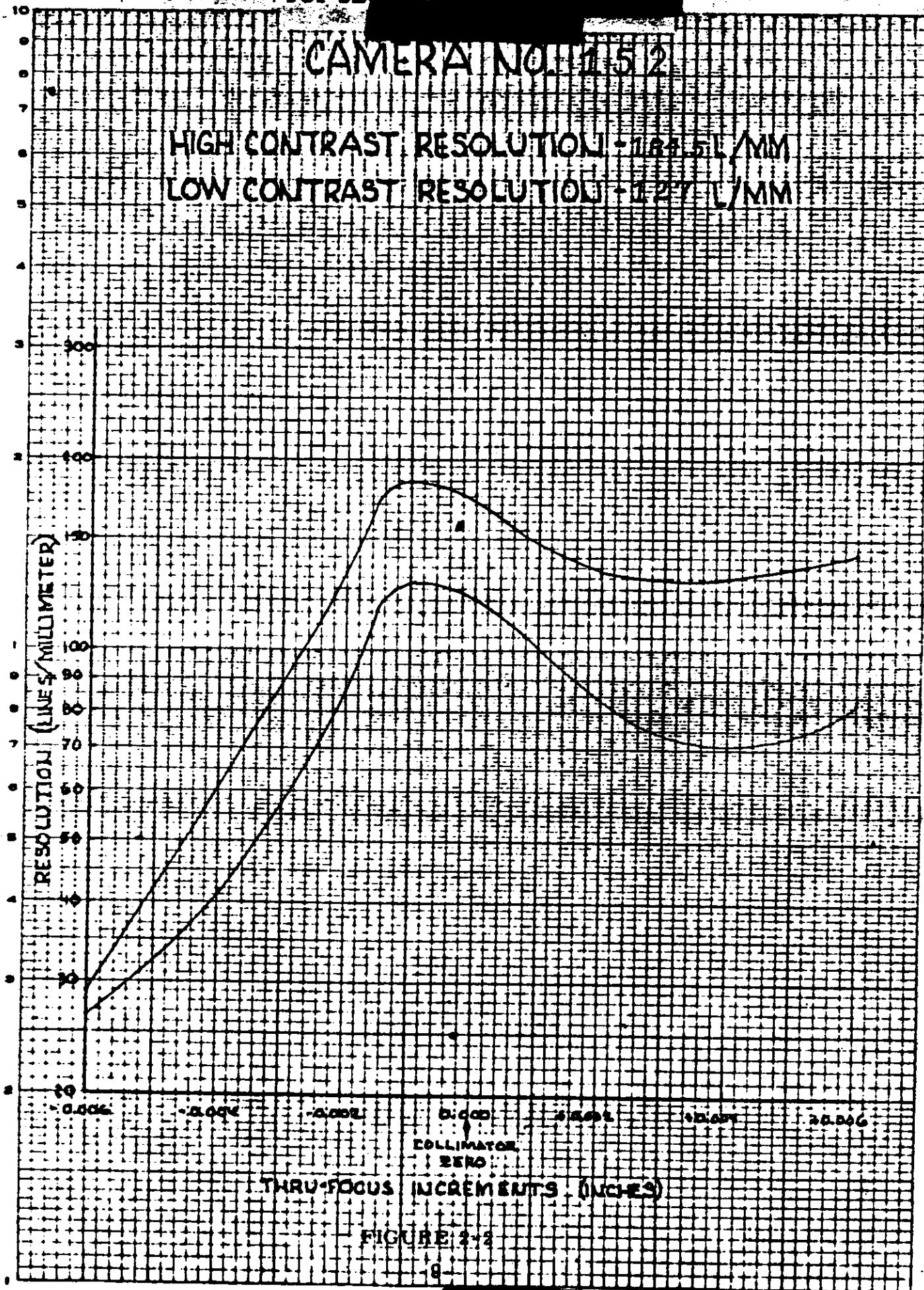
FIGURE 2-

CAMERA NO. 152

HIGH CONTRAST RESOLUTION - 118.5 L/MM
LOW CONTRAST RESOLUTION - 127 L/MM

EUGENE DIETZGEN CO.
MADE IN U.S.A.

NO. 340R L210 DIETZGEN GRAPH PAPER
SEMI-LOGARITHMIC
2 CYCLES X 10 DIVISIONS PER INCH



COLLIMATOR
ZERO

THRU-FOCUS INCREMENTS (INCHES)

FIGURE 2-2

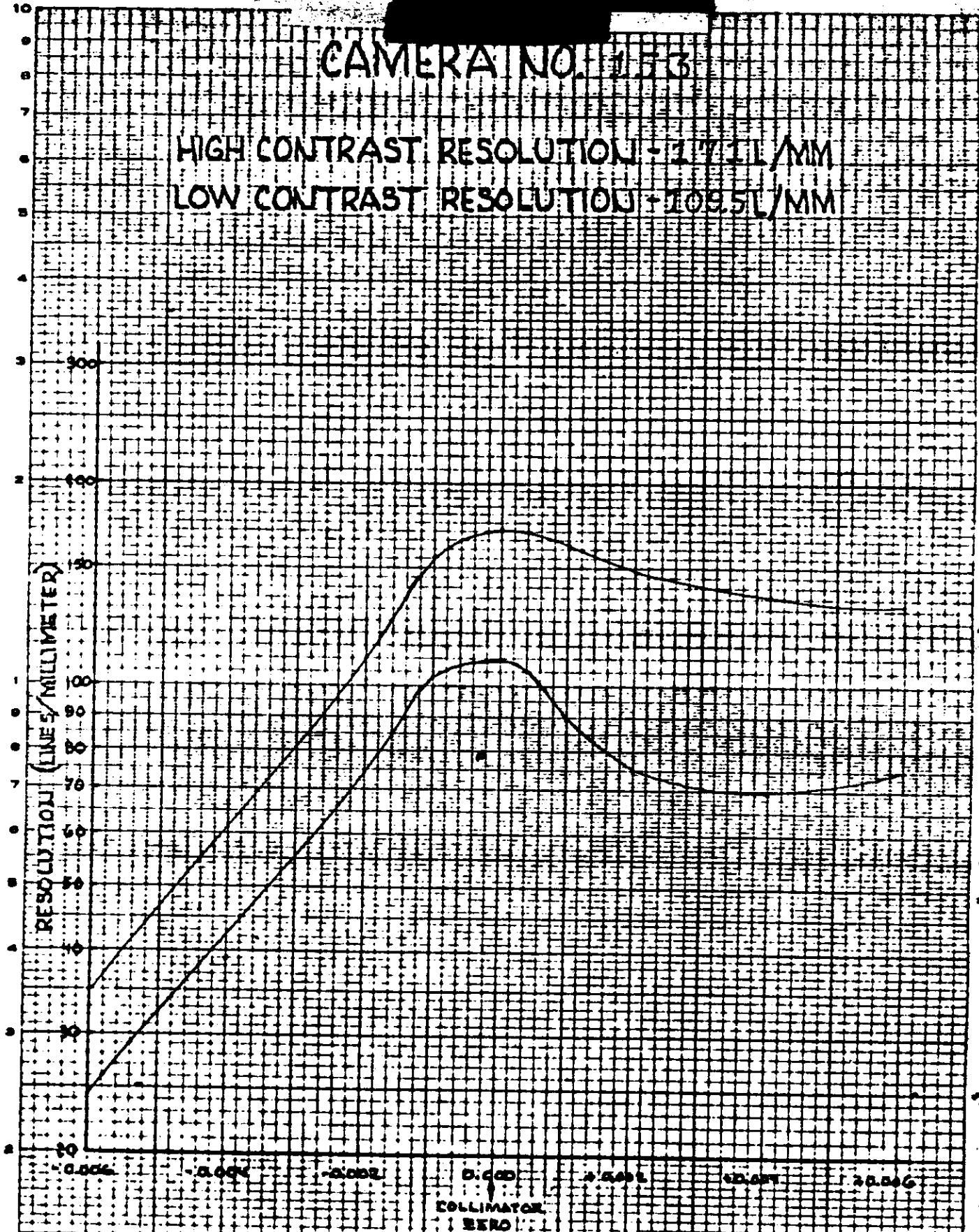
CAMERA NO. 153

HIGH CONTRAST RESOLUTION - 117.11/MM

LOW CONTRAST RESOLUTION - 109.51/MM

SUNEME DIEZON CO.
MADE IN U.S.A.

NO 340R L210 DIETZON GRAPHIC PAPER
SEMI-LOGARITHMIC
2 CYCLES X 10 DIVISIONS PER INCH



THRU-FOCUS INCREMENTS (INCHES)

FIGURE 2-3

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SECTION 3

FLIGHT OPERATIONS

A. COMMAND & INSTRUMENTATION PERFORMANCE

No commanding problems of serious consequence were encountered during the mission. There was one instance in which an H-timer reset deleted a V/H programmer start delay step. This deletion caused the V/H programmer to start late. The reset deletion occurred during the orbit 9 acquisition. The orbit 1 tracking station data was bad, and due to communications problems during orbits 5 and 6 the tracking station was unable to provide tracking data.

Acquisitions during orbit 8 resulted in revisions in the ephemeris predictions. The earlier STC computer predictions for the ephemeris were heavily weighted with poor orbit 1 data and nominal orbital predictions. The revised orbital predictions necessitated a 35-second reset during the orbit 9 acquisition. During the 35-second reset two functions were missed: A V/H programmer delay step and a clock interrogate. The deletion of the delay step caused the V/H programmer to start a maximum of 50 seconds late. This late start was not deleterious to system performance during orbit 9. The IMC error introduced by the late programmer start was less than .5%.

B. PANORAMIC CAMERA PERFORMANCE

Telemetry data, acquired during the engineering operations over indicated nominal panoramic camera operations.

Three flight ramps were used: 8-3, 8-2, and 7-2. The nominal flight plan called for the 8-3 ramp for launch. In orbit 6 the flight ramp was changed from 8-3 to 8-2. In orbit 71 the flight ramp was changed from 8-2 to 7-2. The changes in the V/H ramp settings were made to allow the V/H programmer to better match the vehicle orbit. Camera cycle rate performance is summarized as follows:

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DEVIATIONS BETWEEN PREDICTED AND ACTUAL
PANORAMIC INSTRUMENT CYCLE RATES

<u>ORBIT NUMBER</u>	<u>RAMP</u>	<u>TIME UP RAMP</u>	<u>PERCENTAGE ERROR</u>	
			<u>MASTER</u>	<u>SLAVE</u>
9 (Night)	8-2	445 Secs.	- 1.6	- 2.0
31 (Day)	8-2	2130 Secs.	- 0.7	- 1.6
47 (Day)	8-2	2160 Secs.	- 0.4	- 2.0
56 (Night)	8-2	645 Secs.	- 0.5	- 2.0
71 (Night)	8-2	705 Secs.	- 0.7	- 2.2
103 (Night)	7-2	785 Secs.	- 0.3	- 2.4

Approximately 6080 frames were exposed by the master and slave cameras during the nine-day mission.

C. STELLAR/INDEX CAMERA PERFORMANCE

The T/M data from the engineering operations over [redacted] indicated satisfactory performances from the two S/I units. Daytime and nighttime acquisitions were included in these engineering operations. All S/I metering and shutter pulses appeared to be normal.

D. PRESSURE MAKE-UP SYSTEM PERFORMANCE

Pressure make-up system (PMU) performance was monitored by two functions: a pressure monitor that showed the pressure in the nitrogen supply bottle; and a pirani gage that measured the pressure in the vicinity of the panoramic instruments. The PMU system was commanded ON and OFF by camera ON/OFF commands. This was the second PMU system employed in the Corona J reconnaissance program.

The pirani gage T/M data from the engineering operations are presented in Figures 3-1 through 3-3. The nitrogen supply pressure is shown in Figure 3-4. These data indicate satisfactory PMU system performance.

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E. CLOCK PERFORMANCE

The performance of the clock was satisfactory for the 9-day mission. Table 3-1 presents the clock/systems time correlation data.

F. THERMAL ENVIRONMENT SUMMARY

All thermal data from the [REDACTED] acquisitions are presented in Tables 3-2 and 3-3. The panoramic cameras, supply spools, and thrust cone temperatures were corrected for self-heating. The self-heating characteristics for the aforementioned sensors were determined from the results of a special temp sensor self-heating test conducted in the TASC chamber.

Table 3-4 presents these calibration data. The predicted and in-flight temperatures for Mission 1010-1 are compared in Figures 3-5 through 3-7.

G. RECOVERY SYSTEM PERFORMANCE

A. Mission 1010-1 Recovery

The Mission 1010-1 recovery capsule was retrieved with a successful air catch on orbit 65. The physical condition of the capsule and the recovery sequence indicated the recovery events were normal in all aspects.

B. Mission 1010-2 Recovery

The Mission 1010-2 recovery capsule was retrieved with a successful air catch on orbit 144. The recovery events were normal in all aspects.

No deactivation period was initiated after the Mission 1010-2 recovery. VHF command exercises were conducted until the vehicle power was depleted. All contact was lost by orbit 166. All A/P tape events were utilized by orbit 144.

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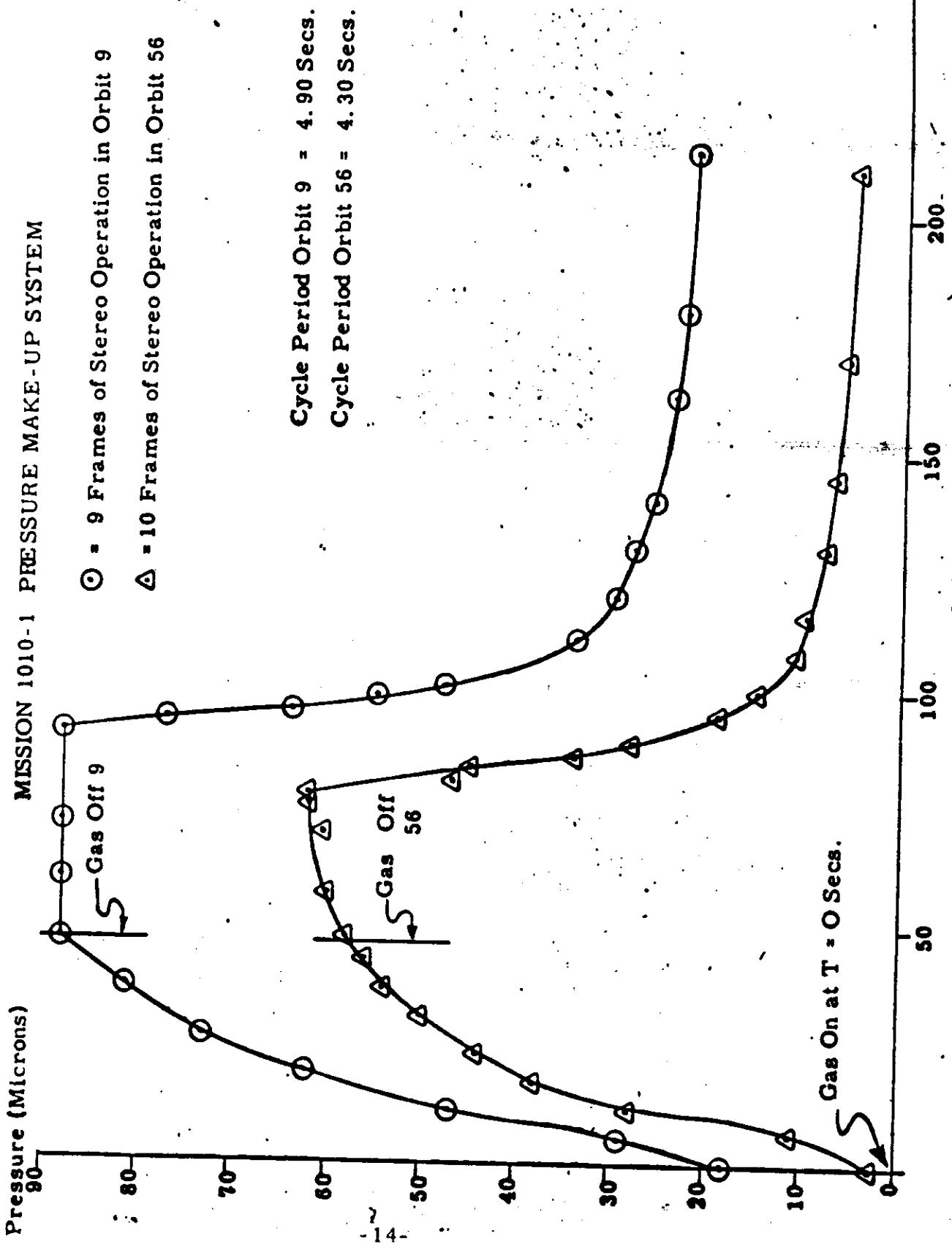
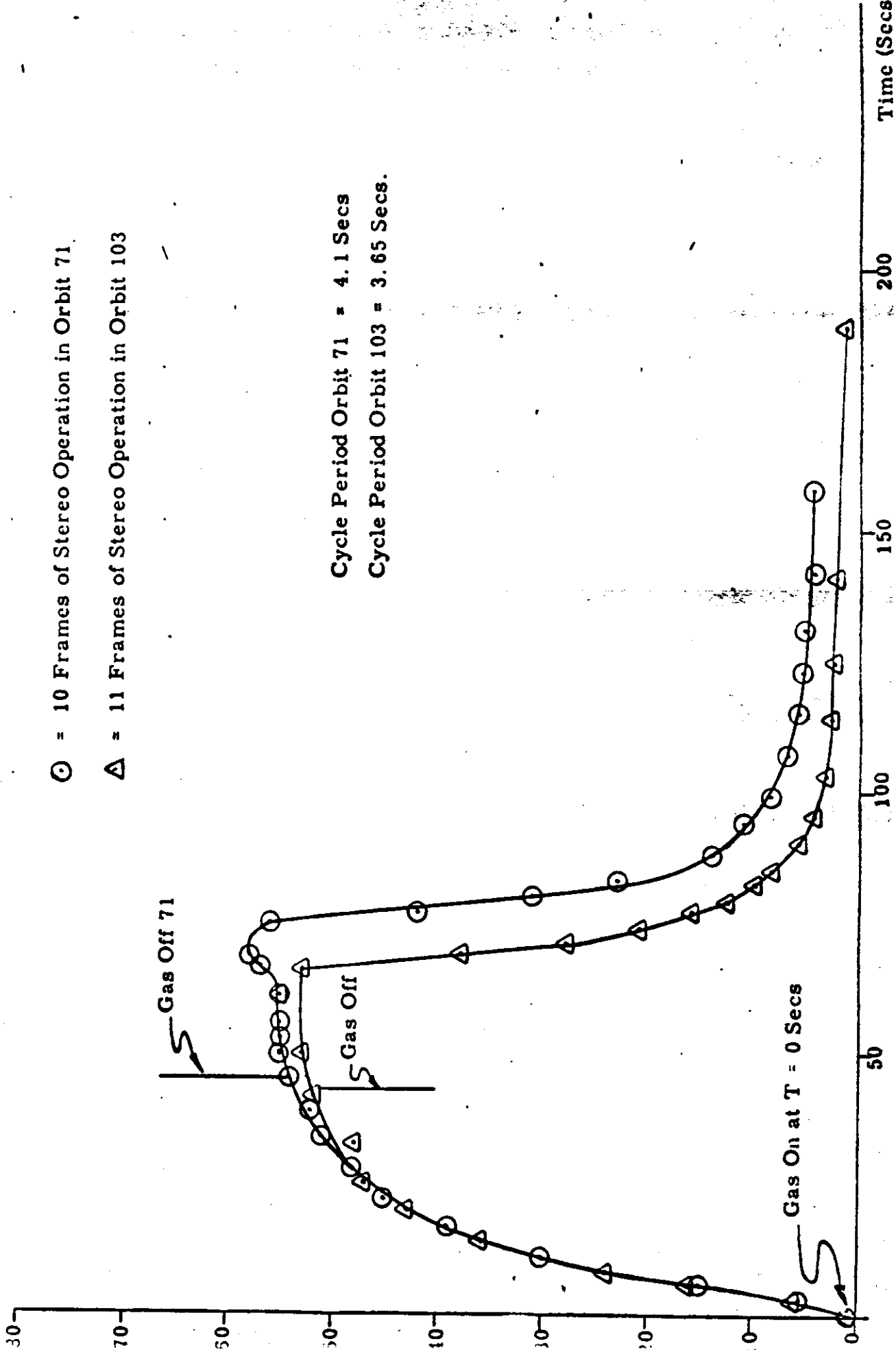


FIGURE 3-1

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MISSION 1010-2 PRESSURE MAKE-UP SYSTEM

Pressure (Microns)



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MISSION 1010 PRESSURE SUMMARY

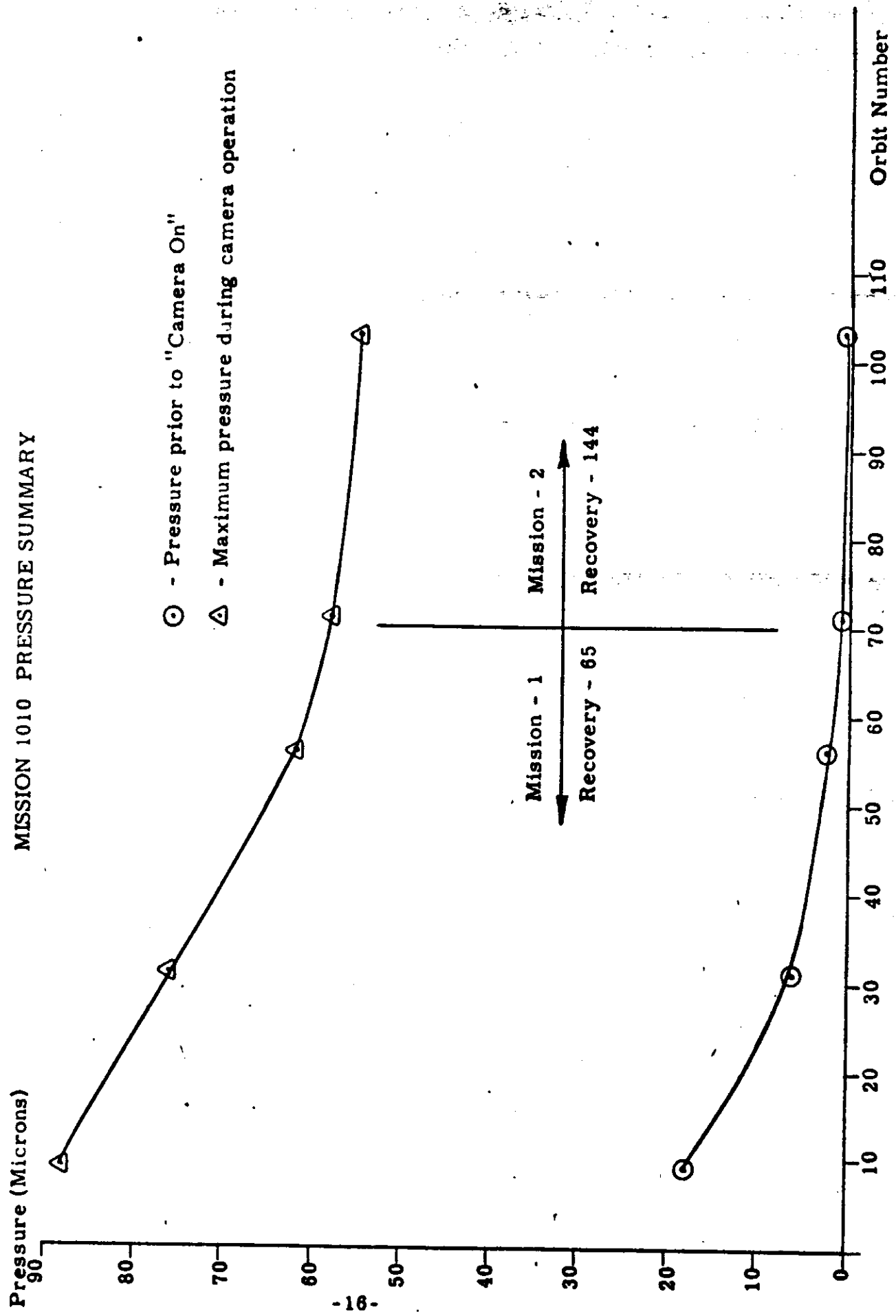


FIGURE 3-3

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MISSION 1010 NITROGEN SUPPLY PRESSURE

N₂ Pressure PSIG

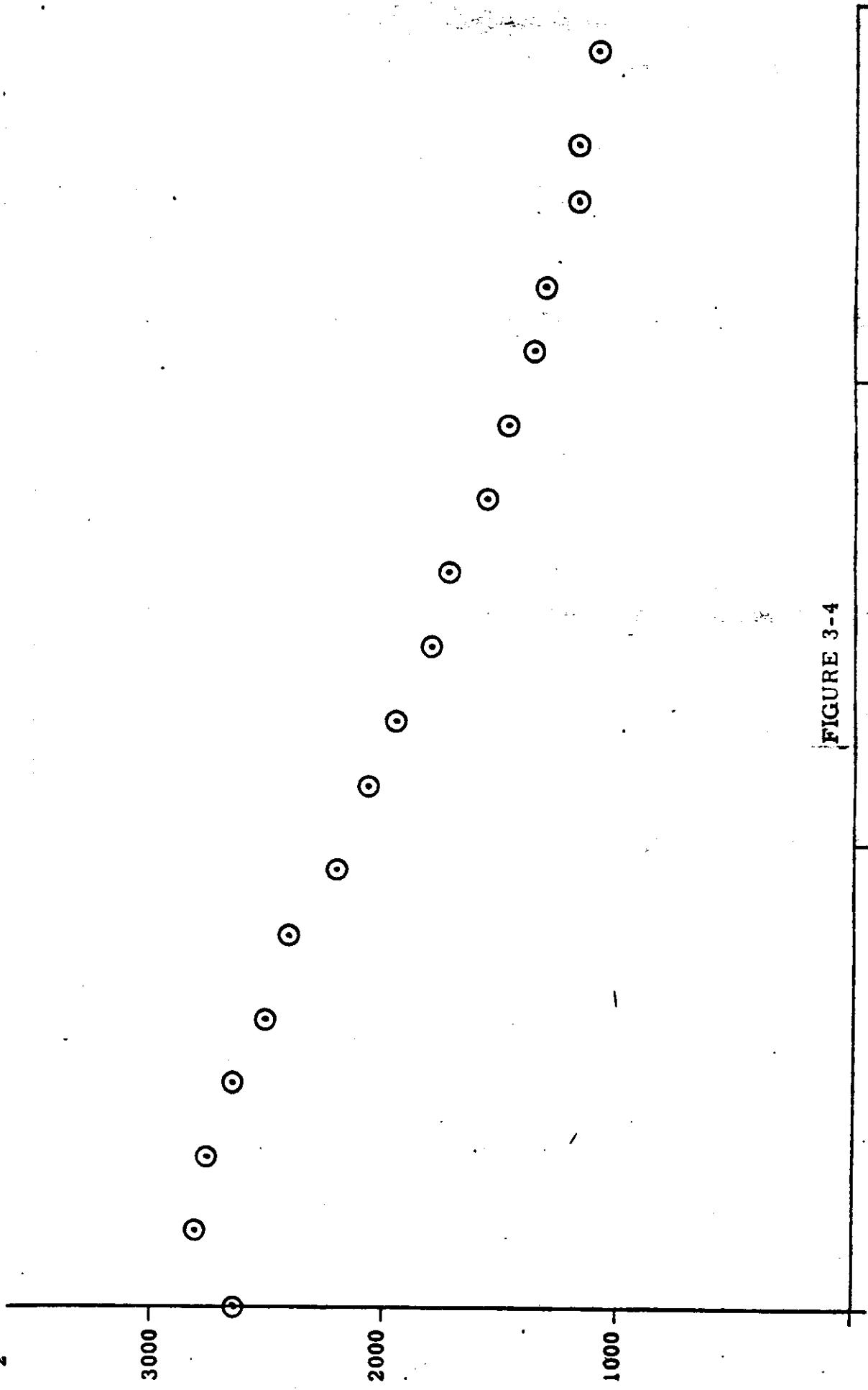


FIGURE 3-4

50

100

140

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Orbit Number

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MISSION 1010-1 TEMPERATURES - PREDICTED AND ACTUAL

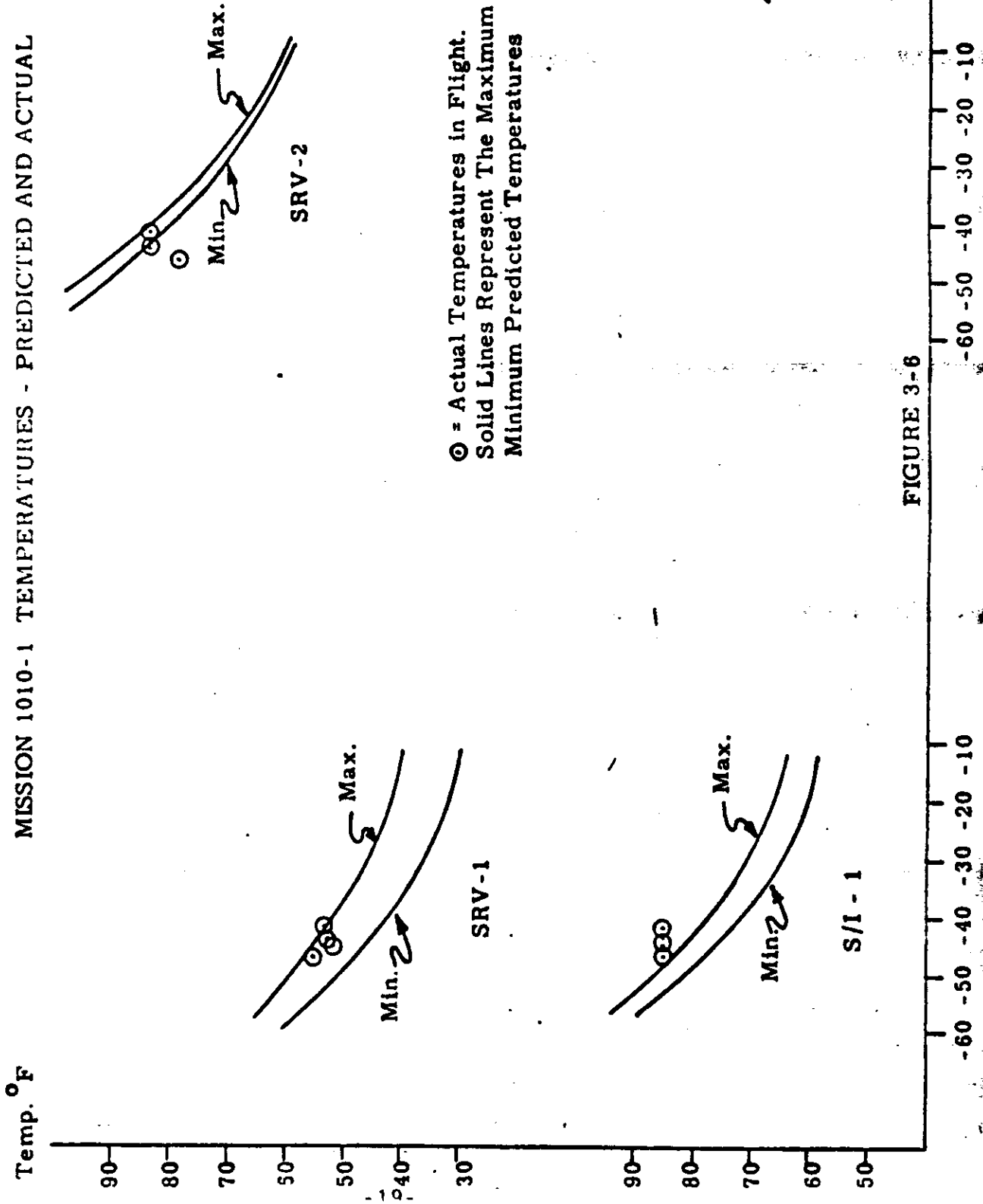
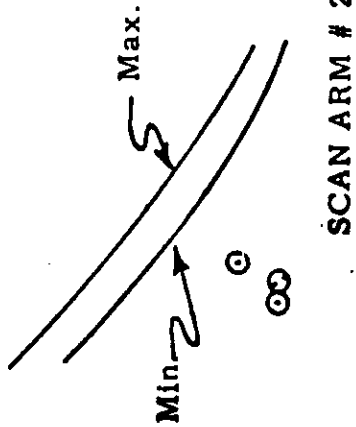
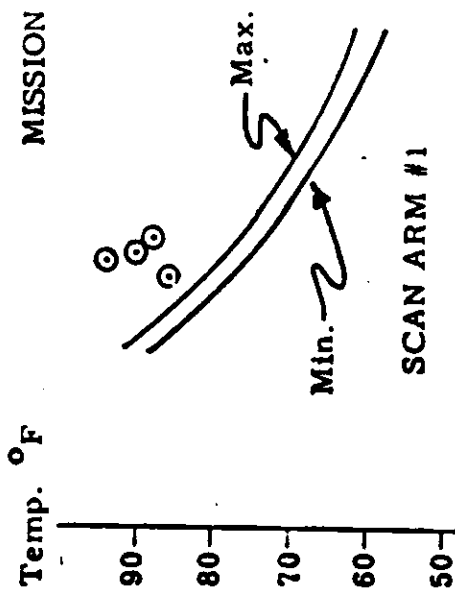


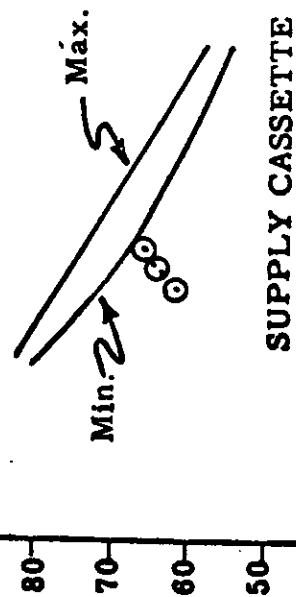
FIGURE 3-6

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MISSION 1010-2 TEMPERATURES - PREDICTED AND ACTUAL



⊙ = Actual Temperatures in Flight.
Solid Lines Represent the Maximum and Minimum Predicted Temperatures



Orbit	Temperature
8	-47
24	-45
40	-44
56	-42

FIGURE 3-7

TABLE 3-1

J-11 CLOCK/SYSTEM TIME CORRELATION

<u>ORBIT</u>	<u>SYSTEM TIME RAW DATA</u>	<u>CLOCK TIME</u>	<u>SMOOTHED SYSTEM TIME</u>	<u>DELTA DIFFERENCE</u>
<u>MISSION 1</u>				
1	1350.885	207900.436	1350.895	.010 +
8	38009.975	244559.533	38009.983	.008 +
9	43827.135	250376.691	43827.139	.004 +
16	83682.870	290232.430	83682.868	.002 -
24	39183.430	332133.002	39183.430	.000
31	79059.551	372009.132	79059.550	.001 -
40	40256.317	419605.907	40256.313	.004 -
47	79901.820	459251.416	79901.812	.008 -
56	41024.535	506774.146	41024.531	.004 -
63	80804.910	9683.618	80804.905	.005 -
<u>MISSION 2</u>				
71	36047.032	51325.748	36047.025	.007 -
79	81666.305	96945.037	81666.302	.003 -
87	36833.560	138512.302	36833.557	.003 -
95	82471.728	184150.486	82471.730	.002 +
103	38027.710	226106.472	38027.705	.005 -
110	77807.472	265886.248	77807.472	.000
119	38865.991	313344.785	38865.997	.006 +
126	78273.005	352751.807	78273.009	.004 +
135	39496.435	400375.253	39496.443	.008 +

Smoothed System Time = -206549.490 + .999999752917070 x Clock Time

Delta Difference = Smoothed System Time - Raw System Time

TABLE 3-2

J-11 TEMPERATURE SUMMARY

<u>SENSOR</u>	<u>ORBITS ACQUIRED</u>																		
<u>Master Camera</u>	0	9	16	24	31	40	47	56	63	71	79	87	95	103	110	119	126	135	
3	66	60	57	63	56	59	54	62	52	53	68	50	67	67	67	69	65	58	
4	72	69	66	72	65	68	64	72	61	62	56	59	53	56	56	58	52	56	
5	68	75	70	77	69	74	67	76	67	68	61	66	60	63	60	64	58	62	
6	65	85	80	85	80	82	78	85	74	77	71	74	67	70	67	71	66	68	
7	66	78	73	78	73	74	72	79	69	69	65	67	64	63	64	64	62	62	
8	71	76	71	77	71	73	68	78	66	67	60	64	59	62	59	62	58	60	
9	69	84	78	84	77	79	63	82	72	75	68	72	65	70	66	70	64	66	
10	66	71	70	71	67	66	65	72	63	59	59	59	58	54	58	57	56	54	
11	100	86	91	94	86	90	83	88	86	75	79	80	78	69	62	75	73	77	
12	73	65	60	67	60	63	58	68	57	57	51	55	50	53	51	53	49	52	
13	68	80	78	82	76	76	73	81	73	67	67	63	65	60	59	61	62	58	
AVG.	68	74	70	76	69	71	66	77	65	65	61	63	59	60	59	61	57	60	
<u>Slave Camera</u>																			
3	62	80	77	81	76	78	73	81	72	74	70	73	68	69	66	69	64	66	
4	63	74	69	77	70	74	66	77	66	71	64	69	62	67	61	67	59	63	
5	64	71	67	73	66	69	66	76	64	67	62	65	60	61	58	62	58	60	
6	60	66	61	66	63	64	62	68	58	60	56	58	54	54	54	55	53	53	
7	62	69	66	71	56	66	63	71	63	61	60	59	58	55	58	57	56	54	
8	64	70	63	71	64	69	62	72	62	66	59	63	57	61	56	62	56	59	
9	67	63	58	65	57	62	57	66	57	59	55	57	52	54	52	56	51	54	
10	65	70	68	71	68	65	64	71	64	62	61	59	59	56	59	58	56	55	
11	94	63	57	63	60	62	60	68	58	62	56	58	57	60	65	60	56	55	
12	66	75	69	77	69	73	68	78	65	69	64	68	62	65	60	65	60	62	
13	67	72	69	74	70	69	68	74	68	66	66	63	63	62	68	63	62	59	
AVG.	64	70	67	73	66	68	65	73	63	65	61	63	59	60	59	61	57	58	
<u>Supply Spools</u>																			
1	60	58	57	61	61	62	61	64	59	61	58	58	56	56	56	57	56	55	
2	60	66	63	67	64	68	64	68	63	65	62	64	59	63	58	62	58	59	

Notes: All data corrected for self-heating except injection.
Camera averages do not include sensor #11.

TABLE 3-3

J-11 TEMPERATURE SUMMARY

<u>SENSOR</u>	<u>ORBITS ACQUIRED</u>																		
<u>Fairing ("A")</u>	0	9	16	24	31	40	47	56	63	71	79	87	95	103	110	119	126	134	
<u>Barrel #1 ("B")</u>	OBH	48	76	51	70	48	67	51	70	4	78	1	14	1	14	1	7	1	
1	OBH	18	15	21	15	18	12	18	12	3	-4	-1	-7	-1	-4	-1	-7	-	
2	OBH	2	15	5	15	2	12	5	12	19	58	19	61	19	64	16	35	1	
3	OBH	83	88	88	86	83	86	86	83	67	122	67	122	63	119	60	97	6	
4	OBH	120	153	126	142	120	139	120	134	62	98	65	92	62	86	58	83	5	
5	OBH	91	154	94	143	88	138	91	135	-	-	-	-	-	-	-	-	-	
6																			
<u>Barrel #2</u>	163	67	111	67	106	64	103	64	100	58	97	61	92	54	86	54	83	5	
1	158	62	139	65	131	62	126	62	126	62	120	62	120	55	118	55	95	5	
2	186	22	66	22	60	19	57	22	60	22	57	22	63	19	63	19	38	1	
3	194	4	4	7	4	7	0	7	0	4	0	4	0	4	-3	4	-3		
4	191	16	25	16	22	19	22	19	22	12	19	9	16	9	19	9	12		
5																			
<u>Conic Adapter</u>	162	64	94	67	89	61	86	64	83	55	83	58	80	55	77	52	64	5	
1																			
<u>Clock</u>	91	75	71	75	71	77	71	75	71	69	64	66	64	69	62	66	60	5	
1	95	75	73	77	73	77	73	77	71	71	64	69	64	69	62	66	62	6	
2																			
<u>Thrust Cone "A" to "B" SRV</u>	119	62	58	62	57	60	56	60	56	68	64	65	63	64	62	63	61	6	
1	76	86	81	86	80	84	79	84	77	79	74	74	72	72	71	69	67	7	
2																			
<u>Stellar-Index Camera</u>	86	92	89	92	89	92	86	92	83	76	70	70	67	67	64	64	64	6	
1	64	79	76	79	73	79	73	79	70	69	62	65	59	62	59	62	59	5	
2																			
<u>Recovery Battery "B" SRV</u>	68	79	81	84	84	84	82	84	82	81	81	81	79	80	82	80	84	8	
1																			
<u>Master Cassette</u>	90	55	48	52	48	53	50	53	50	-	-	-	-	-	-	-	-	-	
1																			

TABLE 3-4

VEHICLE 1177 PAYLOAD J-11 SELF-HEATING TEST

SUMMARY OF SELF-HEATING CORRECTION CURVES

TS TC2	TS TC1	TS 203	TS 212	TS 110	TS 207	TS 2
TS SS2	TS SS1	TS 209	TS 103	TS 210	TS 113	TS 1
		TS 106	TS 206	TS 213		
		TS 109	TS 205			
		TS 105	TS 108			
		TS 104	TS 112			
		TS 208	TS 107			
		TS 204				

<u>Time</u> <u>(Min)</u>	<u>No. 1</u>	<u>No. 2</u>	<u>No. 3</u>	<u>No. 4</u>	<u>No. 5</u>	<u>No. 6</u>	<u>No. 7</u>
0.10	0.5	0.5	0.9	1.1	1.3	2.0	4.0
0.13	0.6	0.6	1.1	1.4	1.6	2.6	5.0
0.16	0.7	0.8	1.4	1.8	2.0	3.2	6.0
0.20	0.9	1.0	1.6	2.0	2.3	3.6	7.0
0.25	1.0	1.2	1.8	2.3	2.5	3.9	8.0
0.32	1.1	1.4	2.1	2.5	2.9	4.4	10.0
0.40	1.3	1.7	2.4	2.9	3.3	4.9	12.0
0.50	1.6	2.0	2.8	3.4	3.8	5.6	14.0
0.63	1.9	2.5	3.4	3.9	4.5	6.4	16.0
0.79	2.1	2.8	3.7	4.3	5.0	7.0	18.0
1.00	2.2	3.0	4.1	4.7	5.4	7.6	20.0
1.26	2.3	3.1	4.4	5.0	5.7	8.1	21.0
1.58	2.5	3.3	4.7	5.4	6.1	8.6	22.0
2.00	2.6	3.5	5.1	5.8	6.6	9.3	23.0
2.51	2.7	3.6	5.3	6.1	6.9	9.6	24.0
3.16	2.8	3.7	5.6	6.4	7.3	10.1	24.0
3.98	2.9	3.8	6.0	6.8	7.7	10.7	25.0
5.01	3.0	4.0	6.4	7.3	8.3	11.4	27.0
6.31	3.1	4.1	6.7	7.6	8.6	11.8	27.0
7.94	3.1	4.1	7.0	7.9	9.1	12.3	28.0
10.00	3.2	4.3	7.4	8.4	9.6	13.0	28.0
12.59	3.3	4.3	7.6	8.7	9.9	13.4	29.0
15.85	3.3	4.4	7.9	9.0	10.4	13.8	29.0
19.95	3.4	4.4	8.3	9.5	10.9	14.5	29.0
25.12	3.4	4.5	8.6	9.8	11.3	14.9	30.0
31.62	3.5	4.5	8.9	10.2	11.8	15.4	30.0
39.81	3.5	4.5	9.2	10.5	12.2	15.7	30.0
50.12	3.6	4.6	9.5	10.9	12.7	16.2	30.0
63.10	3.6	4.6	9.8	11.3	13.2	16.7	30.0
79.43	3.7	4.6	10.1	11.7	13.7	17.1	30.0
100.00	3.7	4.7	10.4	12.2	14.3	17.7	30.0

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SECTION 4

MISSION 1010-1 RECOVERY SYSTEM

SRV #644 was received at A/P on 4 October 1963. The receiving weight was 147 pounds. After modifications and incorporation of outstanding E.O.'s, the SRV was delivered to systems test for incorporation into the J-11 system.

The following major modifications were made to SRV #644 during the testing phase at A/P:

1. 10/4/63 - The electronic components in the thrust cone were flowcoated.
2. 10/5/63 - The W-4 cable was found to be damaged at the plug and was replaced.
3. 6/2/64 - FEDR 1310; the water seal gasket was replaced as it had lifted out of its groove.
4. 6/30/64 - The mating studs were reworked as they were not shorted to the thrust cone ring.

The capsule was delivered for shipment to VAFB on 13 July 1964. No components were replaced or repaired at VAFB.

A successful air catch of the capsule was made on orbit 65. The impact point was within normal tolerances. All capsule re-entry events occurred within tolerance. Table 4-1 lists the sequence of monitored re-entry and recovery event times.

The condition of the recovered capsule was satisfactory with damage limited to normal paint blistering. Post flight inspection and test showed no anomalies.

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MISSION 1010-1

RECOVERY SEQUENCE OF EVENTS

<u>Event</u>	<u>System Time</u>	<u>Delta Time</u>	
		<u>Actual</u>	<u>Nominal</u>
Transfer	-	-	-
Electrical Disconnect	-	-	0.90 + .43 - .40
* Separation	4875.50	-	2.00 + .25
** Spin	4878.00	-	3.40 + .30
Retro	4885.00	7.00	7.55 + .45
Despin	-	-	10.75 + .54
T/C Separation	4897.00	-	1.50 + .15
Voltage Mon. Closed	4972.32	75.32	104.00 + 44.
"G" Switch Open	5405.52	433.20	-
Parachute Cover Off	5439.80	34.28	34.00 + 1.5
Drogue Chute Deployed	5440.54	0.74	0.75 + .08
Drogue Chute Release	5450.62	10.08	10.05 + 1.0
Main Chute Deployed	5451.42	0.80	0.80 + .20
Main Chute Disreefed	5455.61	4.19	4.00 + 1.7

* From Transfer

** From Elect. Disc.

The event times not recorded were not available due to noise on the T/M channels.

TABLE 4-1

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SECTION 5

MISSION 1010-2 RECOVERY SYSTEM

SRV #652 was received at A/P on 30 December 1963 at a receiving weight of 154 pounds. After modification and incorporation of outstanding E. O. 's the capsule was delivered to systems test for incorporation into the J-13 system. The original SRV assigned to J-11B produced a soft wrap during the TASC test. SRV #652 was assigned to J-11 on 19 June 1964.

The following modifications were made to SRV #652 during the test phase at A/P:

1. 6/24/64 - The mating studs were reworked to short to the thrust cone ring.
2. 6/30/64 - A lanyard hole was drilled in the forebody to comply with T22-720, revision B.

The capsule was delivered for shipment to VAFB on 13 July 1964. Testing at VAFB was completed without problems.

The second recovery unit was successfully recovered by air catch on orbit 144. The impact point was within normal tolerances. Table 5-1 is a tabulation of the sequence of monitored re-entry and recovery event times.

Post flight inspections and tests showed all events to be normal. Damage to the recovery system was limited to normal blistering of paint.

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MISSION 1010-2

RECOVERY SEQUENCE OF EVENTS

<u>Event</u>	<u>System Time</u>	<u>Delta Time</u>	
		<u>Actual</u>	<u>Nominal</u>
Transfer	3266.00	-	-
Electrical Disconnect	3266.94	0.94	0.90 + .43 - .40
*Separation	3268.00	2.00	2.00 + .25
**Spin	3270.35	3.41	3.40 + .30
Retro	3277.90	7.55	7.55 + .45
Despin	3288.62	10.72	10.75 + .54
T/C Separation	3290.20	1.58	1.50 + .15
Voltage Mon. Closed	3364.22	74.02	104.00 + .44
"G" Switch Open	3841.14	476.92	-
Parachute Cover Off	3875.28	34.14	34.00 + 1.5
Drogue Chute Deployed	3876.00	0.72	0.75 + .08
Drogue Chute Release	3886.00	10.00	10.05 + 1.0
Main Chute Deployed	3886.62	0.62	0.80 + .20
Main Chute Disreefed	3890.75	4.13	4.00 + 1.7

* From Transfer

** From Elect. Disc.

TABLE 5-1

~~TOP SECRET~~

SECTION 6

MASTER (FWD) PANORAMIC CAMERA

A. COMPONENT ASSIGNMENT

Component	Serial Number
Main Camera	152
Main Camera Lens	1252435
Supply Horizon Camera	132B
Supply Horizon Camera Lens	812279
Take-up Horizon Camera	132A
Take-up Horixon Camera Lens	812267
Supply Cassette	SC-26

B. CAMERA DATA AND FLIGHT SETTINGS

Main Camera:

Lens	24" f/3.5
Slit Width	0.175"
Filter Type	Wratten
Film Type	Eastman Type 3404

Supply (Port) Horizon Camera:

Lens	55mm f/6.8
Aperture Setting	f/6.8
Exposure Time	1/100 second
Filter Type	Wratten 25

Take-up (Starboard) Horizon Camera:

Lens	55mm f/6.8
Aperture Setting	f/8.0
Exposure Time	1/100 second
Filter Type	Wratten 25

C. POST FLIGHT PERFORMANCE EVALUATION

The quality of the photography produced by the Master camera was very good throughout both missions. The information content of the photography was considered excellent. The missions were considered approximately equal to Mission 1009. A small soft area was present at the take-up end of the format during Mission 1010-1 however it was not present during Mission 1010-2.

The electro-mechanical operation of the camera system was normal during both missions. Light leaks affected the third frame from start and fifth frame from end of most passes. The magnitude of the fog caused by the leaks correlates with the length of camera sit time. These frames are located between the shutter and input metering roller and near the Recovery Barrel-Fairing interface.

Emulsion scratches were present at each end of the format during both missions. A fine scratch, about two inches long, was at the take-up end near the camera number edge and a series of short scratches were near both format edges under the data block. The data lost by this degradation is exceedingly small however the released emulsion can produce minus density streaks if it becomes deposited on the field flattener or filter. This streaking was observed during thirty-nine frames pass D88.

The emulsion scratches near the data block are attributed to sharp edges on the scan head rollers. Steps have been taken to hone the roller edges on future cameras.

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The horizon camera and associated fiducials operated satisfactorily throughout both missions as did the data block, end-of-pass mark and time track. The time track was too close to the format but was usable.

Minor edge static was observed at random intervals through both missions. The character of the static pattern indicated that it could have been produced either on the ground or in flight. No corona discharge was observed.

~~TOP SECRET~~ [REDACTED]

SECTION 7

SLAVE (AFT) PANORAMIC CAMERA

A. COMPONENT ASSIGNMENT

Component	Serial Number
Main Camera	153
Main Camera Lens	1282435
Supply Horizon Camera	164B
Supply Horizon Camera Lens	813527
Take-up Horizon Camera	166A
Take-up Horizon Camera Lens	814014
Supply Cassette	SC-26

B. CAMERA DATA AND FLIGHT SETTINGS

Main Camera:

Lens	24" f/3.5
Slit Width	0.175"
Filter Type	Wratten 21
Film Type	Eastman Type 3404

Supply (Starboard) Horixon Camera:

Lens	55mm f/6.8
Aperture Setting	f/8.0
Exposure Time	1/100 second
Filter Type	Wratten 25

Take-up (Port) Horizon Camera:

Lens	55mm f/6.8
Aperture Setting	f/6.8
Exposure Time	1/100 second
Filter Type	Wratten 25

C. POST FLIGHT PERFORMANCE EVALUATION

The photographic quality and information content of the imagery produced by the Slave camera during both missions was comparable to the Master camera photography. The photography was degraded by the minor effects of the usual light leaks and minus density streaks.

The formats were also degraded by emulsion scratching but to a lesser degree than the Master camera. Scratching was limited to the take-up end, data block edge, where fine scratches and some abrasion was present. The largest scratch was about four inches long.

A minus density streak of variable length was present from pass D04 to D07. It was about 1/2 inch wide and varied from six to thirty inches long however the photographic effect was minor. It is postulated that a piece of material became lodged in the filter area and was in the slit area intermittently through pass D07 when it fell away.

Intermittent dendritic static was noted in a few random frames originating at the film edge. As in the case of the Master camera, the marking could have been created in flight or on the ground.

The horizon cameras and fiducials operated satisfactorily throughout both missions. The data block functioned properly during the missions as did the end-of-pass mark.

The time track was very good during both missions with the exception of the first frame of passes D06, D07 and A09E. In these cases the time track was continuous for the first frame however the 200 cycle pulse could be detected.

SECTION 8

PANORAMIC CAMERA EXPOSURE

The exposure parameters for both cameras were a 0.175 inch wide slit and a Wratten 21 filter. Historically a 0.200 inch wide slit has been incorporated in cameras flown during September. The narrower slit was selected to achieve a better match of camera and film processing as well as reducing the sensitivity of the system to image motion.

The illumination conditions during both missions were slightly lower than experienced during recent missions. The frequency distributions of the solar elevations and solar azimuths encountered during the photographic operations are shown in Figures 8-1 to 8-4.

The nominal exposure times are shown as a function of latitude for passes D-08, D-72 and D-136 in Figures 8-5 to 8-7. The predicted level of processing for the original negative is based on the in-flight performance estimate and is tabulated below with the processing levels reported by

<u>Mission</u>	<u>Camera</u>		<u>Primary</u>	<u>Intermediate</u>	<u>Full</u>
1010-1	FWD	Predicted	0	21	79
		Reported	0	13	87
1010-1	AFT	Predicted	0	21	79
		Reported	0	19	81
1010-2	FWD	Predicted	0	50	50
		Reported	0	16	84
1010-2	AFT	Predicted	0	50	50
		Reported	0	23	77

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The variation between the predicted and reported processing levels is significantly less than observed during recent missions. The use of the narrower camera slit did provide a better exposure - processing match.

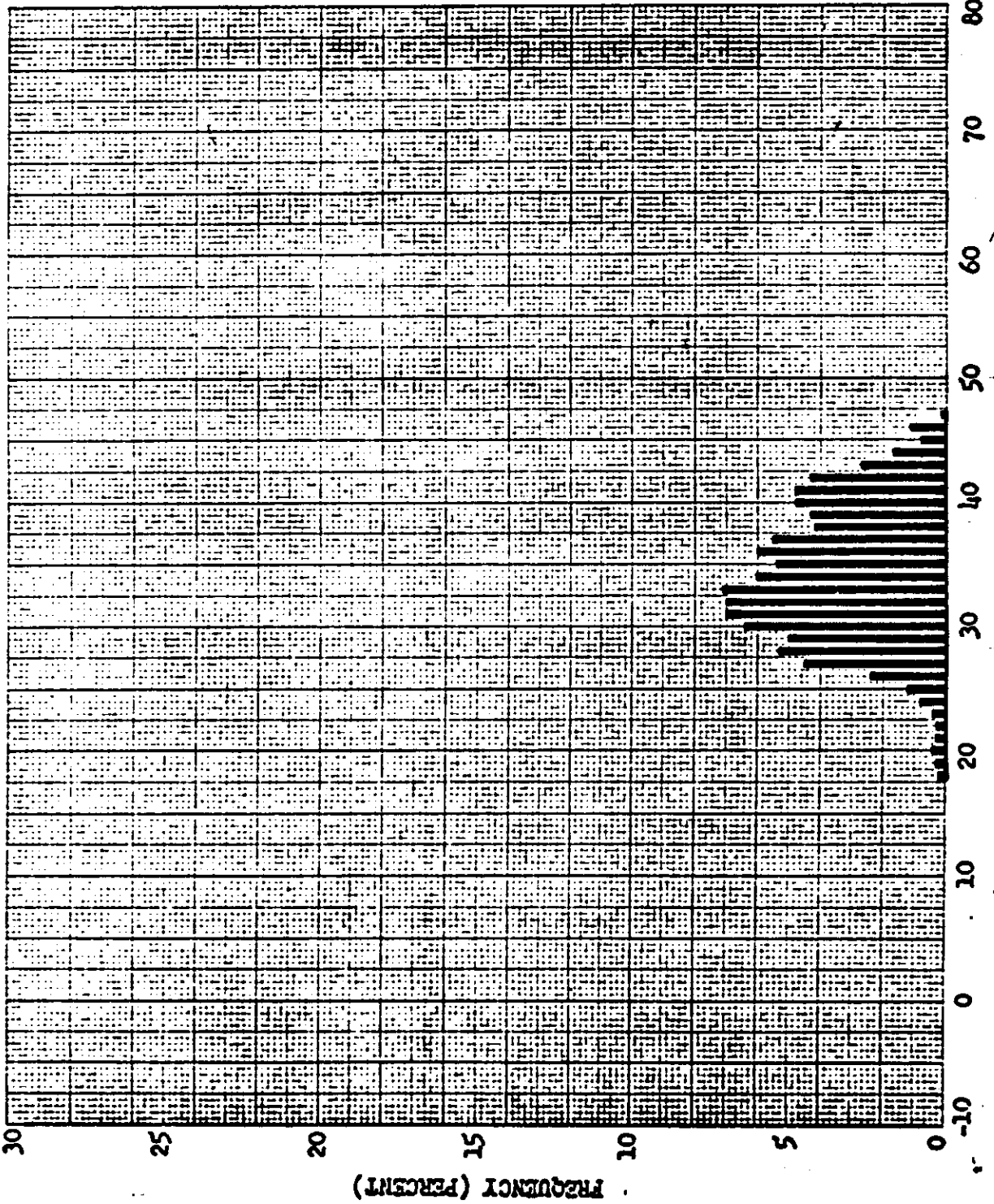
A comparison was made between the exposure time calculated from the time word displayed by the Binary Data Block and the exposure time derived from the 200 cycle time track. The exposure time from these two sources was determined for engineering passes D-47 and D-93 and plotted on Figure 8-8.

The exposure time from all three sources match each other to a much closer degree than observed in recent missions. Normally the Binary Data Block exposure time is approximately 6% slower than the Time Track exposure time.

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SOLAR ELEVATION FREQUENCY DISTRIBUTION



Mission No: 1010-1
Payload No: J-11
Camera No: 152
Launch Date: 9/14/64
Launch Time: 2254 Z
Inclination: 84.9°

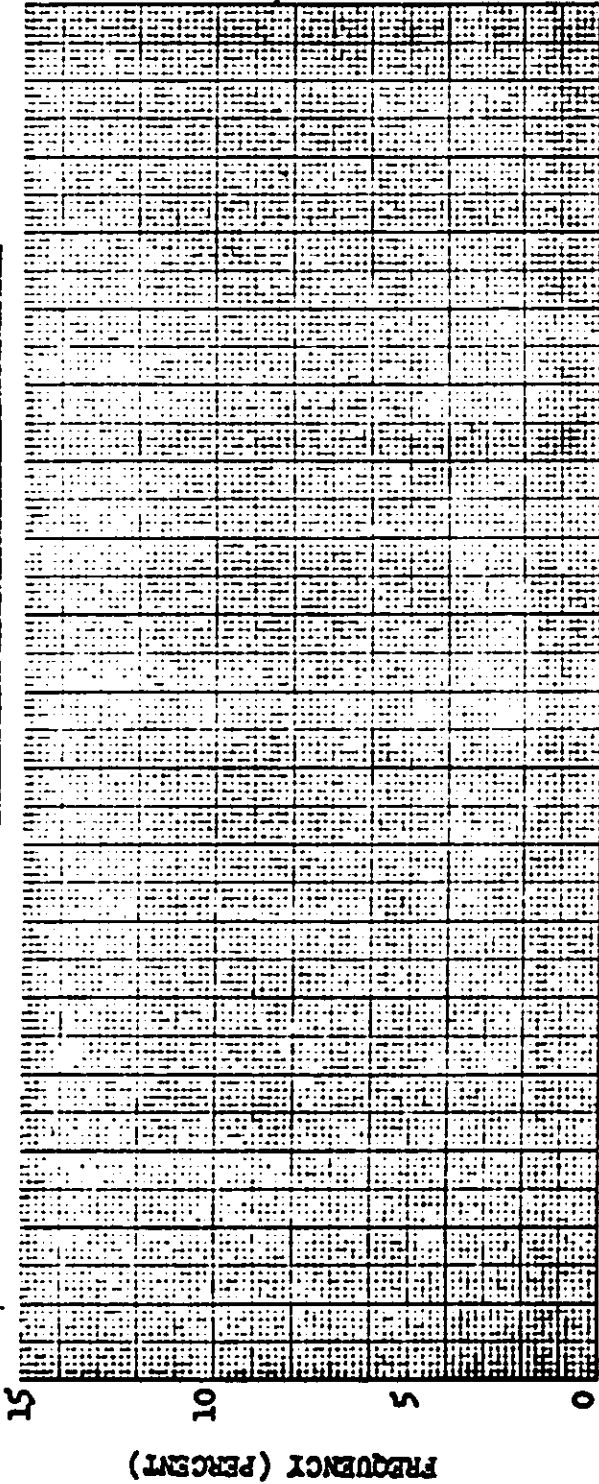
SOLAR ELEVATION (DEGREES)

FIGURE 8-1

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SOLAR AZIMUTH FREQUENCY DISTRIBUTION



Mission No: 1010-1

Payload No: J-11

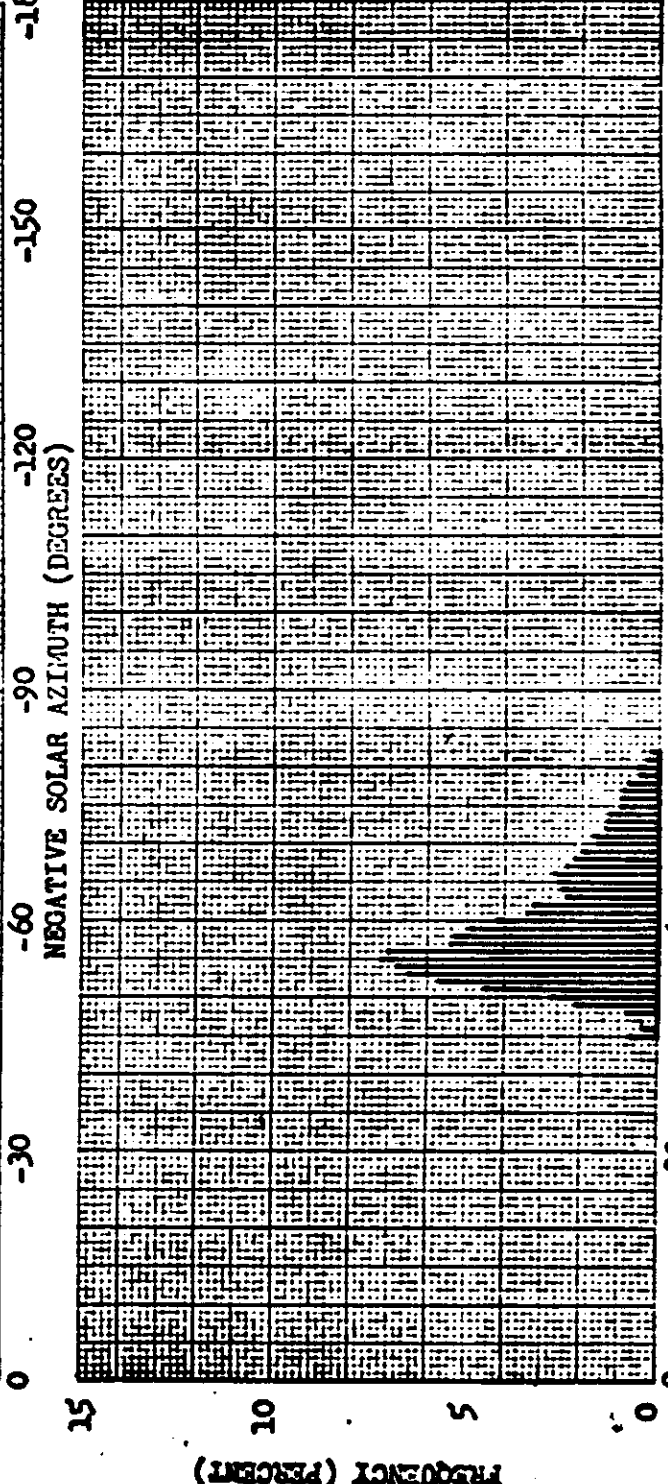
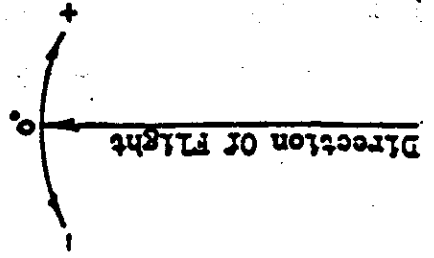
Camera No: 152

Launch Date: 9/11/64

Launch Time: 2254 Z

Inclination: 84.9°

SIGN NOTATION



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SOLAR ELEVATION FREQUENCY DISTRIBUTION

Mission No: 1010-2

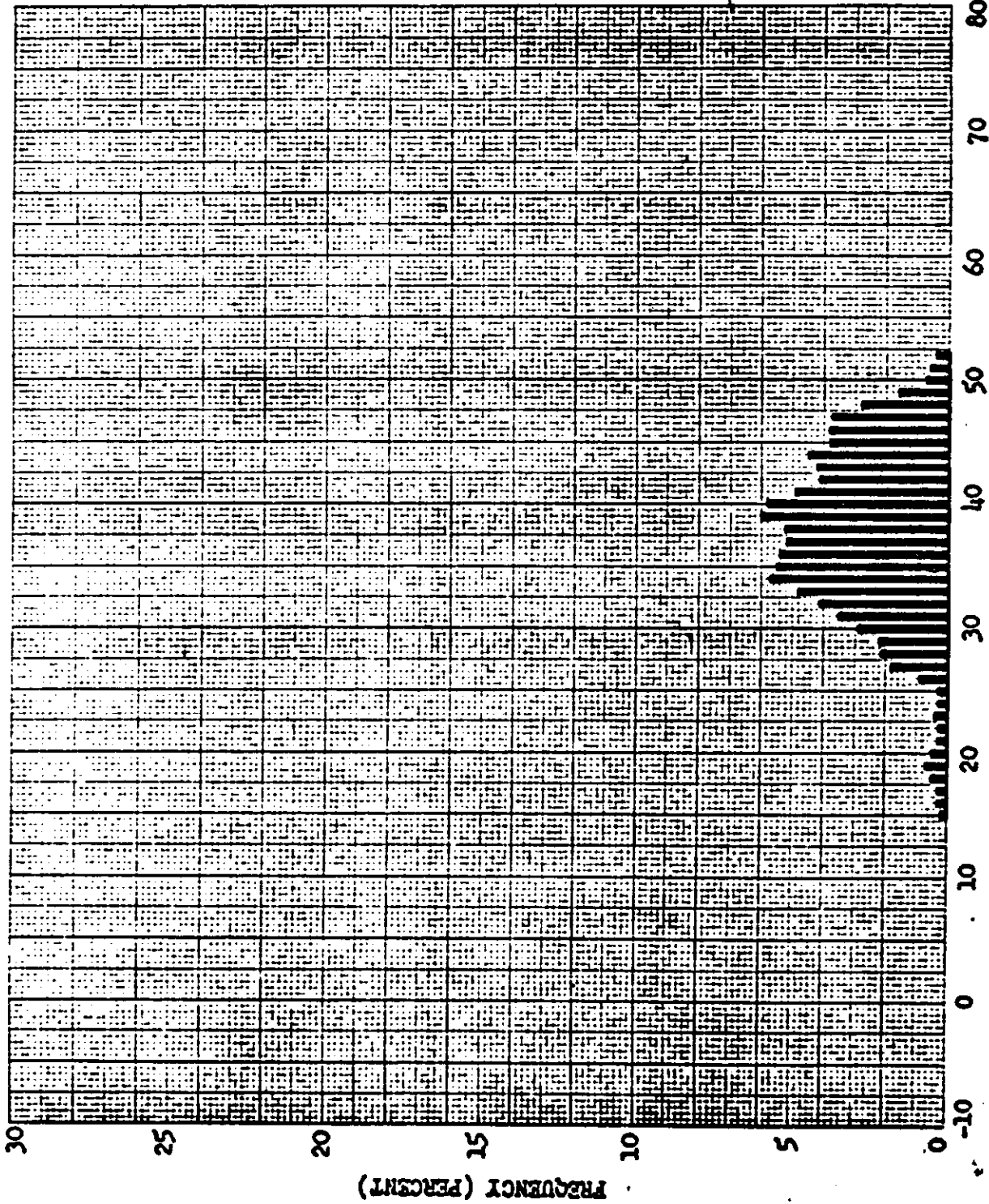
Payload No: J-11

Camera No: 152

Launch Date: 9/14/64

Launch Time: 2254 Z

Inclination: 84.9°



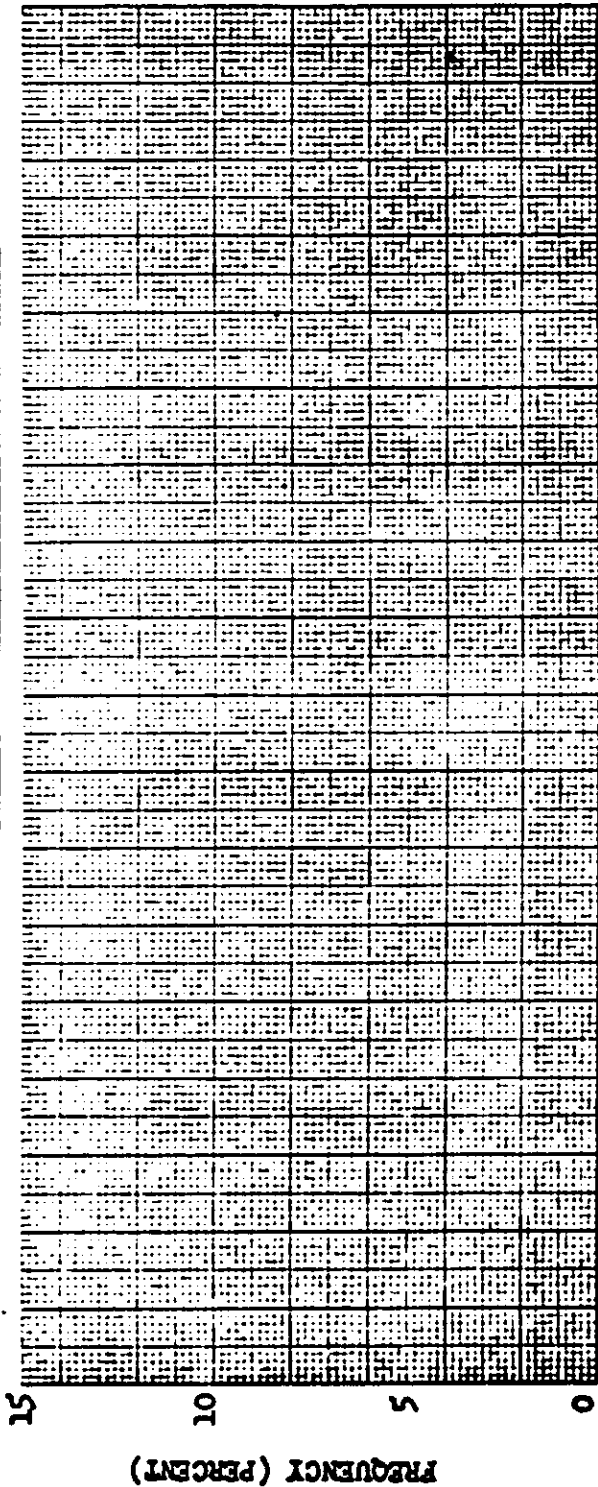
SOLAR ELEVATION (DEGREES)

FIGURE 8-3

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SOLAR AZIMUTH FREQUENCY DISTRIBUTION



Mission No: 1010-2

Payload No: J-11

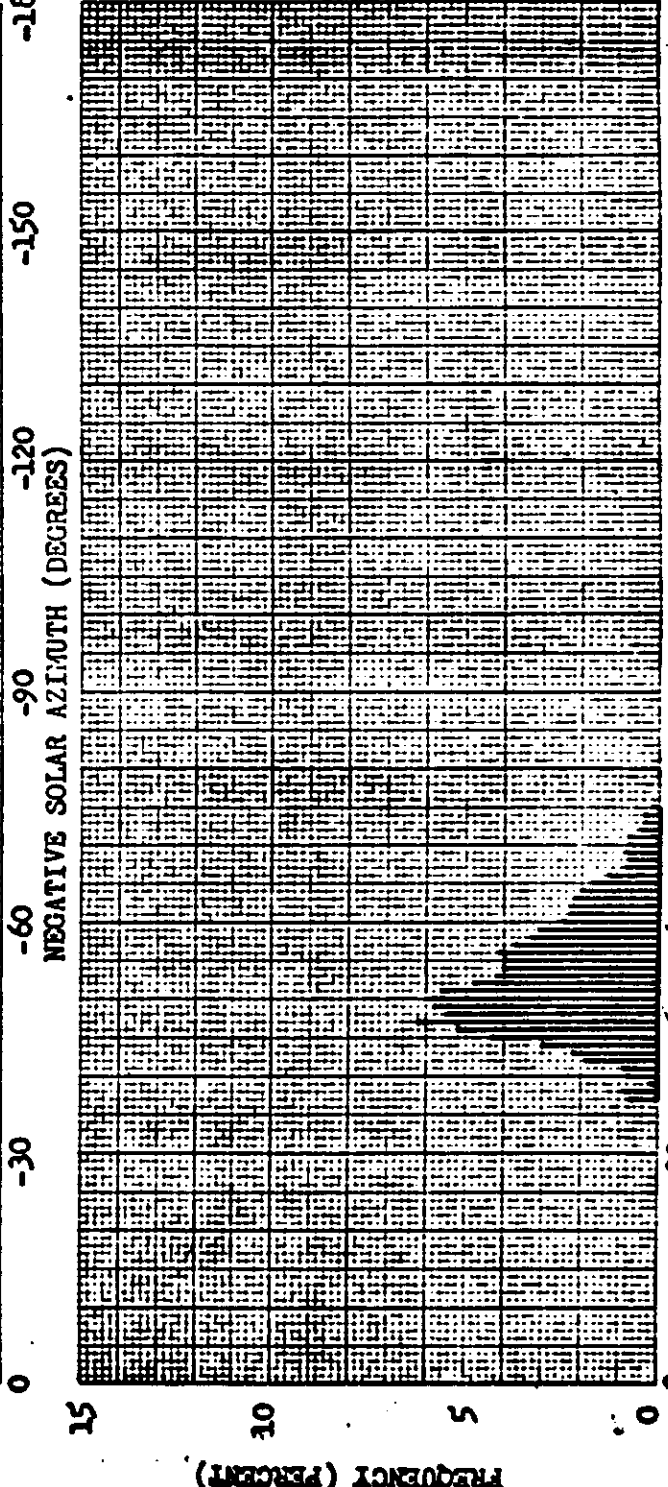
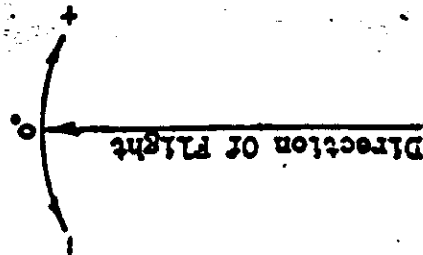
Camera No: 152

Launch Date: 9/14/64

Launch Time: 2254 Z

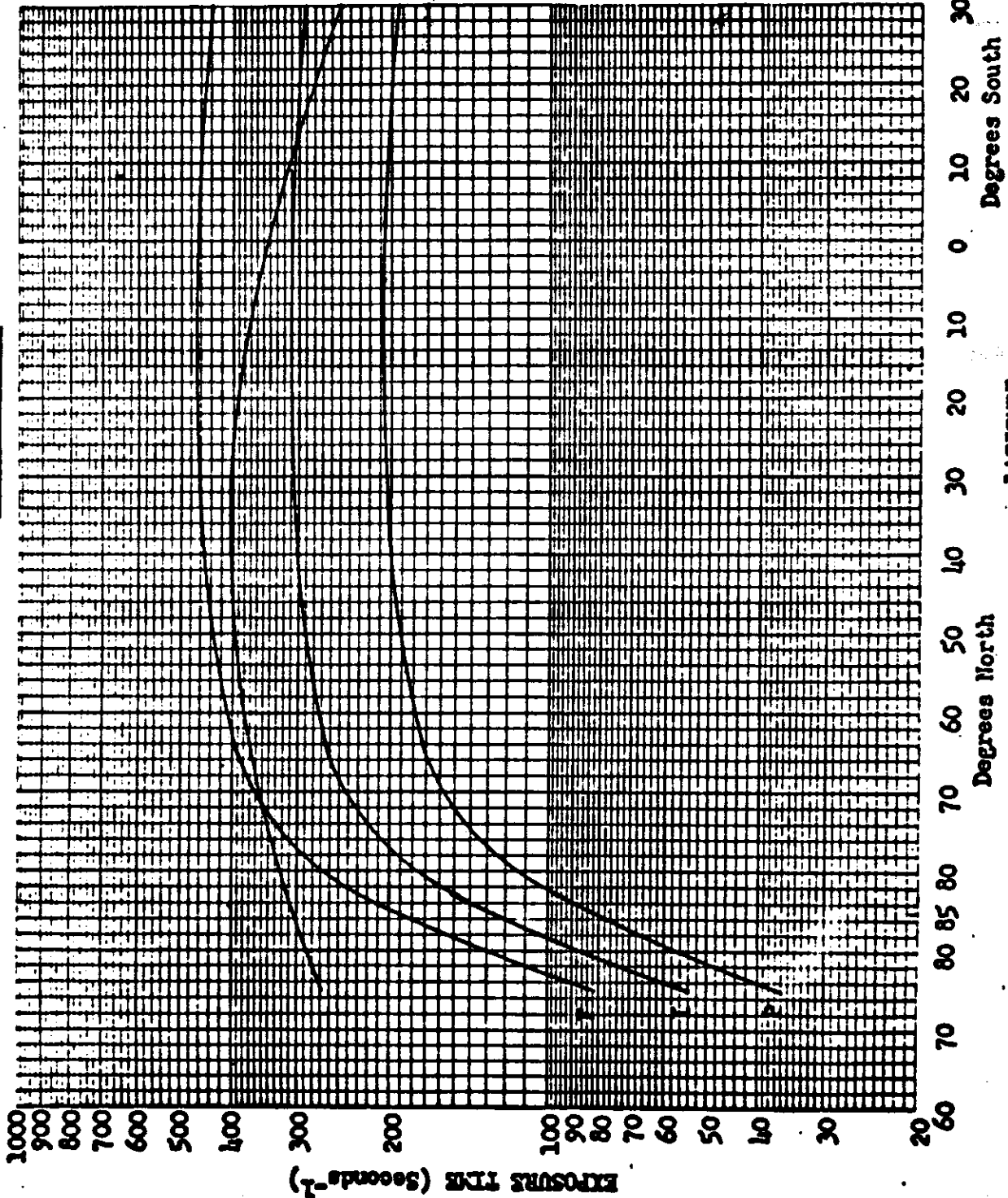
Inclination: 84.9°

SIGN NOTATION



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EXPOSURE POINTS

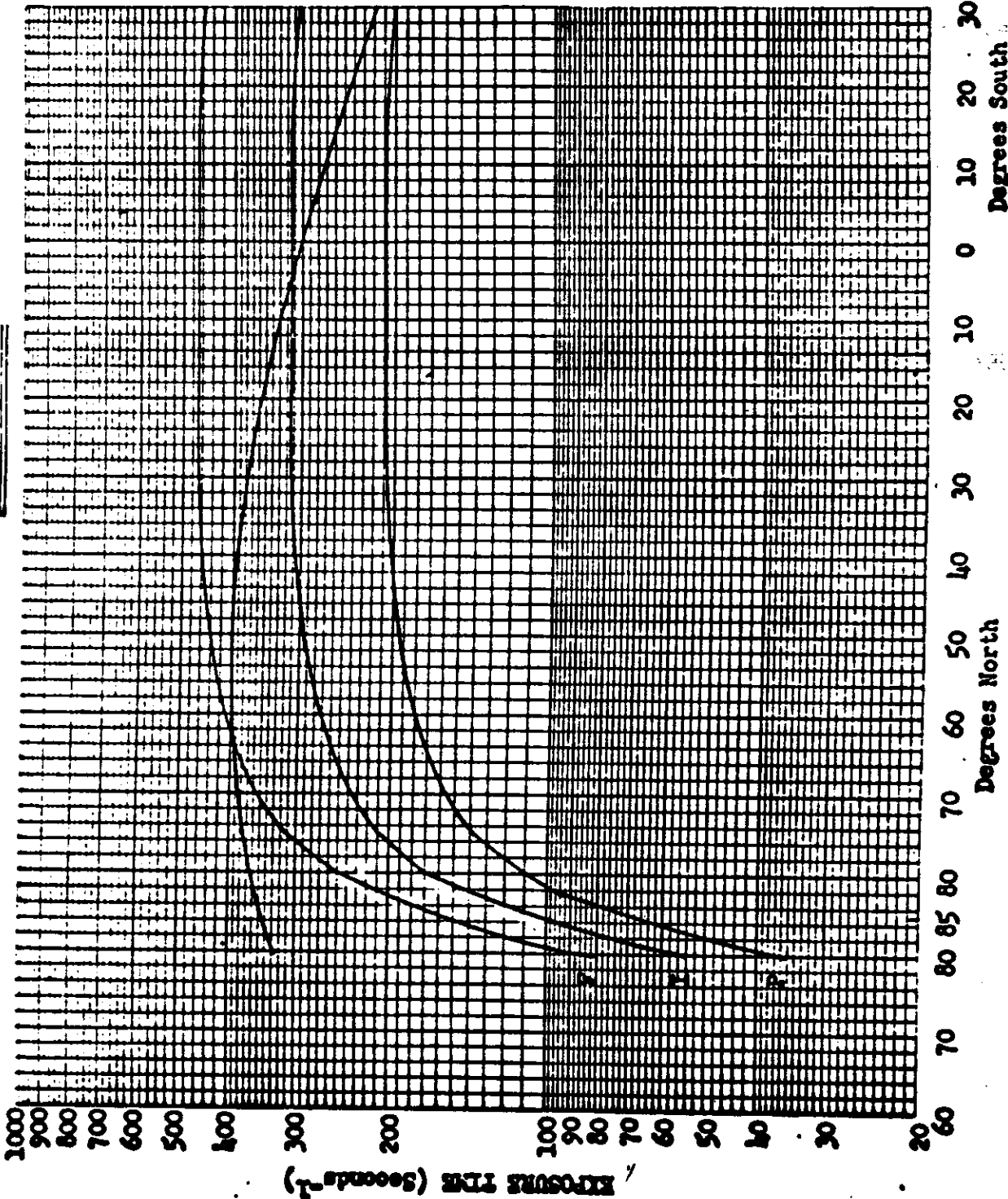


Mission No: 1010
 Payload No: J-11
 Camera No: 152 - 153
 Pass No: 8
 Launch Date: 9/11/64
 Launch Time: 2253 Z
 Slit Width: .175
 Filter Type: Wratten 21
 Film Type: M404

FIGURE 8.5

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EXPOSURE POINTS



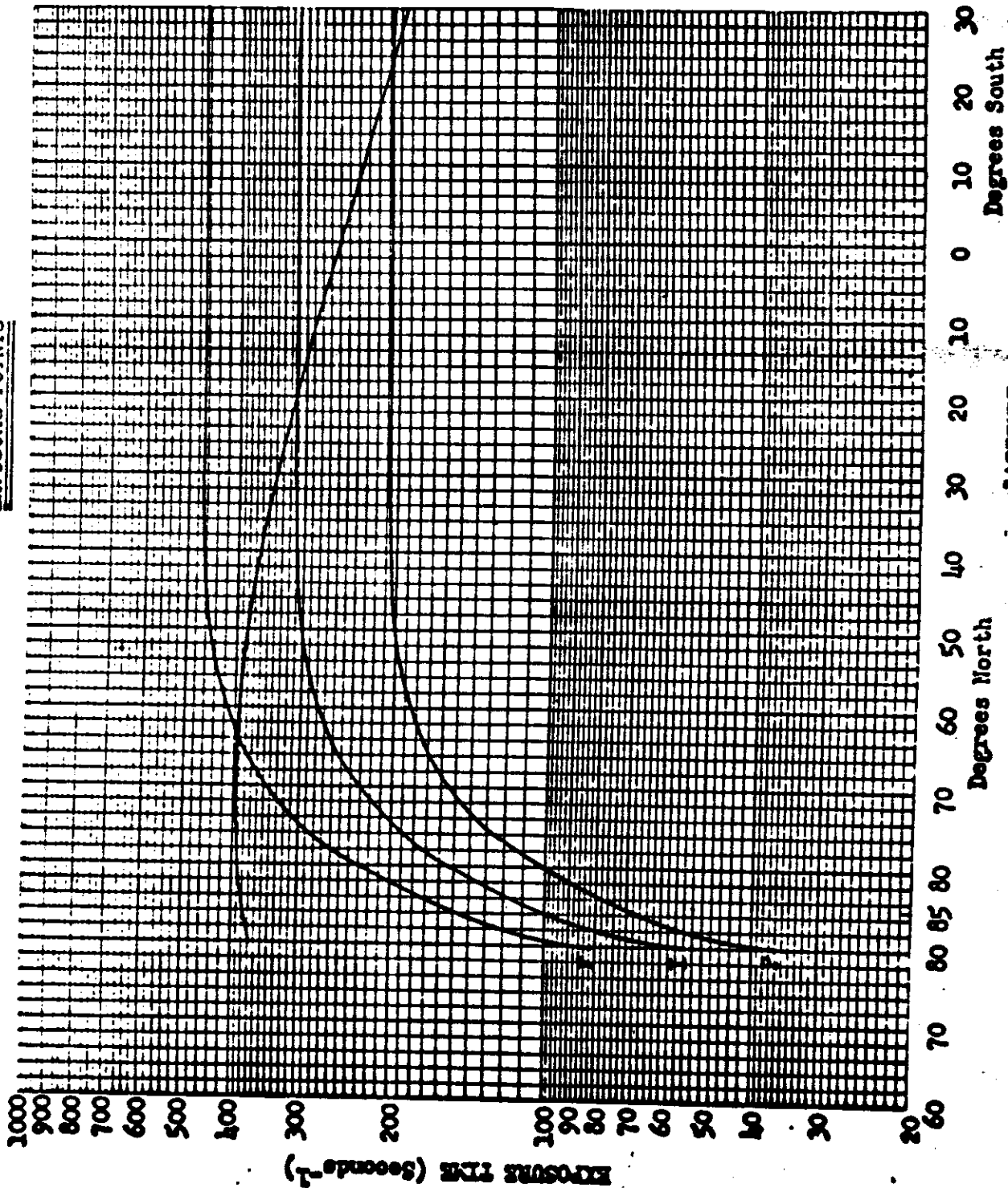
Mission No: 1010
 Payload No: J-11
 Camera No: 152 - 153
 Pass No: 72
 Launch Date: 9/11/64
 Launch Time: 2253 Z
 Slit Width: .175
 Filter Type: Wratten 21
 Film Type: 1444

LATITUDE

FIGURE 8-6.

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EXPOSURE POINTS

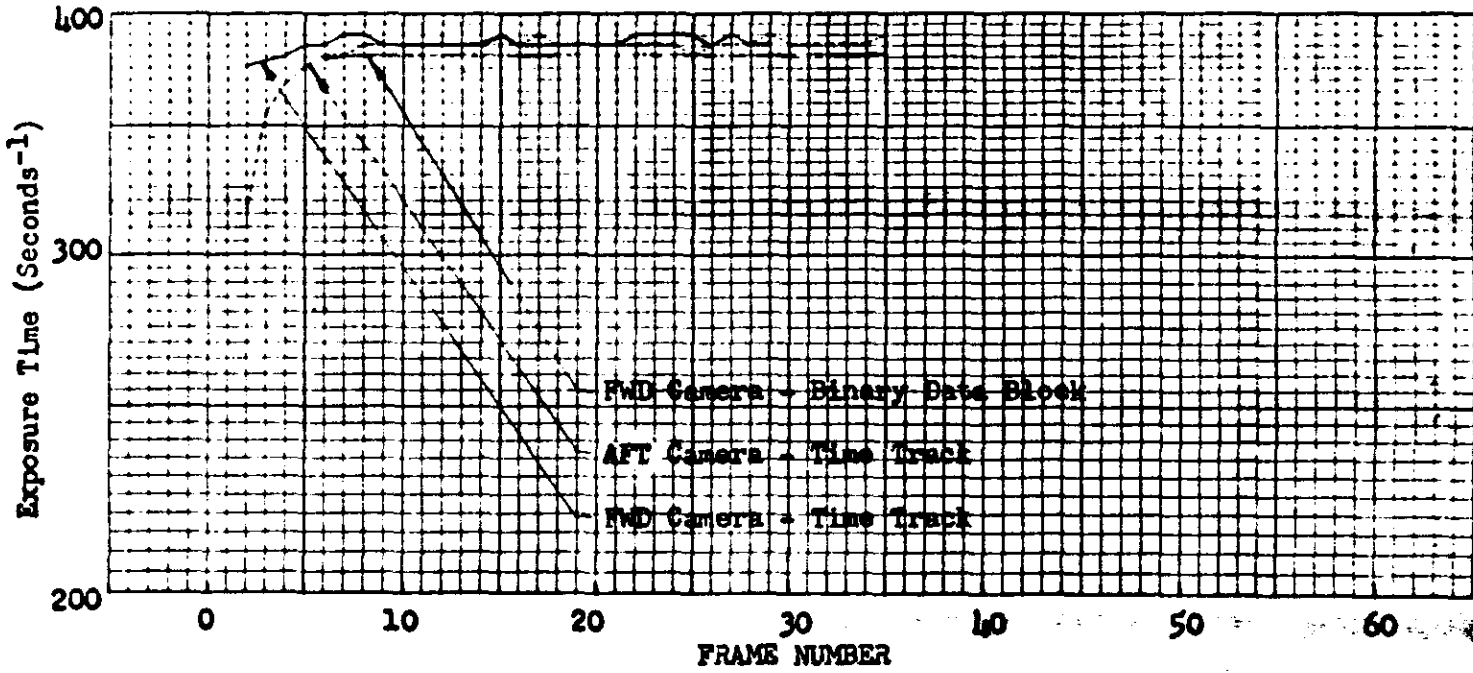


Mission No: 1010
 Payload No: J-11
 Camera No: 152 - 153
 Pass No: 136
 Launch Date: 9/14/64
 Launch Time: 2253 Z
 Slit Width: .175
 Filter Type: Wratten 21
 Film Type: W404

LATITUDE
FIGURE 8-7

EXPOSURE TIME VARIATION

MISSION 1010-1
PASS D47



MISSION 1010-2
PASS D93

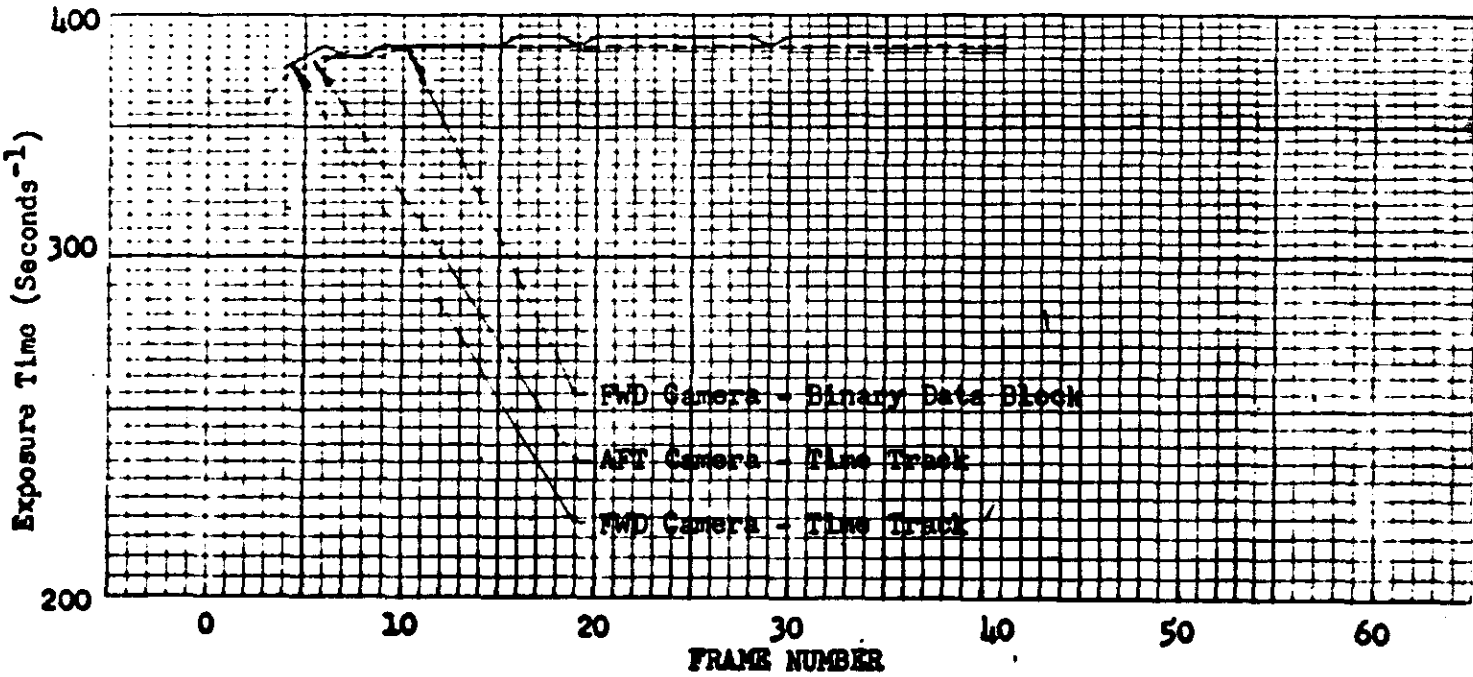


FIGURE 8-8

**SECTION 9
DIFFUSE DENSITY MEASUREMENTS**

Tables 9-1 and 9-2 list mission data supplied by AFSPPL. This data includes the visual Reciprocal Edge Spread (RES) values, the area on the format in which the value was obtained and the general characteristics of the edge as shown on the data key page. The densitometric measurements of the base plus fog, minimum and maximum terrain densities and the maximum cloud densities are also listed with other general data such as solar elevation, latitude and overlap.

The columns are arranged in the following order:

<u>COLUMN NUMBER</u>	<u>HEADING</u>	<u>DATA</u>
1	-	Ascending or Descending pass
2-4	Pas Nbr	Pass Number
5	-	FWD or AFT camera
6-8	Frm Nbr	Frame Number
9-17	Area 1 RES	RES data in area 1
9-11	WWW	With flight RES value
12-14	AAA	Across flight RES value
15	S	Subject - see key
16	T	Terrain - see key
17	Q	Qualifiers - see key
18-26	Area 2 RES	RES data in area 2
27-35	Area 3 RES	RES data in area 3
36-44	Area 4 RES	RES data in area 4
45-53	Area 5 RES	RES data in area 5
54-56	D min	Terrain minimum density
57-59	D max	Terrain maximum density
60-62	D B+F	Base plus fog density
63-65	LIM max	Cloud maximum density

<u>COLUMN NUMBER</u>	<u>HEADING</u>	<u>DATA</u>
66-68	LAT.	Latitude
68	T.	0 = North, 1 = South
69-71	Sun Ele	Solar Elevation
73-74	CLD	Percent cloud cover
75-76	OL	Percent overlap

The data key for the listings of the "Subject", "Terrain" and "Qualifiers" is shown below.

I SUBJECT

1. Buildings
2. Roads, runways
3. Tanks, A/C, other man-made
4. Non-cultural

II TERRAIN

1. Flat
2. Hilly
3. Mountains
4. Flat and snow
5. Hilly and snow
6. Mountains and snow

III EDGE QUALIFIERS

1. Clear
2. Snow
3. Hazy
4. Shadow
5. Snow and Haze
6. Snow and Shadow
7. Haze and Shadow
8. Snow, Haze and Shadow

101C-1

TABLE 9-1

PAS FRMAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D U LIM SUN

ABR ABRHHWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQWWHAAASTQMINMAXB+FMAXLATELECLUOL

CCC1FCC5		01221056N+2710099
CCC1FC08		01421855N+2810099
CCC4FCC5	C78061431	04221601419461N+2403000
CCC4FC15		03423202121260N+25 99
CCC4FC25		019 58N+2600099
CCC4FC36		02200056N+2800199
CCC5FC07	078078412	05309702021852N+2906099
CCC5FC17		05111102021950N+30 99
CCC5FC27	065072411	06310602021349N+3109099
CCC5FC37		04712302022647N+32 99
CCC5FC47	C94094111	04612202023146N+3300505
CCC5FC57		04811402024044N+33 99
CCC5FC67	C94085111	04518002020042N+3400105
CCC5FC77		03110202015241N+35 99
CCC5FC87	C94094111	03718802018039N+3500504
CCC5FC97		02021637N+36 99
CCC5F107		01422136N+3710099
CCC5F115		01422134N+3809699
CCC6FC05	C67C63421	05814201600041N+3500002
CCC6FC15		03614201422840N+3600499
CCC6FC25	C94085121	04020602223038N+3600506
CCC6FC35		04017702224037N+3602599
CCC6FC45	C94104131	03216402223535N+3701005
CCC6FC55		03215402222434N+3700599
CCC6FC65	085099431	03413002224232N+3802506
CCC6FC75		04017302224031N+3802099
CCC6FC85		02223729N+3910099
CCC6FC95		01522527N+3910099
CCC6F104	G78072431	04710701822626N+3909099
CCC6F114		04012802123924N+4004099
CCC6F124	C75C82421	03813602124223N+4004507
CCC6F134		04710902123421N+4103099
CCC6F144	C85078121	04308702123820N+4103508
CCC6F154		06211702122218N+4204099
CCC7FCC5	C7CC67411	04007502218858N+2600105
CCC7FC15		04509002200057N+2799999
CCC7FC25	C82078111	04610002200055N+2899907
CCC7FC35		05008502200054N+2999999
CCC7FC45	C85085111	05416602200052N+3099907
CCC7FC55		05815502200050N+3199999
CCC7FC65	C72C67421	06019002200049N+3200006
CCC7FC75		07816402200047N+3299999
CCC7FC85	C85078421	06018202000045N+3300005
CCC7F1C1		08614201600039N+3699999
CCC7F111078078111		06313801400037N+3700099
CCC7F121		04119401523936N+3799999
CCC7F131	C78C82421	04620202023434N+3805099
CCC7F141		04321602023033N+3899999
CCC7F151	C9CC90431	04721702024231N+3902004
CCC7F161		06111102024230N+3999999

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PAS FRMAREAL RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NBR NBRHHWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQMINMAXB+FMAXLATELECLUOLF

CC23FC05		06507241104816002120460N+2507099
CC23FC15		04807202122359N+2699999
CC23FC25	C75082111	05011002121857N+2705007
CC23FC35		07012602121956N+2899999
CC23FC45	072072112	06012402119454N+2909999
CC23FC55		06215002122153N+2999999
CC23FC65	078072112	07013802122451N+3008599
CC23FC75		06811002122349N+3199999
CC23FC85		06306741207812202121848N+3209799
CC23FC95		05119202121246N+3399999
CC23F105	C70072411	04816602100045N+3400005
CC23F115		06015002100043N+3499999
CC25FC06	078072112	07008402121258N+2609899
CC25FC16		04507102121357N+2799999
CC25FC26	C94094111	04811302116955N+2800205
CC25FC36		04107902111153N+2999999
CC25FC46	C99094111	04011802100052N+3000006
CC25FC56		04013802100050N+3199999
CC25FC66	C99099111	03411002100049N+3200005
CC25FC76		03411002121147N+3299999
CC25FC86	C94104111	03211802118246N+3300006
CC25FC96		04812002017844N+3499999
CC25F106	C94099111	03910602118642N+3504005
CC25F116		04513002021241N+3699999
CC25F123	C85088411	05212802021040N+3700505
CC31FC05	C67070122	04215202023035N+3805500
CC31FC15		03617602024033N+3999999
CC31FC25	C50063421	04419902021631N+4001004
CC31FC32	C82090122	03816002222030N+4101504
CC36FC05		09909411104519702120652N+3008099
CC36FC15		04720202121851N+3105099
CC36FC25	C94104112	04410702122049N+3205005
CC36FC35		04211102122648N+3304599
CC36FC45	078070112	04819702022547N+3404099
CC36FC55		04208702022545N+3503099
CC36FC65		01921743N+3501099
CC36FC75		01921841N+3602099
CC36FC78		01922041N+3704099
CC37FC05		01821259N+2510099
CC37FC15		01520058N+2699999
CC37FC25		01420657N+2709599
CC37FC35	C94090431	04422402200055N+2800006
CC37FC45		04222602021854N+2999999
CC37FC55	C55070213	05210002123052N+3008099
CC37FC65		04009802122051N+3199999
CC37FC75		02222249N+3209999
CC37FC85		04612402221848N+3299999
CC37FC95	052056431	06814202123430N+4107099
CC37F105		04017802222828N+4299999
CC37F115	C64072112	04612202122627N+4205006

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PAS FRMAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NBR NBRHHWAAASTQHHWAAASTQHHWAAASTQHHWAAASTQHHWAAASTQMINMAXB+FMAXLATELECLDOL

CC37F125		04812802121225N+4399999
CC37F135	C78065133	08017002122023N+4306506
CC37F145		02122222N+4399999
CC37F154		02121421N+4410099
CC38FCC5C67C65111		03808202000057N+2600005
CC38FC15		03209502000056N+2799999
CC38FC25	C75078411	02808002000054N+2800005
CC38FC35		02811002000053N+2999999
CC38FC45	C85078411	02814702017652N+3000105
CC38FC55		03210402022050N+3199999
CC38FC65	C85C85111	03815402022849N+3200505
CC38FC75		04014802022847N+3399999
CC38FC88	C7CC72421	03411401621441N+3600503
CC38FC98		04014001417640N+3799999
CC38F108	C78082431	03816401200038N+3800003
CC38F118		02819201200037N+3899999
CC38F128	C94094421	03821801200035N+3900004
CC38F138		02820001200034N+4000099
CC38F148	C82C90121	03422001821032N+4000504
CC38F158		04018001822831N+4199999
CC38F168	C94099121	04615602023029N+4105005
CC38F178		02023028N+4299999
CC38F186	C82C90421	05809002023027N+4309005
CC39FC06		06707241205206801821559N+2509599
CC39FC16		01822058N+2699999
CC39FC26		01222256N+2710099
CC39FC39063067412		04608601220254N+2909999
CC39FC49		07012801921953N+2999999
CC39FC59	C78080411	05911801922951N+3006006
CC39FC69		07912001922250N+3199999
CC39FC83	C82C80411	08612501922348N+3309506
CC39FC93		08015501921746N+3399999
CC39F103	C85C85412	09118201921245N+3406005
CC39F113		07015601922343N+3599999
CC39F123	09C094111	07018501921242N+3601505
CC39F133		06016901921440N+3799999
CC39F137	C78C85112	06816101821840N+3802005
CC40FCC5		01821265N+2110099
CC40FC19	CCC078411	03204301621263N+2308599
CC40FC29		03407502022262N+2499999
CC40FC39	C75C75111	02806202020760N+2501006
CC40FC49		02021259N+2699999
CC40FC63	C67C72112	04811402020957N+2707506
CC40FC73		06012802019855N+2899999
CC40FC83	C82C82111	03610602000054N+2900006
CC40FC93		03613602000052N+3000099
CC40F103	C85C82111	03609802000051N+3100006
CC40F113		04514502000049N+3200099
CC40F123	C78078111	05015002000048N+3300005
CC40F133		05814502000046N+3300099

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PAS FRPAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NBR NBRHHWAAASTQHHWAAASTQHHWAAASTQHHWAAASTQHHWAAASTQHINMAXB+FMXLATELECLDCL

CCC4ACC5	C7CC72431	06424202421062N+23030C0
CCC4AC15		08423902422261N+2499999
CCC4AC25	C74C63431	04511002221459N+2500599
CCC4AC36		02210457N+2700299
CCC5ACC5		02321353N+2910099
CCC5AC11C94072412		C7112202123652N+30085C0
CCC5AC21		C7511702124051N+3108099
CCC5AC31		07911402122649N+3109099
CCC5AC33	C99104412	05811402123649N+2107599
CCC5AC43		05011202123847N+3203099
CCC5AC53	111104111	04514702124446N+3301003
CCC5AC63		04910902123444N+3402599
CCC5AC73	078085211	04210902118242N+3500303
CCC5AC83		03910602118441N+3500299
CCC5AC93	C78078411	04510502120639N+3603501
CCC5A103		02119437N+3710099
CCC5A113		02123036N+3810099
CCC5A115		02122635N+3810099
CCC6ACC5	C78090421	06717801600042N+3400002
CCC6AC15		03917501422941N+3503099
CCC6AC25	C94C90431	04418301400039N+3500204
CCC6AC35		03920002223138N+3602099
CCC6AC45	C90104131	04318402122736N+3600804
CCC6AC55		03613202323735N+3701599
CCC6AC65	C78078121	03917102222433N+3701006
CCC6AC75		04112402122931N+3803099
CCC6AC85	C85094112	07414402123530N+3807099
CCC6AC95		02124028N+3910099
CCC6A1C5		02123427N+3910099
CCC6A1C9	C82085421	07313802123126N+3909599
CCC6A119		04215702024225N+4002099
CCC6A129	C85078121	04016202023523N+4004099
CCC6A139		04110602123921N+4102099
CCC6A149	C82075421	04811602023620N+4101510
CCC6A156		06613002223419N+4204099
CCC7ACC5	C61C52412	05011602221458N+2501002
CCC7AC15		04810402200057N+2699999
CCC7AC25	C47C59412	06410402200055N+2700005
CCC7AC35		05111202300054N+2899999
CCC7AC45	C59072111	06411502000052N+2900007
CCC7AC55		06512002100051N+3099999
CCC7AC65	C59073231	06214302100049N+3000006
CCC7AC75		07216002100048N+3199999
CCC7AC85	C72070222	08516002100046N+3200005
CCC7AC95		04415001800045N+3399999
CCC7A105	C73085111	06814801600040N+3600008
CCC7A115		12514801500038N+3699999
CCC7A125	C72083431	04216001521036N+3701502
CCC7A135		03017001523435N+3799999
CCC7A145	C67C70431	02719001423433N+3802003

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PAS FRMAREAL RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NBR NBRHHWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQHMINMAXB+FMXLATELECLDOLF

CC23ACC5	C65065421	05308202222060N+2406099
CC23AC15		05010702223059N+2503099
CC23AC25	C63C67412	04607802222657N+2602008
CC23AC35		07312402223556N+2705099
CC23AC45		02222655N+2810099
CC23AC55	09C085112	07412002223553N+2909599
CC23AC65		07612402222552N+3007599
CC23AC75		07507241107714202223550N+3108099
CC23AC85		02224049N+3210099
CC23AC95	C94085121	07115002224047N+3204502
CC23A105		08018002222846N+3301099
CC23A115	C75082421	07216602200044N+3400005
CC25ACC5		02221858N+2509599
CC25AC15		07807811207814002121857N+2609699
CC25AC25		05810002122155N+2704099
CC25AC35	C85C82111	05213402215254N+2800202
CC25AC45		04813002100052N+2900099
CC25AC55	C94104111	04513002100051N+3000004
CC25AC65		04412002200049N+3100099
CC25AC75	C9CC94111	04815002200048N+3100004
CC25AC85		05012202100046N+3200299
CC25AC95	1C4C94111	03613302221245N+3300204
CC25A105		05615002219843N+3400299
CC25A115	C9C104111	05015202221642N+3502005
CC25A123		05614402223041N+3603099
CC31ACC5	104094111	06614402424435N+3803304
CC31AC15		05217602324634N+3904099
CC31AC25	C67075411	04419602321432N+3900204
CC31AC32		04217602323731N+4000299
CC36ACC5	C63C67422	07618202423952N+2908599
CC36AC15		05919802423051N+3099999
CC36AC25	C63063422	05415002424449N+3108599
CC36AC35		04812402323448N+3299999
CC36AC45	C67C65412	05610002324247N+3306599
CC36AC55		06209602323845N+3499999
CC36AC66	078082111	04214002323043N+3500299
CC36AC78		05413602321042N+3799999
CC37ACC5		02222660N+2410099
CC37AC15		02120659N+2510099
CC37AC25		01620057N+2610099
CC37AC35	C78090432	07222501920856N+2707099
CC37AC45		04622602322054N+2899999
CC37AC55	C82078422	03811902322053N+2905099
CC37AC65		06617202222651N+3009599
CC37AC75	C85C90121	06213002221049N+3108599
CC37AC85		05212802322748N+3207599
CC37AC98	C67C63112	10220402223230N+4109099
CC37A108		07015002323528N+4207599
CC37A118	C78078111	05419802022827N+4206099
CC37A128		05617802223925N+4308099

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PAS FRMAKEA1 RESAREA2 RESAREA3 RESAREA4 RESAREAS RES D D D LIM SUN

NBR NBRHHWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQHMINMAXB+FMXLATELECLDOL

CC37A138	C85C78111	05217402123623N+4304007
CC37A148	C75082111	06118302124022N+4404007
CC38ACC5	C63C67411	03912802300058N+2600003
CC38AC15		03810402200057N+2700099
LC38AC25	CE5C94111	03711902100055N+2800005
CC38AC35		03110102100054N+2900099
CC38AC45	C90094111	03410702100052N+3000005
CC38AC55		03320802121950N+3100399
CC38AC65	C78078431	03920702122149N+3100503
CC38AC75		04116402022847N+3200599
CC38AC87	C9CC90111	07215901800043N+3500003
CC38AC97		03915901517341N+3600599
CC38A107	C75C82411	09716501414239N+3700304
CC38A117		04716501400038N+3700099
CC38A127	C78082411	04422601400036N+3800004
CC38A137		04621101400035N+3900099
CC38A147	CE5C85421	02921201400033N+4000005
CC38A157		03813701421231N+4002099
CC38A167	CC0C65211	05723002023630N+4104506
CC38A177		07123002123228N+4208099
CC38A186		02223827N+4310099
CC39ACC5		07807241207216102323560N+2409099
CC39AC15		07711002223259N+2509599
CC39AC25		02223257N+2610099
CC39AC35		02223556N+2710099
CC39AC4C072078412		09013502222555N+2809599
CC39AC50		09512702222853N+2909099
CC39AC6C	C85104111	06413502223252N+2904504
CC39AC7C		07811802223050N+3007599
CC39AC8C		02122749N+3110099
CC39AC89	111C82111	08311602023047N+3208003
CC39AC99		08315302022346N+3308599
CC39A109	C90094412	10318902021044N+3408004
CC39A119		06114601622443N+3500399
CC39A129	094082111	04915601520041N+3602004
CC39A137		04314601521240N+3704099
CC4CAC05		01221266N+2010099
CC4CAC15		01421465N+2110099
CC4CAC25	CC0078411	04208601821663N+2209599
CC4CAC35		04013002222262N+2399999
CC4CAC45	C90C85111	04210002122460N+2401007
CC4CAC55		02021859N+2599999
CC4CAC69	C72C75112	05613002222057N+2606006
CC40AC79		05812602219055N+2799999
CC40AC89	C75C85111	04212602100053N+2800005
CC40AC99		04013902200052N+2900099
CC40A1C9	C85C85111	04411602200050N+3000005
CC40A119		05016502200049N+3100099
CC40A129	C85C90111	05215602000047N+3200005
CC40A139		06812602200046N+3300099

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PAS FRMAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NBR NBRWAAAASTQWAAAASTQWAAAASTQWAAAASTQWAAAASTQMINMAXB+FMXLATELECLDUL

CC4CA149		C85085111	05618602200044N+3400005
CC4CA159			04012602200043N+3500099
CC40A165		C78082421	03820002121042N+3600205
CC41ACC5			02022658N+2604099
CC41AC11	085078112		05210202020658N+2704599
CC41AC21			06013302022956N+2801599
CC41AC31		111C94111	04708302023055N+2904599
CC41AC49			10015502023249N+3208599
CC41AC59			11814502023448N+3309099
CC41AC62		094085112	10415902023547N+3309099
CC41AC72			05715402023345N+3402099
CC41AC82		C94094112	04614402019644N+3500206
CC41AC88			04213002017043N+3500199
CC47ACC5		C85085211	05420402000037N+3800002
CC47AC15			C7017602021436N+3900599
CC47AC25		C78094111	04918601822435N+4001006
CC47AC35			04816201721033N+4000299
CC52ACC5			04809702322453N+2907599
CC52AC15			02021852N+3010099
CC52AC26	085078112		04411002022950N+3108599
LC52AC36			05014602022449N+3207099
CC52AC49		C94094111	05211602022647N+3308099
CC52AC59			04913002023245N+3405099
CC52AC69		C78078111	04213601822744N+3504003
CC52AC79			01419542N+3610099
CC52AC89			01421241N+3710099
CC52AC97			01822540N+3810099
CC53ACC5	082075111		03508702100054N+2900003
CC53AC15			03919202121453N+3001099
CC53AC25		C90085111	03320402100051N+3100004
CC53AC35			03614602121250N+3201099
CC53AC52		075075421	08416901822043N+3506599
CC53AC62			04012701422041N+3607099
CC53AC72		C85088111	04716101322640N+3703505
CC53AC82			05517701923238N+3703099
CC53AC92		C78082431	06416802023737N+3802006
CC53A102			06213802023735N+3904099
CC53A112		C85085111	05114102022933N+3901006
CC53A122			04514402123632N+4001599
CC53A132			02122930N+4110099
CC53A142			02122528N+4110099
CC53A152			02123627N+4210099
CC53A16C		C78082111	09612402223225N+4309706
CC53A17C			07616402224024N+4305599
CC53A18C		C82082111	06316202123722N+4405008
CC53A19C			06114702123921N+4501599
CC53A20C		C67065112	06618502122519N+4507099
CC53A21C			09119602223517N+4609599
CC53A219			02119916N+4707099
CC54AC05		078085412	07311601921258N+2609099

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PAS FRPAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NBR NBRHHWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQHMINMAXB+FMAXLATELECLDOLP

CC54AC15		06711001920657N+2709599
CC54AC25		01921955N+2810099
CC54AC35		01921554N+2910099
CC54AC4078082112		07311401921053N+3009099
CC54AC50		07710901922251N+3109099
CC54AC60C75085112		06711901922750N+3208599
CC54AC7C		09513301921848N+3309099
CC54AC78		01921847N+3310099
CC54AC89	C78C85432	04421001420136N+3902099
CC54AC99		06815601421835N+4009599
CC54A110		03816401422133N+4108599
CC54A112	C72C67432	04419001322833N+4108099
CC54A122		04520501822831N+4207599
CC54A132	C85078432	07023502123029N+4207505
CC54A142		07622002023728N+4308099
CC54A146		02023427N+4409599
CC55ACC5	094090111	05210202020960N+2509599
CC55AC15		04209501920659N+2699999
CC55AC25	C99094111	04009502021057N+2702504
CC55AC35		04010001921056N+2897999
CC55AC45	1C4104111	05012201922054N+2906099
CC55AC55		06613001822652N+3099999
CC55AC65	C78C72412	08814001922651N+3106005
CC55AC75		05711801921049N+3299999
CC55AC85	C78078411	12516502020448N+3300105
CC55AC95		07615001600046N+3400099
CC55A1C5	C9C088111	03914401300045N+3400005
CC55A112		03213401200043N+3600099
CC55A122	C9CC94111	05615201300039N+3700005
CC55A132		07015001100037N+3800099
CC55A142	C9C099111	05211801200036N+3900099
CC55A148		07014501500035N+4000099
AC56ACC5		02200038S-3194999
CC56ACC5		02119271N+1706099
CC56AC15		02116170N+1905099
CC56AC17	10409411106509802020270N+1906099	
CC56AC27		02020268N+2010099
CC56AC42		01921161N+2510099
CC56AC52		01921159N+2610099
CC56AC62	06507211209513002021657N+2709099	
CC56AC72		05213902021756N+2802599
CC56AC82	1C4118111	04215402109654N+2901507
CC56AC92		04913602115053N+3000599
CC56A1C2	C94C75121	04711802012451N+3100205
CC56A112		05414402000050N+3200099
CC56A122	1C4104111	04412402000048N+3300008
CC56A132		04913102100046N+3400099
CC56A142	C99111111	05410902021145N+3500408
CC56A149	C93104111	03910902122044N+3601599
CC61ACC5	C9C085111	050C9402222043N+3500503

101C-1

PAS FRMAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NBR NBRHHWAAASTQHWHAAASTCHWHAAASTCHWHAAASTQHWHAAASTQHMINMAXB+FMXLATELECLDOL

CC61AC15

CC61AC25

B F

C72094111

05412602223442N+3703599

07016602220040N+3802505

Nt=0

1C1C-2

TABLE 9-2

PAS FRMAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

ABR ABRHHWAAASTQHhWAAASTChhWAAASTChhWAAASTOHhWAAASTQHINMAXB+FMXLATELECLDOLF

CC65FC1C		02123520N+4610099
CC68FCC5	072068411	<u>052</u> 09602222554N+29050C0
CC68FC15		<u>037</u> 10502222853N+3004099
CC68FC25	078067411	<u>038</u> 08602222051N+3103099
CC68FC35		<u>045</u> 07502221650N+3206599
CC68FC45	C94104111	<u>043</u> 10002221848N+3302504
CC68FC55		<u>044</u> 10202019446N+3306099
CC68FC65	C72085111	<u>047</u> 12002017045N+3500506
CC68FC75		<u>050</u> 07802016043N+3600299
CC68FC85	C9CC78111	<u>038</u> 07402122242N+3700507
CC68FC95		<u>058</u> 09502123040N+3806599
CC68F1C5	C78C85112	<u>056</u> 11302023239N+3907599
CC68F115		02222837N+3910099
CC69FCC5		02019670N+1710099
CC69FC15	C9C094411	<u>033</u> 09102014069N+19010C8
CC69FC25		<u>032</u> 05302000068N+2000099
CC69FC35	C7CC65411	<u>034</u> 06402000066N+21000C8
CC69FC45		<u>032</u> 07402000065N+2200099
CC69FC64	C78085111	<u>030</u> 06802000058N+2700006
CC69FC74		<u>030</u> 09502000057N+2800099
CC69FC84	C85085111	<u>028</u> 10002000055N+2900006
CC69FC94		<u>034</u> 08402000054N+3000099
CC69F1C4	C78C85421	<u>030</u> 21602200052N+3100008
CC69F114		<u>032</u> 22002100051N+3200099
CC69F122	C82C90421	<u>028</u> 19501800050N+32000C8
CC69F132		<u>036</u> 14201420242N+3702099
CC69F142	C67072422	<u>086</u> 14001317040N+3800506
CC69F152	C82075432	<u>068</u> 15001211439N+3900299
CC69F162		01222437N+4010099
CC69F172		01422235N+4010099
CC69F182		01222534N+4110099
CC69F19C	C51C49432	<u>053</u> 10001623033N+4209599
CC69F2C0		<u>055</u> 16802223431N+4209599
CC69F21C	C94C90412	<u>064</u> 13202223230N+4308099
CC69F216		<u>050</u> 12702223629N+4407599
CC7CFC1C		<u>072</u> 07821207914802222552N+3208099
CC7CFC2C		02222650N+3310099
CC7CFC3C		<u>100</u> 15702223048N+3309599
CC7CFC33	C63C55422	<u>079</u> 16302223048N+3409099
CC7CFC43		<u>074</u> 13902222746N+3504099
CC70FC53	C78078432	<u>087</u> 22202222945N+3506599
CC7CFC63		<u>058</u> 14302222643N+3607099
CC7CFC73	C75C67431	<u>044</u> 22802223542N+3702005
CC70FC83		<u>063</u> 18602200040N+3800099
CC7CFC93	C67061411	<u>098</u> 18302221539N+3904099
CC70F1C3		<u>110</u> 18802221937N+4001099
CC70F113		<u>055</u> 05543214221402223435N+4109599
CC70F123		<u>065</u> 22802223234N+4108599
CC70F133	C94C90431	<u>043</u> 23002223032N+4201007
CC70F143		<u>049</u> 23502223231N+4303099

Note: Underlined Drain values indicate reading made in shadow area.

1G1C-2

PAS FRPAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NBR NBRWAAASTGHWAAASTGHWAAASTGHWAAASTGHWAAASTGHWAAASTGMINMAXB+FMXLATELECLDOLF

CC7CF153	085070431	05211402223829N+4406099
CC7CF161		06515402223827N+4507099
AC71FCC5		021000405-3100099
CC71FCC5	085090111	03209302010059N+2500105
CC71FC15		03209302020658N+2600299
CC71FC25	C94104111	03507502000056N+2700008
CC71FC35		03507502000055N+2800099
CC71FC45	C99C94111	03506602000053N+2900006
CC71FC55		03810002000052N+3000099
CC71FC65	C94104111	04810702018450N+3100205
CC71FC75		04612702020249N+3200599
CC71FC85	C63C85112	05815001819347N+3301505
CC71FC95		08814501817046N+3401099
CC71F106	C59C59412	08811401500044N+3500099
CC71F116		08811501200043N+3600099
CC71F126	C63C63412	08015401200041N+3700099
CC71F136		05615001200040N+3800099
CC71F146	C94C94111	02810501200039N+3900099
CC71F156		03014601200037N+4000099
CC71F163	C94104111	04413801200036N+4100008
CC84FCC5	C94C85421	04020202319954N+2900405
CC84FC15		03007502120853N+3001099
CC84FC25	C75C85421	037C9902021051N+3102507
CC84FC35		04311802021750N+3204099
CC84FC45C75078421		05610002022048N+3306099
CC84FC55		07811802022346N+3409599
CC84FC65	C72C82421	04012002021845N+3505006
CC84FC75		04615402022643N+3505099
CC84FC85	C94C99111	05614002022242N+3602008
CC84FC95		05010802022940N+3701599
CC84F105	104090111	05211702022039N+3802599
CC84F115		08414202022037N+3909599
CC84F125		02022535N+4010099
CC84F135		02021634N+4105099
CC84F14CC72085412		10216801920233N+4105099
CC84F150		06011602022931N+4205099
CC84F160	C82070112	06410702022830N+4309099
CC84F170		02023128N+4309099
CC84F180		02022626N+4405099
CC84F190		02023025N+4503099
CC84F198	C94111111	05409802022224N+4601010
CC84F200		04210202024422N+4703099
CC84F210078070111		05019202022821N+4802099
CC85FCC5	104078422	03006002000059N+2500000
CC85FC15		03007802000058N+2700099
CC85FC25	C85C94111	03909402012857N+2800100
CC85FC35		02609002021255N+2903099
CC85FC43	C85C82431	03217201919854N+3001500
CC85FC53		04021202020047N+3400299
CC85FC63	C94C85411	03316702019845N+3500200

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PAS FRMAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREAS RES D D D LIM SUN

NER NBRHHAAASTCHHHAAASTQHHAAASTCHHHAAASTQHHAAASTQMINMAXB+FMXLATELECLDGL

CC85FC73		05214202000044N+3600099
CC85FC83	104C94432	062158019C0042N+3700006
CC85FC93		07216801900041N+3700099
CC85F103	C99111431	04021602022039N+3800510
CC85F113		05718701922438N+3906099
CC85F123	C78090431	08817001821236N+4008506
CC85F133		05815401822534N+4107599
CC85F143		08513401822233N+4209899
CC85F144	C82082432	07814601822433N+4209599
CC85F154		04212701823431N+4307099
CC85F164	C72C94432	03815201822830N+4304099
CC85F174		05412601822828N+4406599
CC85F184		01822926N+4509899
CC85F186	C72C72432	09612101822826N+4509799
CC85F196		04911201923425N+4605099
CC85F206	C94104432	06611002023723N+4708099
CC85F216		08412702022221N+4809099
CC85F226		05618801922020N+4905099
CC85F228	C94072432	05218801923220N+4904099
CC86FCC5	C67C85412	03607101819058N+2601004
CC86FC15		03508001820657N+2702599
CC86FC25	C94104112	03807601822655N+2803505
CC86FC35		03610901820554N+2902599
CC86FC45	C99094111	04912001821752N+3005005
CC86FC55		05008001822651N+3107599
CC86FC65		06009401820850N+3208099
CC86FC75	C75104111	04610201921848N+3305599
CC86FC85	C85104111	05615801917447N+3400205
CC86FC95		0431580180C045N+3500099
CC86F105	C94118111	06417701800044N+3600006
CC86F115		03421202022042N+3700299
CC86F125	C82C72432	03720201821241N+3801010
CC86F135		04222202018639N+3900599
CC86F145	C82104431	04519902022938N+4001010
CC86F155		05822201922436N+4102099
CC87FCC5		02020460N+2510099
CC87FC15		02019659N+2610099
CC87FC18	085094111	04808801821259N+2708599
CC87FC28		05011602020657N+2808099
CC87FC38	C85104111	05311402020456N+2907099
CC87FC44		05008402022455N+2905099
CC87FC55	C94094111	04409001822650N+3203599
CC87FC65		04616801922049N+3302599
CC87FC75	104090111	05116601921848N+3401507
CC87FC85		07616202000C46N+3500099
CC87FC95	C82075111	09219401900045N+3600008
CC87FC99		08517001900044N+3600099
CC88FCC5	104C85111	05008202021355N+1905099
CC88FC15		04408801821254N+2107599
CC88FC25	111104111	04812401820652N+2306005

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PAS FRMAREAL RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NR NRWWWAAASTQWWWAAASTQWWWAAASTQWWWAAASTQWWWAAASTQMINMAXD+FMXLATELECLDUL

C101FC63		09417802000041N+3800099
C101FC73	C78C72412	09015802000039N+3900099
C101FC83		09413001419438N+4006099
C101FC93	C63C65432	07012001320236N+4108599
C101F103		01422335N+4210099
C101F113	C99C94431	03220201222433N+4307599
C101F123		09023201622632N+4408599
C101F133	C78C78432	06823001823630N+4408599
C101F143		06421501923428N+4509599
C101F156	078078111	05210802023226N+4709099
C101F166		04807802023425N+4808599
A1C3FC05		02100039S-3400099
C115FC05	C72C85422	03609002021250N+3206099
C115FC15		03010601821249N+3405099
C115FC25	10410411	03809301821547N+3505599
C115FC35		03409801821446N+3608505
C115FC45	C94C94111	03212801822444N+3703599
C115FC55		03011601600043N+3800099
C115FC65		01800041N+3900099
C115FC69		01821741N+3906099
C116FC05	C85C90411	07714001500043N+3700008
C116FC15		03011001412842N+3800159
C116FC25	C85078121	05014401419040N+3902011
C116FC35		06808201422038N+4009899
C116FC45		01421737N+4110099
C116FC55		01222235N+4210099
C116FC65		01422433N+4210099
C116FC75		01322632N+4310099
C116FC85		01322630N+4410099
C116FC95		01322428N+4510099
C116F105		01322227N+4610099
C116F115C82C85411		07008801322425N+4709599
C116F125		07510601322823N+4709599
C116F135	072070422	06410001623422N+4809099
C116F145		02023820N+4905099
C116F155C72085412		10322902022618N+5001599
C116F165		11316502023617N+5106099
C116F175		02022515N+5206099
C117FC05C65C67431		05223002022051N+3208502
C117FC15		04822802022350N+3302599
C117FC25	C63C61432	04223202022848N+3401503
C117FC35		05016302022247N+3500799
C117FC45		07018802022045N+3600210
C117FC55		05517602022444N+3707099
C117FC65	C61060431	04815602021242N+3800510
C117FC75		10014601520641N+3907599
C117FC85		06013501421039N+4008599
C117FC95		04415001422437N+4107599
C117F105	C72C72412	04619301422636N+4208099
C117F115		03721701423034N+4304099

ICIC-2

PAS FRMAREAL RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NBR NBRHHWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQMINMAXB+FMXLATELECLDUL

C117F125	C59070431	03022401422633N+4404510
C117F135		03822701622631N+4500899
C117F145	C65C65431	04223602022530N+4601508
C117F155		05523302023028N+4702099
C117F165	C67067111	04813402023027N+4802010
C118FC05		01919175N+1310099
C118FC15		07507543105620002017274N+1509599
C118FC25		02019073N+1610099
C118FC35		02019271N+1710099
C118FC45		02020270N+1810099
C118FC55		02022064N+2210099
C118FC65		03105202021163N+2409099
C118FC75	C67072212	032C6702121461N+2507599
C118FC85		03408502121060N+2606099
C118FC95	104094111	03610302020059N+2707099
C118F105		09811802122257N+2809599
C118F115		08610602121655N+2909599
C118F118	C57067112	08612002121755N+2909899
C118F128		066C9502121853N+3109899
C118F138		06707211207811802023152N+3209599
C118F148		04113902000050N+3300099
C118F158	C94078111	05614402000049N+3400007
C118F168		08016501900047N+3500099
C118F178	111118111	12017002100046N+3600009
C118F188		09016802100044N+3700099
C118F198C67072111		05612601600043N+3800099
C131FC05C94078412		04811502122255N+2908599
C131FC15		040C9402019854N+3000299
C131FC25	111094111	04408602017252N+3205008
C131FC35		04611602000050N+3300099
C131FC44	118125411	04007802000049N+3300008
C133FC05	C94C99111	04211002019253N+3000306
C133FC15		03611002021052N+3100399
C133FC25	C82C75431	04811302021750N+3205510
C133FC35		04716402020448N+3300399
C133FC45	C94C99411	03817702000047N+3500010
C133FC55		04120002022645N+3600599
C133FC65	C82085211	05022002013444N+3704510
C133FC75		08418002022542N+3808599
C133FC85		02000040N+3900099
C133FC95		01500039N+4000099
C133F105	C7C061211	08814701300037N+4100010
C133F115		03622501321835N+4200599
C133F125	C78C85431	03122401300034N+4300010
C133F135		03020001400032N+4400099
C133F145	C67C63431	03623402200031N+4500008
C133F155		04823502023529N+4602599
C133F163	C67C78431	04215402024028N+4703502
C134FC05	C78070212	07209402020052N+3109004
C134FC15		06313002000051N+3300099

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PAS FRPAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NBR NBRHWHAAASTQHWHAAASTQHWHAAASTQHWHAAASTQHWHAAASTQMINMAXB+FMXLATELECLDOL

C134FC25	085094112	07816102000049N+3400010
C134FC35		05819002000048N+3500099
CC65AC12		02023420N+4603099
LC68ACC5	094085121	05911402123054N+2906599
CC68AC15		05610602121053N+3005099
LC68AC25	C78065411	04111602122851N+3102007
CC68AC35		04708802022050N+3205099
CC68AC45	C65070112	06311002022348N+3309099
CC68AC55		05812202022247N+3401599
CC68AC65	C78094111	04311702019445N+3500305
CC68AC75		04810502020044N+3601099
CC68AC85	C99118111	04408902121042N+3701005
CC68AC95		05513002023741N+3807099
CC68A105	C94094112	04710002023039N+3906099
CC68A115		06410402022438N+3909999
CC69ACC5		02120071N+1710099
CC69AC15	C78078412	06508702121670N+1902007
CC69AC25		03707002100069N+2000099
CC69AC35	C67075421	04106902100067N+2100007
CC69AC45		03707502100066N+2200099
CC69AC62	C67075411	04508002100059N+2500002
CC69AC72		03607402100058N+2600099
CC69AC82	C72082411	03410802100057N+2700007
CC69AC92		03509502100055N+2800099
CC69A102	104118111	03419202100054N+2900007
CC69A112		04222202100052N+3000099
CC69A122	C67078421	04221602100051N+3100005
CC69A133		06013001522242N+3601099
CC69A143	063067411	06415401419441N+3700599
CC69A153		06016001300039N+3800099
CC69A163C72072111		03018201317838N+3903399
CC69A173		01322236N+4010099
CC69A183		01322835N+4110099
CC69A195	065072432	08612701324233N+4209099
CC69A205		05415402024231N+4309599
CC69A215	C72078112	08013802024230N+4305007
CC70ACC5		02023052N+3010099
CC70CAC15		02022851N+3110099
CC70CAC16		06507511208714001822051N+3106599
CC70AC26		01923349N+3209899
CC70CAC36		01822048N+3309899
CC70CAC38	C72065412	09212201823447N+3309099
CC70CAC48		08215001823246N+3404599
CC70CAC58	C55063432	08018501923444N+3508099
CC70CAC68		06412201922743N+3607099
CC70CAC78	C85072433	04817001923341N+3701006
CC70CAC88		07016402000040N+3700099
CC70CAC98		02021038N+3803099
CC70A104	C63057412	10016802021337N+3904008
CC70A114		11017201823236N+4009899

1C1C-2

PAS FRPAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NBR NBRHHAAASTQHWWAAASTCHWWAAASTCHWWAAASTQHWWAAASTQMINMAXB+FMAXLATELECLUCLU

CC7CA124		14517502022834N+4009999
CC7CA130	C63C59431	06820201821233N+4104006
CC7CA140		05017501823532N+4201099
CC70A150	C94C82431	04217802023030N+4301006
CC7CA160		07413001824229N+4308599
AC71ACC5		02000C38S-3200099
CC71ACC5	C72C78411	05207201823460N+2502503
CC71AC15		03209401817859N+2600199
CC71AC25	C9CC99111	03810401800057N+2700007
CC71AC35		03809201800056N+2800099
CC71AC45	C75C85111	03809201800054N+2900007
CC71AC55		03615001800053N+3000079
CC71AC65	C85085111	04810501800051N+3100007
CC71AC75		06612601800050N+3200099
CC71AC85	C75082421	05514801820049N+3301507
CC71AC95		06019601920247N+3401099
CC71A105	C78C70421	10219001800046N+3500007
CC71A115		11417401600044N+3600099
CC71A125	C67072411	07615401400043N+3700008
CC71A135		09718501200041N+3800099
CC71A145	C78072411	11016001200033N+4100007
CC71A155		03016001200032N+4200099
CC71A164	C94C82431	05817001500030N+4300009
CC84ACC5	C72072411	04821002021855N+2902502
CC84AC15		03417501921554N+3001099
CC84AC25	C85C99411	035C9401921352N+3101005
CC84AC35		04511001922351N+3204599
CC84AC45	C85078112	04010601921449N+3305005
CC84AC55		07912901921047N+3409899
CC84AC65	C99082411	07312501822146N+3507508
CC84AC75		04613201923544N+3502099
CC84AC85	C094094111	05814201923043N+3601508
CC84AC95		04617202022441N+3702599
CC84A105	104104111	04014502021040N+3802099
CC84A115		06013501820038N+3901099
CC84A125		01921436N+4010099
CC84A135		01921835N+4110099
CC84A145		01920633N+4107599
CC84A149	104094111	09211401921233N+4207099
CC84A159		06212401922331N+4306099
CC84A169		01923629N+4310099
CC84A179		01923128N+4409999
CC84A189		02024426N+4507599
CC84A199		01824025N+4605099
CC84A203	C78082412	09011602022024N+4601599
CC84A213		06015802014522N+4703099
CC85AC05	104C94412	03508602019060N+2501502
CC85AC15		03407602000059N+2600099
CC85AC25	C94C85412	032C8702000058N+2700005
CC85AC35		03610302017456N+2800599

ICIC-2

PAS FRMAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NBR NBRHHWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQHMINMAXB+FHAXLATELECLDUL

CC85AC45	1C4094412	03612002020655N+2902005
CC85AC55		05021802020647N+3400599
CC85AC65	C94C90431	04518502000046N+3500004
CC85AC75		05119202000044N+3600099
CC85AC85	C78072732	06417301900042N+3700099
CC85AC95		05318102000041N+3700098
CC85A1C5	C94111111	04922101900039N+3800010
CC85A115		05223001923238N+3901099
CC85A125		<u>078082412</u> 09719602023036N+4004099
CC85A135		07816202023134N+4107599
CC85A145		08115102023833N+4108599
CC85A15C094078422		06916701923432N+4208599
CC85A160		05914301924330N+4307599
CC85A17C	C78085431	04622502024229N+4304510
CC85A18C		08316402023927N+4408099
CC85A190		01924325N+4509599
CC85A194	C85104112	09915602024625N+4508099
CC85A2C4		05915002024323N+4605099
CC85A214	C85C94422	08515802024522N+4707015
CC85A224		10814402024220N+4809599
CC86ACC5	C72C67412	04007502019359N+2603099
CC86AC15		03610602023258N+2701599
CC86AC25	C85078412	03614702023056N+2802006
CC86AC35		04209302023555N+2901099
CC86AC45	111118111	05013002023253N+3001006
CC86AC55		05013202022852N+3106099
CC86AC65	111C94111	05013702023251N+3207599
CC86AC75		05410402023249N+3308599
CC86AC85	104118111	06812801822048N+3402006
CC86AC95		06518801816246N+3500599
CC86A1C5	118118111	10016201800045N+3600010
CC86A115		05815001922843N+3700399
CC86A125	C94C99431	03520901921642N+3700106
CC86A135		04221001923840N+3800599
CC86A145	C67C67431	04824002021839N+3900208
CC86A155		08223602024237N+4099999
CC87ACC5078075112		06309501821661N+2407099
CC87AC15		01922760N+2510099
CC87AC25	C72078112	06910602022859N+2609099
CC87AC35		04610301923257N+2708599
CC87AC44	1C4118111	05810601922456N+2806505
CC87AC55		05010001821451N+3103099
CC87AC65	C99111111	05613402023050N+3303006
CC87AC75		06017602022448N+3402599
CC87AC85	C85104111	07015002023047N+3501005
CC87AC95		05619602112945N+3601099
CC88ACC5	C94085121	06510802024056N+2807099
CC88AC15		04811802023255N+2904599
CC88AC25	C94078121	05611002023553N+3004006
CC88AC35		06213802024052N+3206099

FAS FRMAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES.D D D LIM SUN

NRB NBRHHHAAAATQHWWAAASTCWWHAAAATCWWHAAAATQWWHAAAATQMINMAXB+FMXLATELECLDOL

CC8BAC45	C9C085121	06218002023550N+3304007
CC8BAC55		05714802024049N+3404099
CC8BAC65	C99C90111	05013002023647N+3502507
CC8BAC75		06412502024046N+3603099
CC8BAC85	118C94411	07012202222744N+3702007
CC8BAC95		02017033N+4200399
CC8BA1C5		02116231N+4300399
CC8BA1C7	078C94412	14816802218230N+4400599
CC8BA117		08621402200030N+4400099
CC93ACC5	C78090112	07215802022842N+3706007
CC93AC15		06414202124241N+3803099
CC93AC25	C85C94111	06516902124039N+3905008
CC93AC35		09914702023937N+4006099
CC98ACC5	104C94411	04211802022055N+2902503
CC98AC15		05014802000054N+3000099
CC98AC25	C85C94431	03821602000052N+3100099
CC98AC35		02015851N+3201599
CC98AC43		02020649N+3305599
C1CCACC5	118104111	C4415802217754N+2900103
C1CCAC15		03610202020553N+3000299
C1CCAC25	104111111	03911202022051N+3100505
C1CCAC35		C3413402020649N+3200299
C1CCAC45	C59C90212	03816002023448N+3304099
C1CCAC55		04613602023246N+3407099
C1COAC65	C9CC82432	05817602023245N+3506599
C1CCAC75		04813802023643N+3600099
C1CCAC85	C7C078121	04612001822841N+3703008
C1CCAC95		04412401822340N+3802099
C1CCA1C5	C85C94211	04313001821438N+3900510
C1CCA115		04012001620937N+4000499
C1CCA125	C94094121	C7414401821835N+4105008
C1CCA135		10213401721433N+4207599
C1CCA145	C85082111	08010601621232N+4309099
C1CCA155		01221030N+4410099
C1CCA165		10410441107317301221028N+4509599
C1CCA175		01222027N+4510099
C1CCA185	118111211	05810401520325N+4608099
C1COA195		06414001723024N+4707099
C1COA2C5	C78C72212	08216001823222N+4805013
C1CCA215		01822820N+4908099
C1COA221	C78C85212	C9317201823219N+5008599
C1C1ACC5	063072431	08011802022651N+3209099
C1C1AC15		01621650N+3310099
C1C1AC25	C85C72433	03621201418648N+3401007
C1C1AC35		04322401622047N+3502099
C1C1AC45		10817701822445N+3609599
C1C1AC48	C82C70411	07814801820844N+3604008
C1C1AC58		05816401621643N+3703099
C1C1AC68	C7CC72411	07413001200041N+3800009
C1C1AC78		07013001200040N+3900099

TOP SECRET

ICIC-2

PAS FRMAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NR BRWWAAASTCWWAAASTCWWAAASTCWWAAASTCWWAAASTQWWAAASTQMINMAXB+FMAXLATELECLDOL

C1C1AC88	C94C85433	05018001319238N+4001510
C1C1AC98		06114001421436N+4104099
C1C1A108		01322635N+4210099
C1C1A114	085072432	07813001322834N+4209099
C1C1A124		04021201421632N+4301599
C1C1A134		01423030N+4410099
C1C1A137	C72078422	07416801523430N+4409099
C1C1A147		08215502023028N+4507599
C1C1A157	C61070412	08214602023125N+4708099
C1C1A165		06010401923525N+4707099
A1C3ACC5		016000385-3800099
C115ACC5	C85078411	04012002021451N+3205007
C115AC15		03610001822050N+3406099
C115AC25	C78075211	04210501821448N+3504008
C115AC35		04008802023046N+3607099
C115AC45	C85C94111	03512001822045N+3705099
C115AC55		03010801822042N+3801099
C115AC65		01800041N+3900099
C115AC69		01815041N+3900599
C116ACC5	C94C99432	09216001400044N+3700005
C116AC15		05615501200043N+3800059
C116AC25	C94C94412	04511601119841N+3902010
C116AC35		07414401120139N+4009599
C116AC46	085094422	08012201222437N+4109699
C116AC56		01222036N+4210099
C116AC66		01121834N+4310099
C116AC76		01122432N+4310099
C116AC86		01222031N+4410099
C116AC96		01221829N+4510099
C116A106		01321927N+4610099
C116A116		07208241208812901222425N+4709599
C116A126		06612501222224N+4808599
C116A136	C9CC90432	07618001623422N+4908099
L116A146		08217001923020N+4905099
C116A156085094411		07017001922019N+5005099
C116A166		01723017N+5104099
C116A171		01722516N+5104599
C117ACC5	078094422	09313101921852N+3109599
C117AC15		04122902022451N+3205099
C117AC25	C63072412	04722602022249N+3304003
C117AC35		05523101920547N+3400599
C117AC45	C94C99431	05615801221046N+3601007
C117AC55		04014901219544N+3705099
C117AC65	C75C85432	03020501322243N+3802007
C117AC75		03513801221041N+3900599
C117AC85		08515001216839N+4099999
C117AC9C	C72075412	08019201220639N+4009099
C117A1CC		04117301222837N+4104599
C117A11C	078072411	05716001222735N+4206599
C117A12C		05121901222234N+4303099

101C-2

PAS FRMAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NBR NBRHHWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQHWWAAASTQMINMAXB+FMXLATELECLDUL

C117A13C	C85094411	03922901322732N+4403508
C117A14C		04022201321830N+4501099
C117A15C	C54C75431	03322001322329N+4601508
C117A160		04223001322927N+4705099
C118ACC5		01615676N+1210099
C118AC15		01818274N+1401599
C118AC21		08506543305620601818274N+1401599
C118AC41		01917871N+1710099
C118AC51		01921566N+2110099
C118AC61	072063412	07612501420064N+2209099
C118AC71		02003001320263N+2305099
C118AC81134118111		03005202021061N+2405099
C118AC91		04007002021660N+2505099
C118A1C1	C94085111	04012502021858N+2705099
C118A111		01922257N+2810099
C118A121		06706311208213301922055N+2908099
C118A131		06514801922054N+3008599
C118A141	072063112	08613601921852N+3108099
C118A151		07214601920451N+3201599
C118A161	C76C72411	08819601900049N+3300009
C118A171		06018001400048N+3400099
C118A181	C82070411	07217001200046N+3600010
C118A191		05015401317245N+3700399
C131ACC5		02021056N+2901009
C131AC05067C85412		06013402019856N+2908003
C131AC19		05209402000054N+3000099
C131AC29	111118111	04811801919052N+3204006
C131AC39		05314001900051N+3300099
C131AC44	111C94112	04414001900050N+3300008
C133Acc5	C78085111	05013402000054N+3000007
C133AC15		06413801921053N+3100299
C133AC25	C59C85121	06813401920051N+3201510
C133AC35		05413401921049N+3401599
C133AC45	C85C85431	04218002022048N+3500509
C133AC55		03415001924846N+3601099
C133AC65	C85C72431	07021801822644N+3701010
C133AC75		07016201522643N+3809099
C133AC85	C72C67422	07015601420241N+3904008
C133AC95		01420440N+4002099
C133A105		01400038N+4100099
C133A115	C85C75433	05120301222436N+4202007
C133A125		04920401300035N+4300099
C133A135	C90C85433	07219201200033N+4400008
C133A145		07522001200031N+4500099
C133A155	C94C94433	02517601222230N+4601008
C133A16C		04823001423429N+4602099
C134ACC5	078104112	06312001921953N+3006004
C134AC15		07209201820552N+3203099
C134AC25	1C4125111	06018401900050N+3300009
C134AC35		06218702000048N+3400099

1C1C-2

PAS FRPAREA1 RESAREA2 RESAREA3 RESAREA4 RESAREA5 RES D D D LIM SUN

NBR NBRWWWAAASTQWWWAAASTQWWWAAASTQWWWAAASTQWWWAAASTQMINMAXB+FMXLATELECLDCL

C134AC45

104104421

C7014601600047N+3500010

C134AC53

05217801900046N+3600099

E F

N+-0

PA

The diffuse density measurements made by AFSPPL were computer sorted at A/P to permit analysis of the density ranges encountered at the three processing levels. A study of sorting techniques showed that no absolute method was available to separate the density values as the accuracy of the Processing History published by [REDACTED] appears rather low and processing transition phases are not accounted for. The sorting technique selected uses the base fog density values where measurements up to 0.09 density are considered as having received Primary processing, 0.10 to 0.17 as Intermediate and above 0.17 density as Full. The percentage of original negative that was processed at each level, based on the computer sort, is tabulated below with the predicted and reported processing percentages.

<u>Mission</u>	<u>Camera</u>		<u>Primary</u>	<u>Intermediate</u>	<u>Full</u>
1010-1	FWD	Predicted	0	21	79
		Reported	0	13	87
		Computed	0	9	91
1010-1	AFT	Predicted	0	21	79
		Reported	0	19	81
		Computed	0	16	84
1010-2	FWD	Predicted	0	50	50
		Reported	0	16	84
		Computed	0	13	87
1010-2	AFT	Predicted	0	50	50
		Reported	0	23	77
		Computed	0	25	75

The correlation of the reported and computed percentages at the three processing levels is very good for both missions.

~~TOP SECRET~~

The tabulations of density frequency distributions for Missions 1010-1 and 1010-2 are shown in Tables 9-3 through 9-6. The graphical presentation of the density distribution are computer plotted in Figures 9-1 through 9-36.

Analysis of these plots and the associated mean and median density values show that there was a slight reduction in all values as compared with recent missions. AFSPPL reported this same lower density level and added that the resulting values were within the nominal density range.

Table 9-7 shows the distribution of the minimum terrain density measurements that are within and outside of the desired control range of 0.40 to 0.90 density. The percentage of values below 0.40 is greater than usually experienced however it is significant to note that less than 2% of the density values were below 0.30 density. It appears reasonable to control processing at the present range of 0.40 to 0.90 density as the unavoidable spread below 0.40 is apparently at a density level that does not produce a detectable loss in information content.

An extensive study is in process to ascertain the inter-relationship of the conditions of illumination, resulting densities and exposure-processing parameters.

~~TOP SECRET~~

MISSION • ICIC-1 • INSTRUMENT • FWD 2-09-64 DENSITY FREQ 0000

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			L.L.E.		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
0												
0.01												
0.02												
0.03												
0.04												
0.05												
0.06												
0.07												
0.08												
0.09												
0.10												
0.11												
0.12												
0.13												
0.14												
0.15												
0.16												
0.17												
0.18												
0.19												
0.20												
0.21												
0.22												
0.23												
0.24												
0.25												
0.26												
0.27												
0.28												
0.29												
0.30												
0.31												
0.32												
0.33												
0.34												
0.35												
0.36												
0.37												
0.38												
0.39												
0.40												
0.41												
0.42												
0.43												
0.44												
0.45												
0.46												
0.47												
0.48												
0.49												
0.50												
0.51												
0.52												
0.53												
0.54												
0.55												
0.56												
0.57												
0.58												
0.59												
0.60												
0.61												
0.62												
0.63												
0.64												
0.65												
0.66												
0.67												
0.68												
0.69												
0.70												
0.71												
0.72												
0.73												
0.74												
0.75												
0.76												
0.77												
0.78												
0.79												
0.80												
0.81												
0.82												
0.83												
0.84												
0.85												
0.86												
0.87												
0.88												
0.89												
0.90												
0.91												
0.92												
0.93												
0.94												
0.95												
0.96												
0.97												
0.98												
0.99												
1.00												
TOTAL												

TABLE 9-3

MISSICA • 1010-1

• INSTRUMENT • FWD

2-09-64

DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMECIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
C. 51	C	C	0	C	0	0	3	0	0	3	0	0
C. 52	C	C	0	C	0	0		0	0	7	0	0
C. 53	C	C	0	C	0	0		0	0	3	0	0
C. 54	C	C	0	C	0	0		0	0	3	0	0
C. 55	C	C	0	C	0	0		0	0	3	0	0
C. 56	C	C	0	C	0	0		0	0	1	0	0
C. 57	C	C	0	C	0	0		0	0	1	0	0
C. 58	C	C	0	C	0	0		0	0	6	0	0
C. 59	C	C	0	C	0	0		0	0	9	0	0
C. 60	C	C	0	C	0	0		0	0	2	0	0
C. 61	C	C	0	C	0	0		0	0	2	0	0
C. 62	C	C	0	C	0	0		0	0	2	0	0
C. 63	C	C	0	C	0	0		0	0	3	0	0
C. 64	C	C	0	C	0	0		0	0	4	0	0
C. 65	C	C	0	C	0	0		0	0	0	0	0
C. 66	C	C	0	C	0	0		0	0	3	0	0
C. 67	C	C	0	C	0	0		0	0	3	0	0
C. 68	C	C	0	C	0	0		0	0	5	0	0
C. 69	C	C	0	C	0	0		0	0	7	0	0
C. 70	C	C	0	C	0	0		0	0	0	0	0
C. 71	C	C	0	C	0	0		0	0	3	0	0
C. 72	C	C	0	C	0	0		0	0	0	0	0
C. 73	C	C	0	C	0	0		0	0	0	0	0
C. 74	C	C	0	C	0	0		0	0	0	0	0
C. 75	C	C	0	C	0	0		0	0	1	0	0
C. 76	C	C	0	C	0	0		0	0	0	0	0
C. 77	C	C	0	C	0	0		0	0	0	0	0
C. 78	C	C	0	C	0	0		0	0	0	0	0
C. 79	C	C	0	C	0	0		0	0	4	0	0
C. 80	C	C	0	C	0	0		0	0	1	0	0
C. 81	C	C	0	C	0	0		0	0	0	0	0
C. 82	C	C	0	C	0	0		0	0	0	0	0
C. 83	C	C	0	C	0	0		0	0	0	0	0
C. 84	C	C	0	C	0	0		0	0	0	0	0
C. 85	C	C	0	C	0	0		0	0	0	0	0
C. 86	C	C	0	C	0	0		0	0	0	0	0
C. 87	C	C	0	C	0	0		0	0	0	0	0
C. 88	C	C	0	C	0	0		0	0	0	0	0
C. 89	C	C	0	C	0	0		0	0	0	0	0
C. 90	C	C	0	C	0	0		0	0	0	0	0
C. 91	C	C	0	C	0	0		0	0	0	0	0
C. 92	C	C	0	C	0	0		0	0	0	0	0
C. 93	C	C	0	C	0	0		0	0	0	0	0
C. 94	C	C	0	C	0	0		0	0	0	0	0
C. 95	C	C	0	C	0	0		0	0	0	0	0
C. 96	C	C	0	C	0	0		0	0	0	0	0
C. 97	C	C	0	C	0	0		0	0	0	0	0
C. 98	C	C	0	C	0	0		0	0	0	0	0
C. 99	C	C	0	C	0	0		0	0	0	0	0
C. 00	C	C	0	C	0	0		0	0	0	0	0
SUBTOTAL	C	C	0	C	0	0	8	3	0	9	4	0

TABLE 9-3

MISSION • IGIC-1

• INSTRUMENT • FWD

2-09-64

DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
1.01	C	C	0	C	C	0	1	0	0	1	0	0
1.02	C	C	0	C	C	0	1	0	0	1	0	0
1.03	C	C	0	C	C	0	1	0	0	1	0	0
1.04	C	C	0	C	C	0	1	0	0	1	0	0
1.05	C	C	0	C	C	0	1	0	0	1	0	0
1.06	C	C	0	C	C	0	1	0	0	1	0	0
1.07	C	C	0	C	C	0	1	0	0	1	0	0
1.08	C	C	0	C	C	0	1	0	0	1	0	0
1.09	C	C	0	C	C	0	1	0	0	1	0	0
1.10	C	C	0	C	C	0	1	0	0	1	0	0
1.11	C	C	0	C	C	0	1	0	0	1	0	0
1.12	C	C	0	C	C	0	1	0	0	1	0	0
1.13	C	C	0	C	C	0	1	0	0	1	0	0
1.14	C	C	0	C	C	0	1	0	0	1	0	0
1.15	C	C	0	C	C	0	1	0	0	1	0	0
1.16	C	C	0	C	C	0	1	0	0	1	0	0
1.17	C	C	0	C	C	0	1	0	0	1	0	0
1.18	C	C	0	C	C	0	1	0	0	1	0	0
1.19	C	C	0	C	C	0	1	0	0	1	0	0
1.20	C	C	0	C	C	0	1	0	0	1	0	0
1.21	C	C	0	C	C	0	1	0	0	1	0	0
1.22	C	C	0	C	C	0	1	0	0	1	0	0
1.23	C	C	0	C	C	0	1	0	0	1	0	0
1.24	C	C	0	C	C	0	1	0	0	1	0	0
1.25	C	C	0	C	C	0	1	0	0	1	0	0
1.26	C	C	0	C	C	0	1	0	0	1	0	0
1.27	C	C	0	C	C	0	1	0	0	1	0	0
1.28	C	C	0	C	C	0	1	0	0	1	0	0
1.29	C	C	0	C	C	0	1	0	0	1	0	0
1.30	C	C	0	C	C	0	1	0	0	1	0	0
1.31	C	C	0	C	C	0	1	0	0	1	0	0
1.32	C	C	0	C	C	0	1	0	0	1	0	0
1.33	C	C	0	C	C	0	1	0	0	1	0	0
1.34	C	C	0	C	C	0	1	0	0	1	0	0
1.35	C	C	0	C	C	0	1	0	0	1	0	0
1.36	C	C	0	C	C	0	1	0	0	1	0	0
1.37	C	C	0	C	C	0	1	0	0	1	0	0
1.38	C	C	0	C	C	0	1	0	0	1	0	0
1.39	C	C	0	C	C	0	1	0	0	1	0	0
1.40	C	C	0	C	C	0	1	0	0	1	0	0
1.41	C	C	0	C	C	0	1	0	0	1	0	0
1.42	C	C	0	C	C	0	1	0	0	1	0	0
1.43	C	C	0	C	C	0	1	0	0	1	0	0
1.44	C	C	0	C	C	0	1	0	0	1	0	0
1.45	C	C	0	C	C	0	1	0	0	1	0	0
1.46	C	C	0	C	C	0	1	0	0	1	0	0
1.47	C	C	0	C	C	0	1	0	0	1	0	0
1.48	C	C	0	C	C	0	1	0	0	1	0	0
1.49	C	C	0	C	C	0	1	0	0	1	0	0
1.50	C	C	0	C	C	0	1	0	0	1	0	0
SUBTOTAL	C	C	0	C	C	0	4	10	5	4	12	5

TABLE 9-3

MISSION • 1010-1

• INSTRUMENT • FWD

2-09-64

DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
1.51	C	C	0	C	C	0	0	1	1	0	0	1
1.52	C	C	0	C	C	0	0	2	1	0	0	1
1.53	C	C	0	C	C	0	0	1	0	0	0	1
1.54	C	C	0	C	C	0	0	2	0	0	0	1
1.55	C	C	0	C	C	0	0	3	0	0	0	1
1.56	C	C	0	C	C	0	0	4	0	0	0	1
1.57	C	C	0	C	C	0	0	0	0	0	0	1
1.58	C	C	0	C	C	0	0	0	0	0	0	1
1.59	C	C	0	C	C	0	0	0	0	0	0	1
1.60	C	C	0	C	C	0	0	0	0	0	0	1
1.61	C	C	0	C	C	0	0	0	0	0	0	1
1.62	C	C	0	C	C	0	0	0	0	0	0	1
1.63	C	C	0	C	C	0	0	0	0	0	0	1
1.64	C	C	0	C	C	0	0	0	0	0	0	1
1.65	C	C	0	C	C	0	0	0	0	0	0	1
1.66	C	C	0	C	C	0	0	0	0	0	0	1
1.67	C	C	0	C	C	0	0	0	0	0	0	1
1.68	C	C	0	C	C	0	0	0	0	0	0	1
1.69	C	C	0	C	C	0	0	0	0	0	0	1
1.70	C	C	0	C	C	0	0	0	0	0	0	1
1.71	C	C	0	C	C	0	0	0	0	0	0	1
1.72	C	C	0	C	C	0	0	0	0	0	0	1
1.73	C	C	0	C	C	0	0	0	0	0	0	1
1.74	C	C	0	C	C	0	0	0	0	0	0	1
1.75	C	C	0	C	C	0	0	0	0	0	0	1
1.76	C	C	0	C	C	0	0	0	0	0	0	1
1.77	C	C	0	C	C	0	0	0	0	0	0	1
1.78	C	C	0	C	C	0	0	0	0	0	0	1
1.79	C	C	0	C	C	0	0	0	0	0	0	1
1.80	C	C	0	C	C	0	0	0	0	0	0	1
1.81	C	C	0	C	C	0	0	0	0	0	0	1
1.82	C	C	0	C	C	0	0	0	0	0	0	1
1.83	C	C	0	C	C	0	0	0	0	0	0	1
1.84	C	C	0	C	C	0	0	0	0	0	0	1
1.85	C	C	0	C	C	0	0	0	0	0	0	1
1.86	C	C	0	C	C	0	0	0	0	0	0	1
1.87	C	C	0	C	C	0	0	0	0	0	0	1
1.88	C	C	0	C	C	0	0	0	0	0	0	1
1.89	C	C	0	C	C	0	0	0	0	0	0	1
1.90	C	C	0	C	C	0	0	0	0	0	0	1
1.91	C	C	0	C	C	0	0	0	0	0	0	1
1.92	C	C	0	C	C	0	0	0	0	0	0	1
1.93	C	C	0	C	C	0	0	0	0	0	0	1
1.94	C	C	0	C	C	0	0	0	0	0	0	1
1.95	C	C	0	C	C	0	0	0	0	0	0	1
1.96	C	C	0	C	C	0	0	0	0	0	0	1
1.97	C	C	0	C	C	0	0	0	0	0	0	1
1.98	C	C	0	C	C	0	0	0	0	0	0	1
1.99	C	C	0	C	C	0	0	0	0	0	0	1
2.00	C	C	0	C	C	0	0	0	0	0	0	1
SUBTOTAL												

TABLE 9-3

MISSION • 1010-1

• INSTRUMENT • FWD

2-09-64

DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.01	C	C	0	C	0	0	0	0	0	0	0	0
2.02	C	C	0	C	0	0	0	0	0	0	0	0
2.03	C	C	0	C	0	0	0	0	0	0	0	0
2.04	C	C	0	C	0	0	0	0	0	0	0	0
2.05	C	C	0	C	0	0	0	0	0	0	0	0
2.06	C	C	0	C	0	0	0	0	0	0	0	0
2.07	C	C	0	C	0	0	0	0	0	0	0	0
2.08	C	C	0	C	0	0	0	0	0	0	0	0
2.09	C	C	0	C	0	0	0	0	0	0	0	0
2.10	C	C	0	C	0	0	0	0	0	0	0	0
2.11	C	C	0	C	0	0	0	0	0	0	0	0
2.12	C	C	0	C	0	0	0	0	0	0	0	0
2.13	C	C	0	C	0	0	0	0	0	0	0	0
2.14	C	C	0	C	0	0	0	0	0	0	0	0
2.15	C	C	0	C	0	0	0	0	0	0	0	0
2.16	C	C	0	C	0	0	0	0	0	0	0	0
2.17	C	C	0	C	0	0	0	0	0	0	0	0
2.18	C	C	0	C	0	0	0	0	0	0	0	0
2.19	C	C	0	C	0	0	0	0	0	0	0	0
2.20	C	C	0	C	0	0	0	0	0	0	0	0
2.21	C	C	0	C	0	0	0	0	0	0	0	0
2.22	C	C	0	C	0	0	0	0	0	0	0	0
2.23	C	C	0	C	0	0	0	0	0	0	0	0
2.24	C	C	0	C	0	0	0	0	0	0	0	0
2.25	C	C	0	C	0	0	0	0	0	0	0	0
2.26	C	C	0	C	0	0	0	0	0	0	0	0
2.27	C	C	0	C	0	0	0	0	0	0	0	0
2.28	C	C	0	C	0	0	0	0	0	0	0	0
2.29	C	C	0	C	0	0	0	0	0	0	0	0
2.30	C	C	0	C	0	0	0	0	0	0	0	0
2.31	C	C	0	C	0	0	0	0	0	0	0	0
2.32	C	C	0	C	0	0	0	0	0	0	0	0
2.33	C	C	0	C	0	0	0	0	0	0	0	0
2.34	C	C	0	C	0	0	0	0	0	0	0	0
2.35	C	C	0	C	0	0	0	0	0	0	0	0
2.36	C	C	0	C	0	0	0	0	0	0	0	0
2.37	C	C	0	C	0	0	0	0	0	0	0	0
2.38	C	C	0	C	0	0	0	0	0	0	0	0
2.39	C	C	0	C	0	0	0	0	0	0	0	0
2.40	C	C	0	C	0	0	0	0	0	0	0	0
2.41	C	C	0	C	0	0	0	0	0	0	0	0
2.42	C	C	0	C	0	0	0	0	0	0	0	0
2.43	C	C	0	C	0	0	0	0	0	0	0	0
2.44	C	C	0	C	0	0	0	0	0	0	0	0
2.45	C	C	0	C	0	0	0	0	0	0	0	0
2.46	C	C	0	C	0	0	0	0	0	0	0	0
2.47	C	C	0	C	0	0	0	0	0	0	0	0
2.48	C	C	0	C	0	0	0	0	0	0	0	0
2.49	C	C	0	C	0	0	0	0	0	0	0	0
2.50	C	C	0	C	0	0	0	0	0	0	0	0
SUBTOTAL												

TABLE 9-3

~~TOP SECRET~~

MISSION • 1010-1 • INSTRUMENT • FWD 2-09-64 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.51	C	C	0	C	0	0	0	0	0	0	0	0
2.52	C	C	0	C	0	0	0	0	0	0	0	0
2.53	C	C	0	C	0	0	0	0	0	0	0	0
2.54	C	C	0	C	0	0	0	0	0	0	0	0
2.55	C	C	0	C	0	0	0	0	0	0	0	0
2.56	C	C	0	C	0	0	0	0	0	0	0	0
2.57	C	C	0	C	0	0	0	0	0	0	0	0
2.58	C	C	0	C	0	0	0	0	0	0	0	0
2.59	C	C	0	C	0	0	0	0	0	0	0	0
2.60	C	C	0	C	0	0	0	0	0	0	0	0
2.61	C	C	0	C	0	0	0	0	0	0	0	0
2.62	C	C	0	C	0	0	0	0	0	0	0	0
2.63	C	C	0	C	0	0	0	0	0	0	0	0
2.64	C	C	0	C	0	0	0	0	0	0	0	0
2.65	C	C	0	C	0	0	0	0	0	0	0	0
2.66	C	C	0	C	0	0	0	0	0	0	0	0
2.67	C	C	0	C	0	0	0	0	0	0	0	0
2.68	C	C	0	C	0	0	0	0	0	0	0	0
2.69	C	C	0	C	0	0	0	0	0	0	0	0
2.70	C	C	0	C	0	0	0	0	0	0	0	0
SUBTOTAL	C	C	0	C	0	0	C	0	0	0	C	0
TOTAL	C	C	0	23	23	25	224	224	218	247	247	243

MISSION 1010-1		INSTR - FWD		2-09-64		PROCESSING AND EXPOSURE ANAL			
PROCESS LEVEL	SAMPLE SIZE	UNCER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED				
PRIMARY	C	C PC	0 PC	0 PC	0 PC				
INTERMEDIATE	23	C PC	35 PC	65 PC	0 PC	0 F			
FULL	224	2C PC	0 PC	76 PC	4 PC	0 P			
ALL LEVELS	247	18 PC	3 PC	75 PC	4 PC	0 P			
PROCESS LEVEL	BASE + FCG	UNCER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSE			
PRIMARY	0.01-C.19	C.01-C.13	0.14-0.39	0.40-0.90	-----	0.91 AND			
INTERMED	0.10-C.17	C.01-C.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AND			
FULL	0.18 AND UP	0.01-0.39	-----	0.40-0.90	0.91-1.69	1.70 AND			

TABLE 9-3

~~TOP SECRET~~

MISSICA • 1010-1 • INSTR • FND • 2-09-64 PLOT OF D MIN • TERRAIN • PROCESSING • INTERMEDIATE
ARITH MEAN • 0.45 • MEDIAN • 0.41 • STD DEV • 0.13 • RANGE • 0.28 TO 0.86 WITH 23 SAMPLES

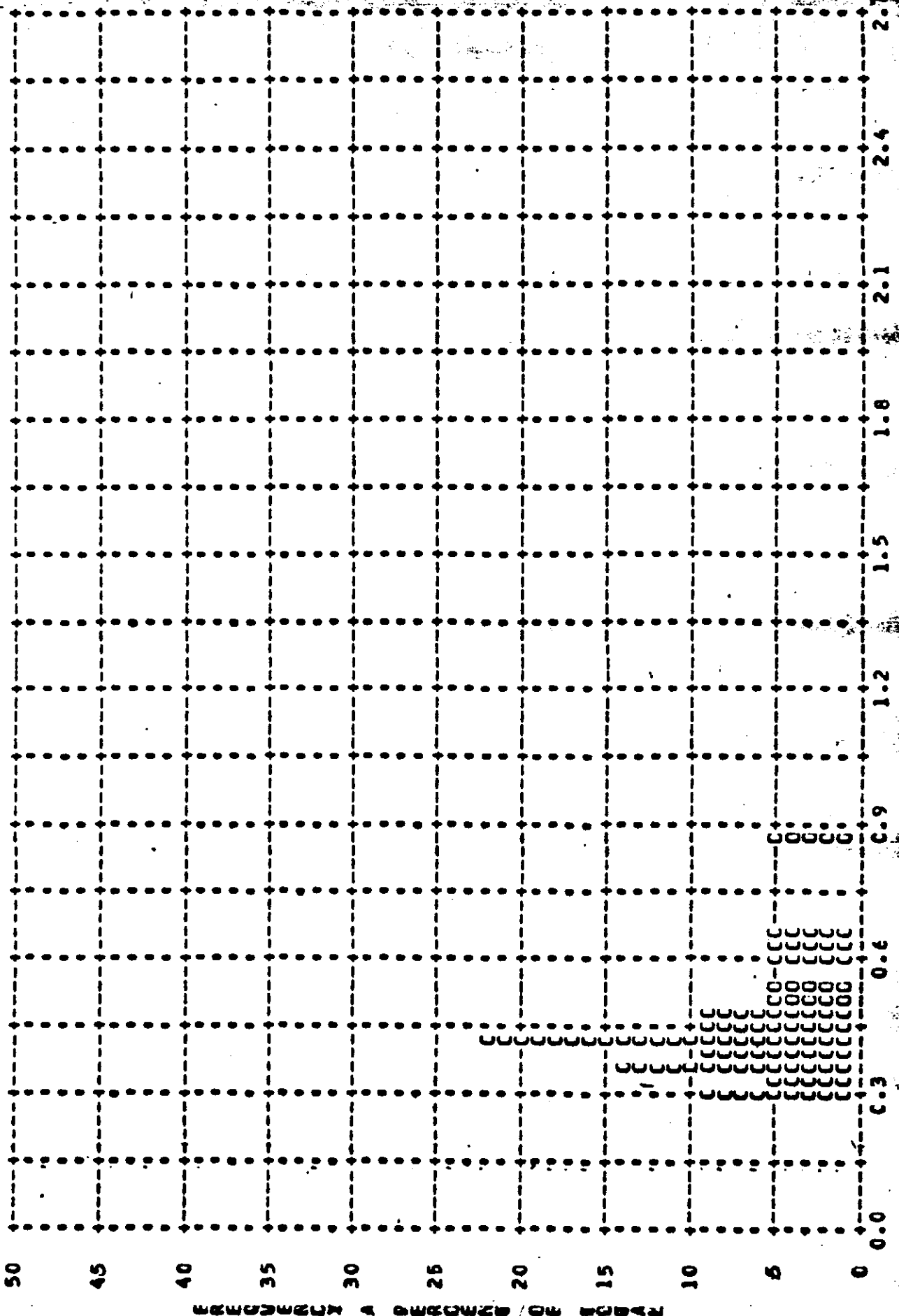


FIGURE 9-1

MISBICA • ICIC-1 • INSTR • FAD • 2-09-64 PLOT OF D MAX • TERRAIN • PROCESSING • INTERMEDIATE
WITH MEAN • 1.35 • MEDIAN • 1.42 • STD DEV • 0.48 • RANGE • 0.43 TO 2.18 WITH 23 SAMPLES

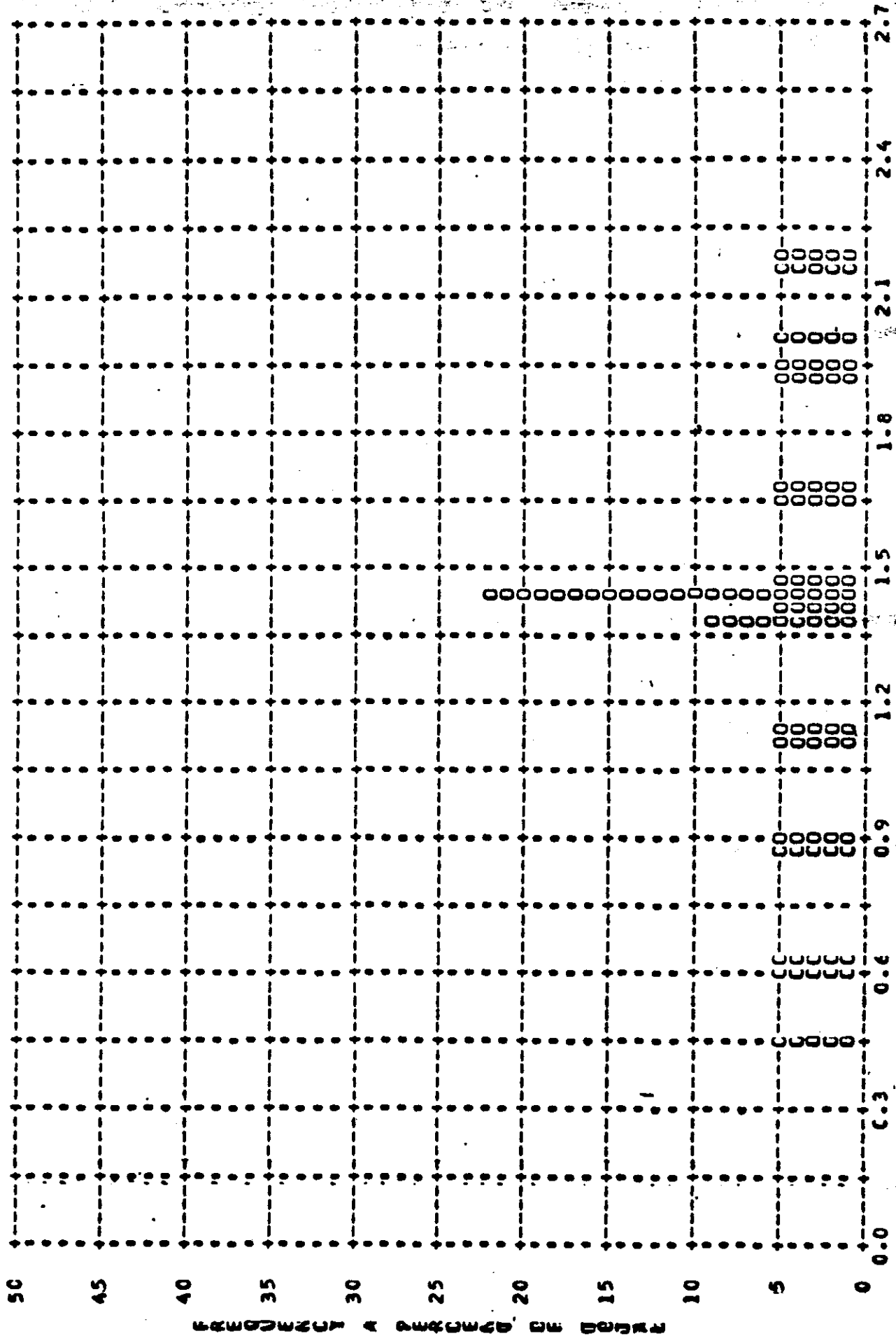


FIGURE 9-2

MISSION • 1010-1 • INSTR • FAD • 2-09-64 PLOT OF D MAX • CLOUD • PROCESSING • INTERMEDIATE
WITH MEAN • 2.06 • MEDIAN • 2.06 • STD DEV • 0.15 • RANGE • 1.76 TO 2.39 WITH 25 SAMPLES

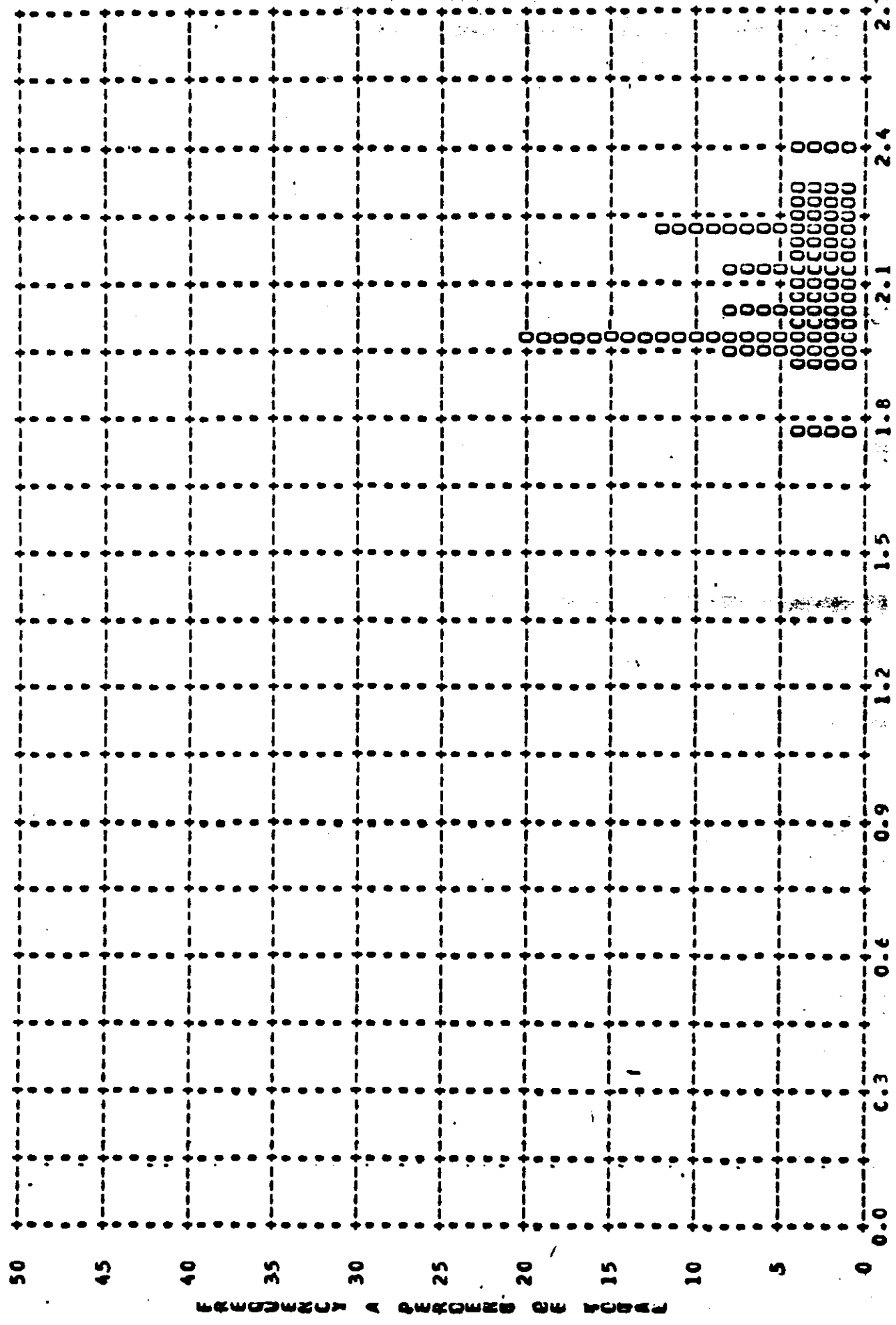


FIGURE 9-3

MISSION • ICIC-1 • INSTR • FAD • 2-09-64 PLOT OF D MIN • TERRAIN • PROCESSING • FULL
ARITH MEAN • 0.52 • MECHAN • C.48 • STD DEV • 0.17 • RANGE • 0.28 TO 1.14 WITH 224 SAMPLES

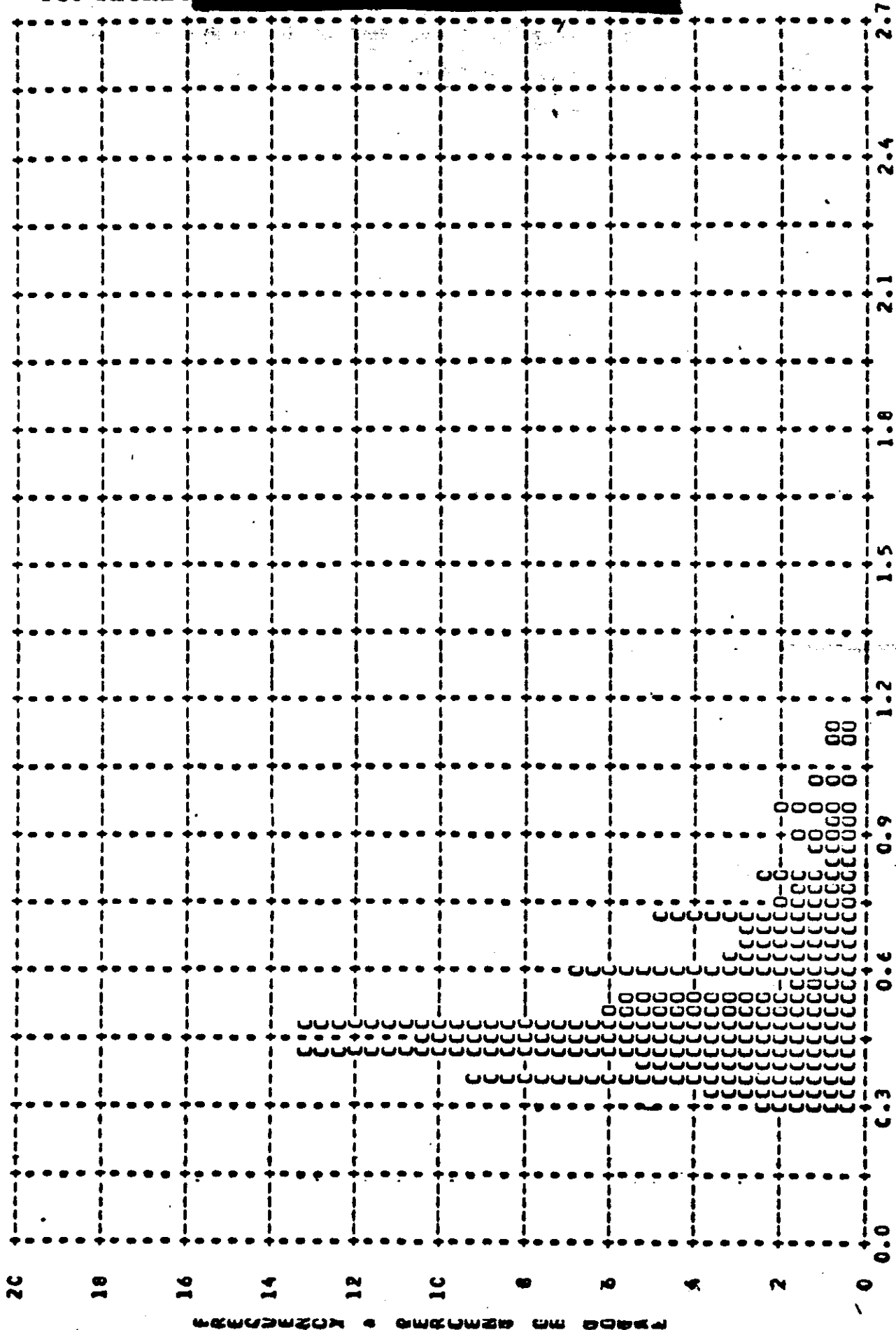


FIGURE 9-4

MISSION • IOIC-1 • INSTR • FWD • 2-05-64 PLOT OF D MAX • TERRAIN • PROCESSING • FULL
ARITH MEAN • 1.38 • MEDIAN • 1.30 • STD DEV • 0.38 • RANGE • 0.62 TO 2.32 WITH 224 SAMPLES

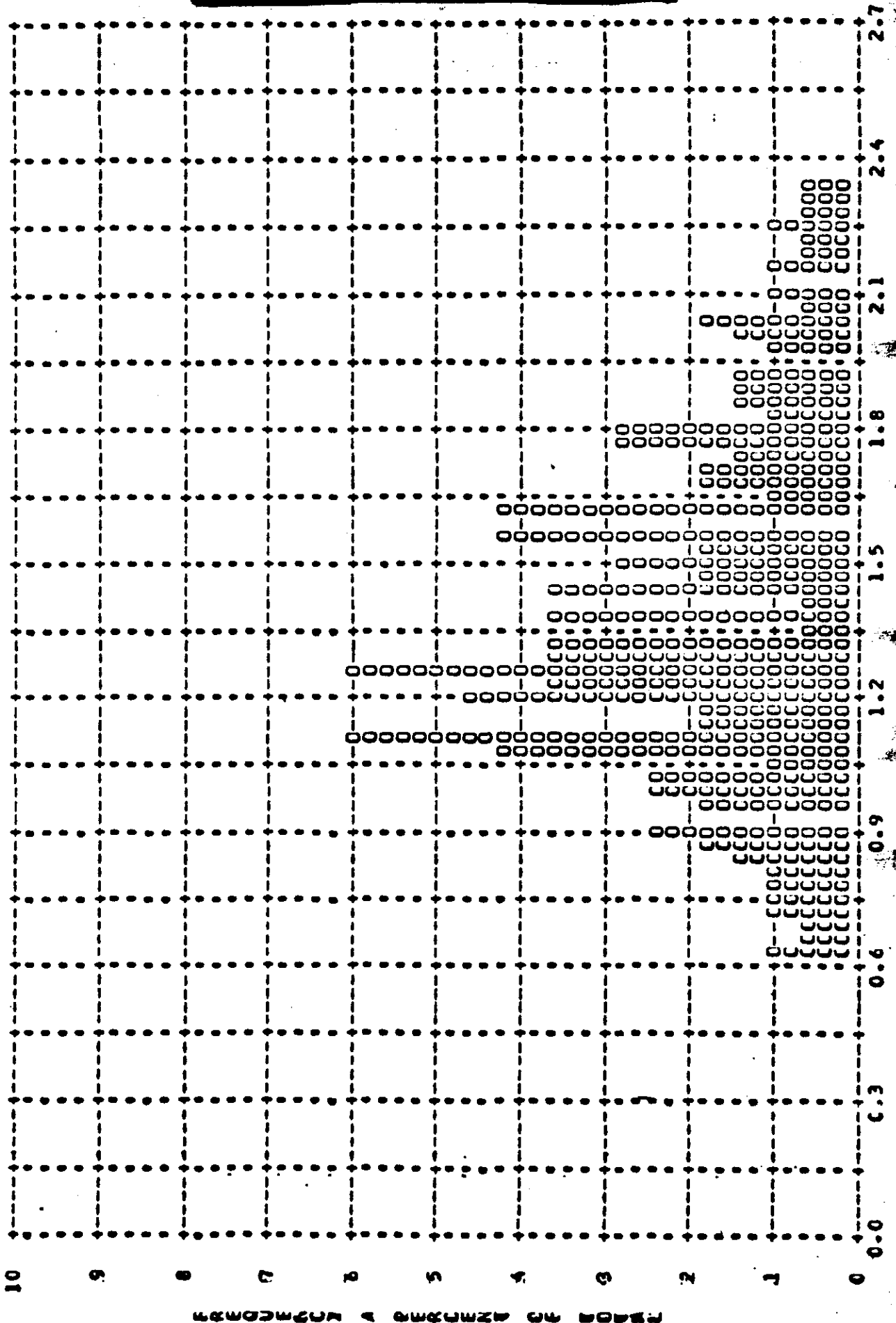


FIGURE 9-5

MISSION • IC10-1 • INSTR • FND • 2-09-64 PLCT OF D MAX • CLOUD • PROCESSING • FULL
WRITH PEAN • 2.17 • PECIAN • 2.20 • STD DEV • 0.21 • RANGE • 1.11 TO 2.42 WITH 218 SAMPLES

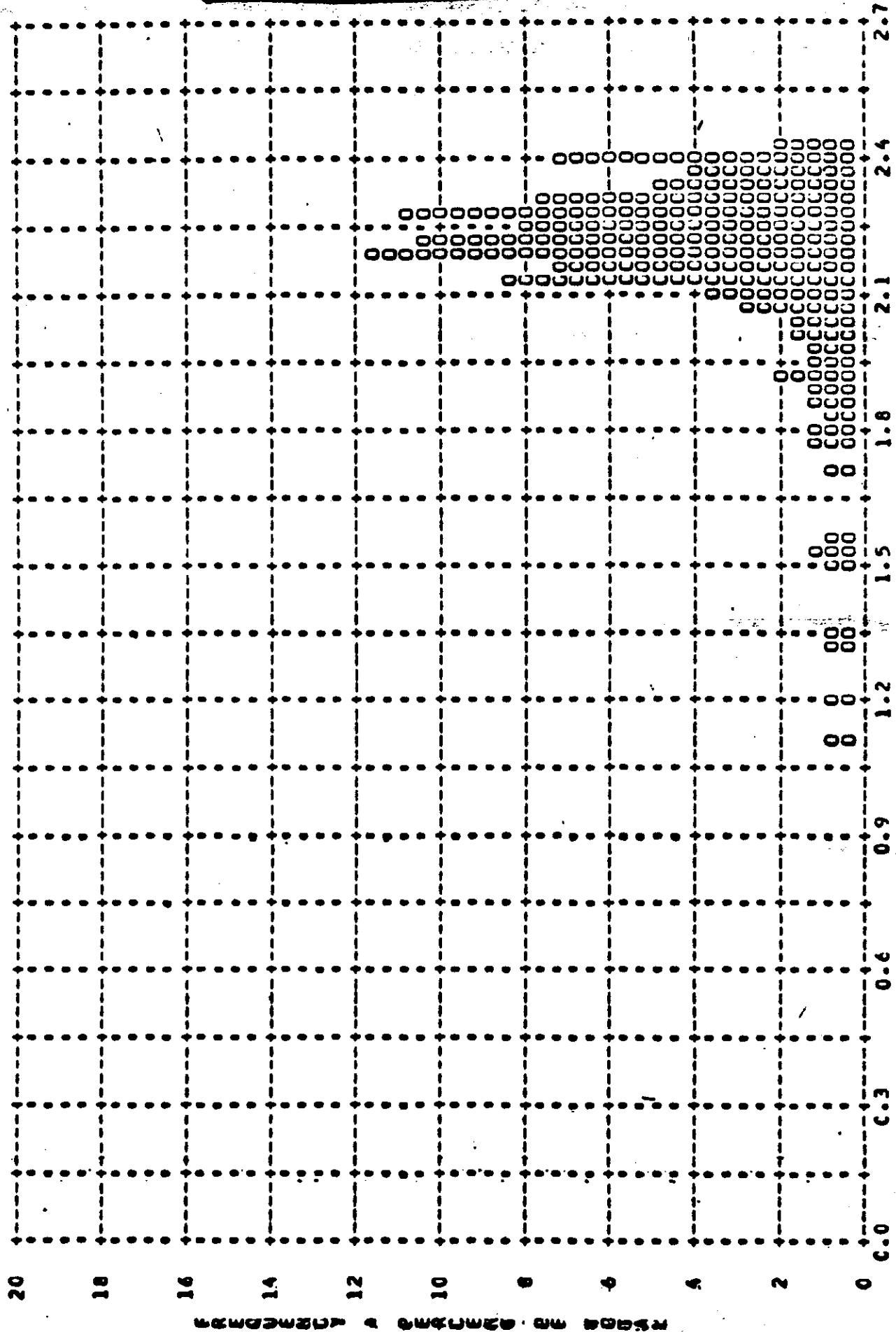


FIGURE 9-6

MISSION • ICIC-1 • INSTR • FWD • 2-09-64 • PLOT OF D MIN • TERRAIN • PROCESSING • ALL LEVELS
BRITH PEAN • 0.52 • PECIAN • C.47 • STD DEV • 0.17 • RANGE • 0.28 TO 1.14 WITH 247 SAMPLES

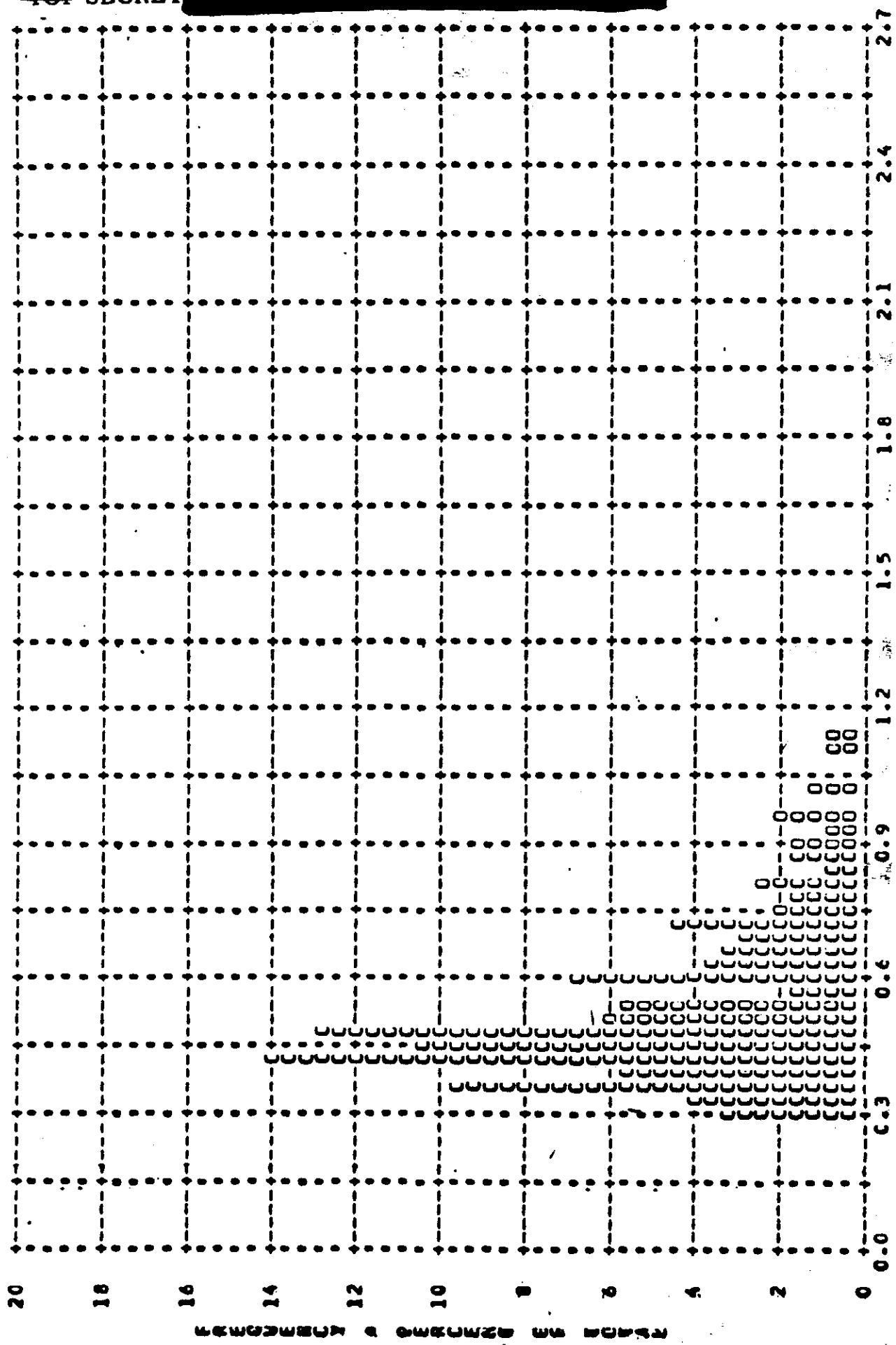
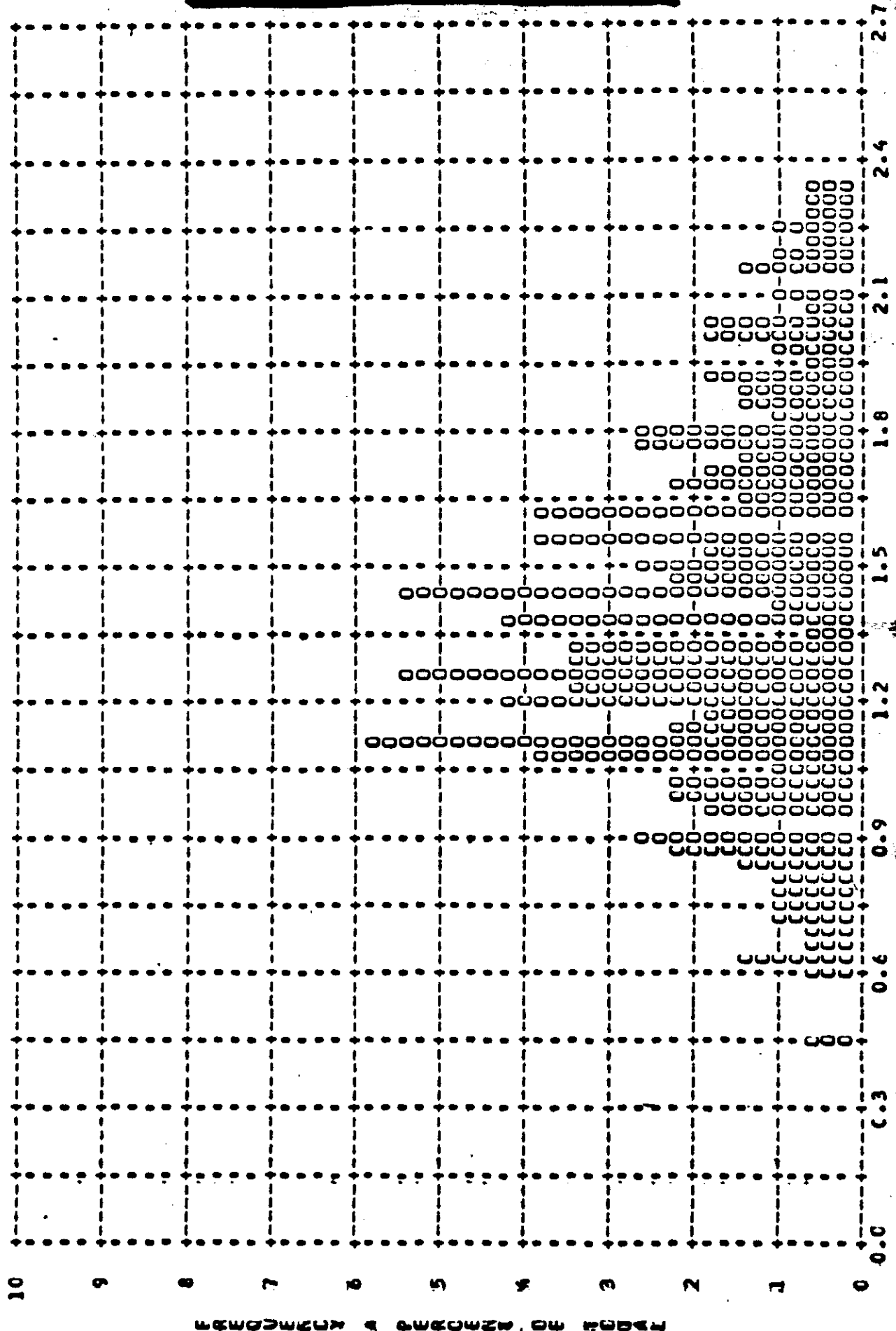


FIGURE 9-7

MISSION • ICIC-1 • INSIR • FND • 2-09-64 PLOT OF D MAX • TERRAIN • PROCESSING • ALL LEVELS
MIRIN PEAN • 1.36 • MEDIAN • 1.32 • STD DEV • 0.39 • RANGE • 0.43 TO 2.32 WITH 247 SAMPLES



MISSION • 101C-1 • INSTR • FND • 2-09-64 PLOT OF D MAX • CLOUD • PROCESSING • ALL LEVELS
DRITH PEAN • 2.16 • PECIAN • 2.20 • STD DEV • 0.20 • RANGE • 1.11 TO 2.42 WITH 243 SAMPLES

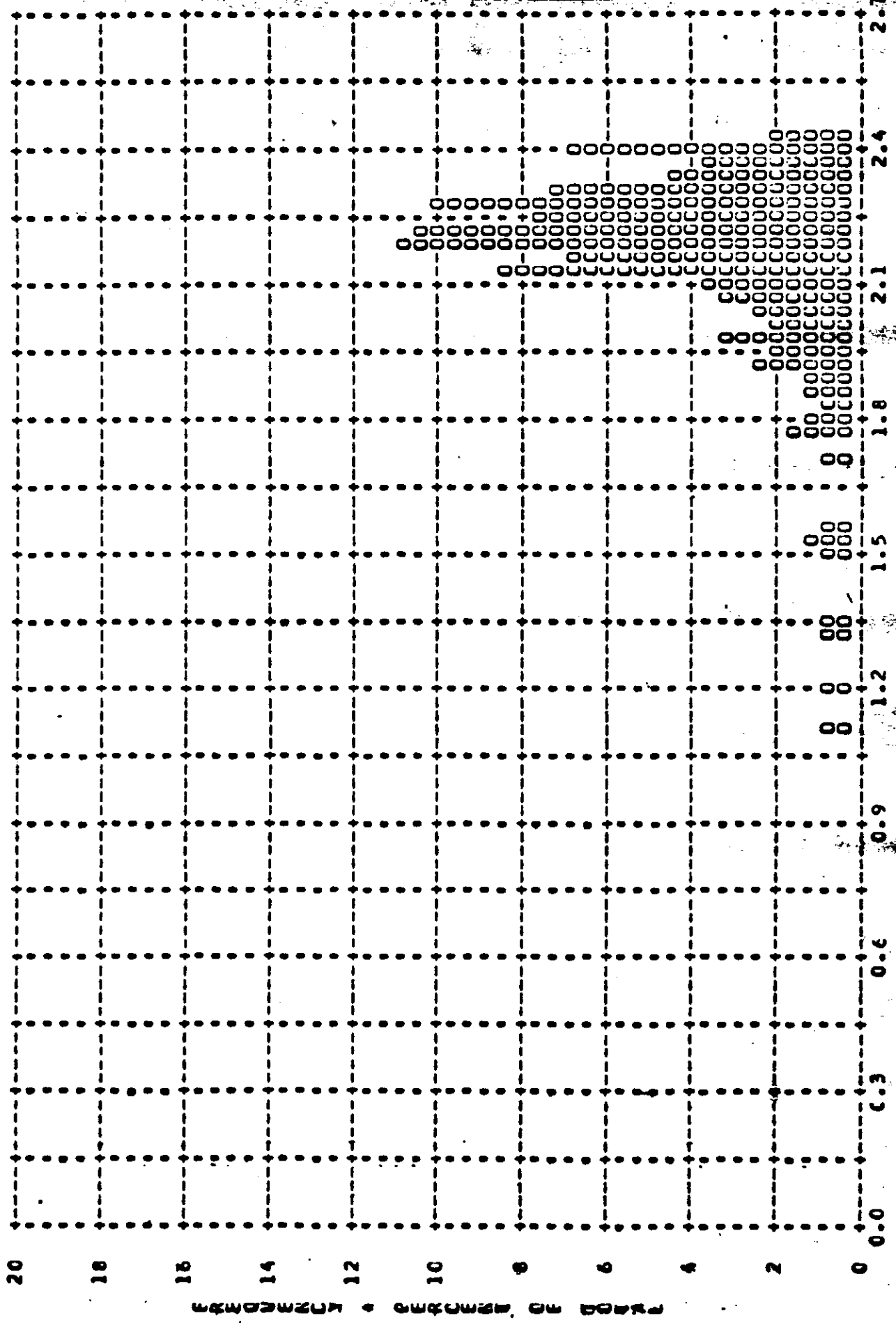


FIGURE 9-9

MISSION • 1010-1

• INSTRUMENT • AFT

2-09-64

DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
0001	0	0	0	0	0	0	0	0	0	0	0	0
0002	0	0	0	0	0	0	0	0	0	0	0	0
0003	0	0	0	0	0	0	0	0	0	0	0	0
0004	0	0	0	0	0	0	0	0	0	0	0	0
0005	0	0	0	0	0	0	0	0	0	0	0	0
0006	0	0	0	0	0	0	0	0	0	0	0	0
0007	0	0	0	0	0	0	0	0	0	0	0	0
0008	0	0	0	0	0	0	0	0	0	0	0	0
0009	0	0	0	0	0	0	0	0	0	0	0	0
0010	0	0	0	0	0	0	0	0	0	0	0	0
0011	0	0	0	0	0	0	0	0	0	0	0	0
0012	0	0	0	0	0	0	0	0	0	0	0	0
0013	0	0	0	0	0	0	0	0	0	0	0	0
0014	0	0	0	0	0	0	0	0	0	0	0	0
0015	0	0	0	0	0	0	0	0	0	0	0	0
0016	0	0	0	0	0	0	0	0	0	0	0	0
0017	0	0	0	0	0	0	0	0	0	0	0	0
0018	0	0	0	0	0	0	0	0	0	0	0	0
0019	0	0	0	0	0	0	0	0	0	0	0	0
0020	0	0	0	0	0	0	0	0	0	0	0	0
0021	0	0	0	0	0	0	0	0	0	0	0	0
0022	0	0	0	0	0	0	0	0	0	0	0	0
0023	0	0	0	0	0	0	0	0	0	0	0	0
0024	0	0	0	0	0	0	0	0	0	0	0	0
0025	0	0	0	0	0	0	0	0	0	0	0	0
0026	0	0	0	0	0	0	0	0	0	0	0	0
0027	0	0	0	0	0	0	0	0	0	0	0	0
0028	0	0	0	0	0	0	0	0	0	0	0	0
0029	0	0	0	0	0	0	0	0	0	0	0	0
0030	0	0	0	0	0	0	0	0	0	0	0	0
0031	0	0	0	0	0	0	0	0	0	0	0	0
0032	0	0	0	0	0	0	0	0	0	0	0	0
0033	0	0	0	0	0	0	0	0	0	0	0	0
0034	0	0	0	0	0	0	0	0	0	0	0	0
0035	0	0	0	0	0	0	0	0	0	0	0	0
0036	0	0	0	0	0	0	0	0	0	0	0	0
0037	0	0	0	0	0	0	0	0	0	0	0	0
0038	0	0	0	0	0	0	0	0	0	0	0	0
0039	0	0	0	0	0	0	0	0	0	0	0	0
0040	0	0	0	0	0	0	0	0	0	0	0	0
0041	0	0	0	0	0	0	0	0	0	0	0	0
0042	0	0	0	0	0	0	0	0	0	0	0	0
0043	0	0	0	0	0	0	0	0	0	0	0	0
0044	0	0	0	0	0	0	0	0	0	0	0	0
0045	0	0	0	0	0	0	0	0	0	0	0	0
0046	0	0	0	0	0	0	0	0	0	0	0	0
0047	0	0	0	0	0	0	0	0	0	0	0	0
0048	0	0	0	0	0	0	0	0	0	0	0	0
0049	0	0	0	0	0	0	0	0	0	0	0	0
0050	0	0	0	0	0	0	0	0	0	0	0	0
0051	0	0	0	0	0	0	0	0	0	0	0	0
0052	0	0	0	0	0	0	0	0	0	0	0	0
0053	0	0	0	0	0	0	0	0	0	0	0	0
0054	0	0	0	0	0	0	0	0	0	0	0	0
0055	0	0	0	0	0	0	0	0	0	0	0	0
0056	0	0	0	0	0	0	0	0	0	0	0	0
0057	0	0	0	0	0	0	0	0	0	0	0	0
0058	0	0	0	0	0	0	0	0	0	0	0	0
0059	0	0	0	0	0	0	0	0	0	0	0	0
0060	0	0	0	0	0	0	0	0	0	0	0	0
0061	0	0	0	0	0	0	0	0	0	0	0	0
0062	0	0	0	0	0	0	0	0	0	0	0	0
0063	0	0	0	0	0	0	0	0	0	0	0	0
0064	0	0	0	0	0	0	0	0	0	0	0	0
0065	0	0	0	0	0	0	0	0	0	0	0	0
0066	0	0	0	0	0	0	0	0	0	0	0	0
0067	0	0	0	0	0	0	0	0	0	0	0	0
0068	0	0	0	0	0	0	0	0	0	0	0	0
0069	0	0	0	0	0	0	0	0	0	0	0	0
0070	0	0	0	0	0	0	0	0	0	0	0	0
0071	0	0	0	0	0	0	0	0	0	0	0	0
0072	0	0	0	0	0	0	0	0	0	0	0	0
0073	0	0	0	0	0	0	0	0	0	0	0	0
0074	0	0	0	0	0	0	0	0	0	0	0	0
0075	0	0	0	0	0	0	0	0	0	0	0	0
0076	0	0	0	0	0	0	0	0	0	0	0	0
0077	0	0	0	0	0	0	0	0	0	0	0	0
0078	0	0	0	0	0	0	0	0	0	0	0	0
0079	0	0	0	0	0	0	0	0	0	0	0	0
0080	0	0	0	0	0	0	0	0	0	0	0	0
0081	0	0	0	0	0	0	0	0	0	0	0	0
0082	0	0	0	0	0	0	0	0	0	0	0	0
0083	0	0	0	0	0	0	0	0	0	0	0	0
0084	0	0	0	0	0	0	0	0	0	0	0	0
0085	0	0	0	0	0	0	0	0	0	0	0	0
0086	0	0	0	0	0	0	0	0	0	0	0	0
0087	0	0	0	0	0	0	0	0	0	0	0	0
0088	0	0	0	0	0	0	0	0	0	0	0	0
0089	0	0	0	0	0	0	0	0	0	0	0	0
0090	0	0	0	0	0	0	0	0	0	0	0	0
0091	0	0	0	0	0	0	0	0	0	0	0	0
0092	0	0	0	0	0	0	0	0	0	0	0	0
0093	0	0	0	0	0	0	0	0	0	0	0	0
0094	0	0	0	0	0	0	0	0	0	0	0	0
0095	0	0	0	0	0	0	0	0	0	0	0	0
0096	0	0	0	0	0	0	0	0	0	0	0	0
0097	0	0	0	0	0	0	0	0	0	0	0	0
0098	0	0	0	0	0	0	0	0	0	0	0	0
0099	0	0	0	0	0	0	0	0	0	0	0	0
0100	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL												
TOTAL												

TABLE 9-4

MISSION • ICIC-1

• INSTRUMENT • AFT

2-09-64

DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
.51	C	C	0	C	C	0	3	0	0	3	0	0
.52	C	C	0	C	C	0	1	0	0	2	0	0
.53	C	C	0	C	C	0	1	0	0	1	0	0
.54	C	C	0	C	C	0	1	0	0	1	0	0
.55	C	C	0	C	C	0	1	0	0	1	0	0
.56	C	C	0	C	C	0	1	0	0	1	0	0
.57	C	C	0	C	C	0	1	0	0	1	0	0
.58	C	C	0	C	C	0	1	0	0	1	0	0
.59	C	C	0	C	C	0	1	0	0	1	0	0
.60	C	C	0	C	C	0	1	0	0	1	0	0
.61	C	C	0	C	C	0	1	0	0	1	0	0
.62	C	C	0	C	C	0	1	0	0	1	0	0
.63	C	C	0	C	C	0	1	0	0	1	0	0
.64	C	C	0	C	C	0	1	0	0	1	0	0
.65	C	C	0	C	C	0	1	0	0	1	0	0
.66	C	C	0	C	C	0	1	0	0	1	0	0
.67	C	C	0	C	C	0	1	0	0	1	0	0
.68	C	C	0	C	C	0	1	0	0	1	0	0
.69	C	C	0	C	C	0	1	0	0	1	0	0
.70	C	C	0	C	C	0	1	0	0	1	0	0
.71	C	C	0	C	C	0	1	0	0	1	0	0
.72	C	C	0	C	C	0	1	0	0	1	0	0
.73	C	C	0	C	C	0	1	0	0	1	0	0
.74	C	C	0	C	C	0	1	0	0	1	0	0
.75	C	C	0	C	C	0	1	0	0	1	0	0
.76	C	C	0	C	C	0	1	0	0	1	0	0
.77	C	C	0	C	C	0	1	0	0	1	0	0
.78	C	C	0	C	C	0	1	0	0	1	0	0
.79	C	C	0	C	C	0	1	0	0	1	0	0
.80	C	C	0	C	C	0	1	0	0	1	0	0
.81	C	C	0	C	C	0	1	0	0	1	0	0
.82	C	C	0	C	C	0	1	0	0	1	0	0
.83	C	C	0	C	C	0	1	0	0	1	0	0
.84	C	C	0	C	C	0	1	0	0	1	0	0
.85	C	C	0	C	C	0	1	0	0	1	0	0
.86	C	C	0	C	C	0	1	0	0	1	0	0
.87	C	C	0	C	C	0	1	0	0	1	0	0
.88	C	C	0	C	C	0	1	0	0	1	0	0
.89	C	C	0	C	C	0	1	0	0	1	0	0
.90	C	C	0	C	C	0	1	0	0	1	0	0
.91	C	C	0	C	C	0	1	0	0	1	0	0
.92	C	C	0	C	C	0	1	0	0	1	0	0
.93	C	C	0	C	C	0	1	0	0	1	0	0
.94	C	C	0	C	C	0	1	0	0	1	0	0
.95	C	C	0	C	C	0	1	0	0	1	0	0
.96	C	C	0	C	C	0	1	0	0	1	0	0
.97	C	C	0	C	C	0	1	0	0	1	0	0
.98	C	C	0	C	C	0	1	0	0	1	0	0
.99	C	C	0	C	C	0	1	0	0	1	0	0
1.00	C	C	0	C	C	0	1	0	0	1	0	0
SUBTOTAL	C	C	0	C	C	0	119	18	1	13	18	1

TABLE 9-4

MISSION • 1020-1 • INSTRUMENT • AFT 2-09-64 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
1.01	C	C	C	C	C	C	0	1	0	0	1	0
1.02	C	C	C	C	C	C	0	1	0	0	1	0
1.03	C	C	C	C	C	C	0	1	0	0	1	0
1.04	C	C	C	C	C	C	0	1	0	0	1	0
1.05	C	C	C	C	C	C	0	1	0	0	1	0
1.06	C	C	C	C	C	C	0	1	0	0	1	0
1.07	C	C	C	C	C	C	0	1	0	0	1	0
1.08	C	C	C	C	C	C	0	1	0	0	1	0
1.09	C	C	C	C	C	C	0	1	0	0	1	0
1.10	C	C	C	C	C	C	0	1	0	0	1	0
1.11	C	C	C	C	C	C	0	1	0	0	1	0
1.12	C	C	C	C	C	C	0	1	0	0	1	0
1.13	C	C	C	C	C	C	0	1	0	0	1	0
1.14	C	C	C	C	C	C	0	1	0	0	1	0
1.15	C	C	C	C	C	C	0	1	0	0	1	0
1.16	C	C	C	C	C	C	0	1	0	0	1	0
1.17	C	C	C	C	C	C	0	1	0	0	1	0
1.18	C	C	C	C	C	C	0	1	0	0	1	0
1.19	C	C	C	C	C	C	0	1	0	0	1	0
1.20	C	C	C	C	C	C	0	1	0	0	1	0
1.21	C	C	C	C	C	C	0	1	0	0	1	0
1.22	C	C	C	C	C	C	0	1	0	0	1	0
1.23	C	C	C	C	C	C	0	1	0	0	1	0
1.24	C	C	C	C	C	C	0	1	0	0	1	0
1.25	C	C	C	C	C	C	0	1	0	0	1	0
1.26	C	C	C	C	C	C	0	1	0	0	1	0
1.27	C	C	C	C	C	C	0	1	0	0	1	0
1.28	C	C	C	C	C	C	0	1	0	0	1	0
1.29	C	C	C	C	C	C	0	1	0	0	1	0
1.30	C	C	C	C	C	C	0	1	0	0	1	0
1.31	C	C	C	C	C	C	0	1	0	0	1	0
1.32	C	C	C	C	C	C	0	1	0	0	1	0
1.33	C	C	C	C	C	C	0	1	0	0	1	0
1.34	C	C	C	C	C	C	0	1	0	0	1	0
1.35	C	C	C	C	C	C	0	1	0	0	1	0
1.36	C	C	C	C	C	C	0	1	0	0	1	0
1.37	C	C	C	C	C	C	0	1	0	0	1	0
1.38	C	C	C	C	C	C	0	1	0	0	1	0
1.39	C	C	C	C	C	C	0	1	0	0	1	0
1.40	C	C	C	C	C	C	0	1	0	0	1	0
1.41	C	C	C	C	C	C	0	1	0	0	1	0
1.42	C	C	C	C	C	C	0	1	0	0	1	0
1.43	C	C	C	C	C	C	0	1	0	0	1	0
1.44	C	C	C	C	C	C	0	1	0	0	1	0
1.45	C	C	C	C	C	C	0	1	0	0	1	0
1.46	C	C	C	C	C	C	0	1	0	0	1	0
1.47	C	C	C	C	C	C	0	1	0	0	1	0
1.48	C	C	C	C	C	C	0	1	0	0	1	0
1.49	C	C	C	C	C	C	0	1	0	0	1	0
1.50	C	C	C	C	C	C	0	1	0	0	1	0
SUBTOTAL							6	124	4	7	13	5

TABLE 9-4

MISSION • 1010-1 • INSTRUMENT • AFT 2-09-64 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY		INTERMEDIATE			FULL			ALL LEVELS			
	MIN	MAX	L	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
1.51	C	C	0	C	0	0	0	0	0	0	0	0
1.52	C	C	0	C	0	0	0	0	0	0	0	0
1.53	C	C	0	C	0	0	0	0	0	0	0	0
1.54	C	C	0	C	0	0	0	0	0	0	0	0
1.55	C	C	0	C	0	0	0	0	0	0	0	0
1.56	C	C	0	C	0	0	0	0	0	0	0	0
1.57	C	C	0	C	0	0	0	0	0	0	0	0
1.58	C	C	0	C	0	0	0	0	0	0	0	0
1.59	C	C	0	C	0	0	0	0	0	0	0	0
1.60	C	C	0	C	0	0	0	0	0	0	0	0
1.61	C	C	0	C	0	0	0	0	0	0	0	0
1.62	C	C	0	C	0	0	0	0	0	0	0	0
1.63	C	C	0	C	0	0	0	0	0	0	0	0
1.64	C	C	0	C	0	0	0	0	0	0	0	0
1.65	C	C	0	C	0	0	0	0	0	0	0	0
1.66	C	C	0	C	0	0	0	0	0	0	0	0
1.67	C	C	0	C	0	0	0	0	0	0	0	0
1.68	C	C	0	C	0	0	0	0	0	0	0	0
1.69	C	C	0	C	0	0	0	0	0	0	0	0
1.70	C	C	0	C	0	0	0	0	0	0	0	0
1.71	C	C	0	C	0	0	0	0	0	0	0	0
1.72	C	C	0	C	0	0	0	0	0	0	0	0
1.73	C	C	0	C	0	0	0	0	0	0	0	0
1.74	C	C	0	C	0	0	0	0	0	0	0	0
1.75	C	C	0	C	0	0	0	0	0	0	0	0
1.76	C	C	0	C	0	0	0	0	0	0	0	0
1.77	C	C	0	C	0	0	0	0	0	0	0	0
1.78	C	C	0	C	0	0	0	0	0	0	0	0
1.79	C	C	0	C	0	0	0	0	0	0	0	0
1.80	C	C	0	C	0	0	0	0	0	0	0	0
1.81	C	C	0	C	0	0	0	0	0	0	0	0
1.82	C	C	0	C	0	0	0	0	0	0	0	0
1.83	C	C	0	C	0	0	0	0	0	0	0	0
1.84	C	C	0	C	0	0	0	0	0	0	0	0
1.85	C	C	0	C	0	0	0	0	0	0	0	0
1.86	C	C	0	C	0	0	0	0	0	0	0	0
1.87	C	C	0	C	0	0	0	0	0	0	0	0
1.88	C	C	0	C	0	0	0	0	0	0	0	0
1.89	C	C	0	C	0	0	0	0	0	0	0	0
1.90	C	C	0	C	0	0	0	0	0	0	0	0
1.91	C	C	0	C	0	0	0	0	0	0	0	0
1.92	C	C	0	C	0	0	0	0	0	0	0	0
1.93	C	C	0	C	0	0	0	0	0	0	0	0
1.94	C	C	0	C	0	0	0	0	0	0	0	0
1.95	C	C	0	C	0	0	0	0	0	0	0	0
1.96	C	C	0	C	0	0	0	0	0	0	0	0
1.97	C	C	0	C	0	0	0	0	0	0	0	0
1.98	C	C	0	C	0	0	0	0	0	0	0	0
1.99	C	C	0	C	0	0	0	0	0	0	0	0
2.00	C	C	0	C	0	0	0	0	0	0	0	0
SUBTOTAL	C	C	0	C	0	0	0	0	0	0	0	0

TABLE 9-4

MISSION • 1010-1 • INSTRUMENT • AFT 2-09-64 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2			0			1			0			1
3			0			0			0			1
4			0			0			0			1
5			0			0			0			1
6			0			0			0			1
7			0			0			0			1
8			0			0			0			1
9			0			0			0			1
10			0			0			0			1
11			0			0			0			1
12			0			0			0			1
13			0			0			0			1
14			0			0			0			1
15			0			0			0			1
16			0			0			0			1
17			0			0			0			1
18			0			0			0			1
19			0			0			0			1
20			0			0			0			1
21			0			0			0			1
22			0			0			0			1
23			0			0			0			1
24			0			0			0			1
25			0			0			0			1
26			0			0			0			1
27			0			0			0			1
28			0			0			0			1
29			0			0			0			1
30			0			0			0			1
SUBTOTAL			0			30			14			18
TOTAL			0			30			14			18

TABLE 9-4

MISSION • 1010-1 • INSTRUMENT • AFT 2-09-64 DENSITY FREQ DISTR

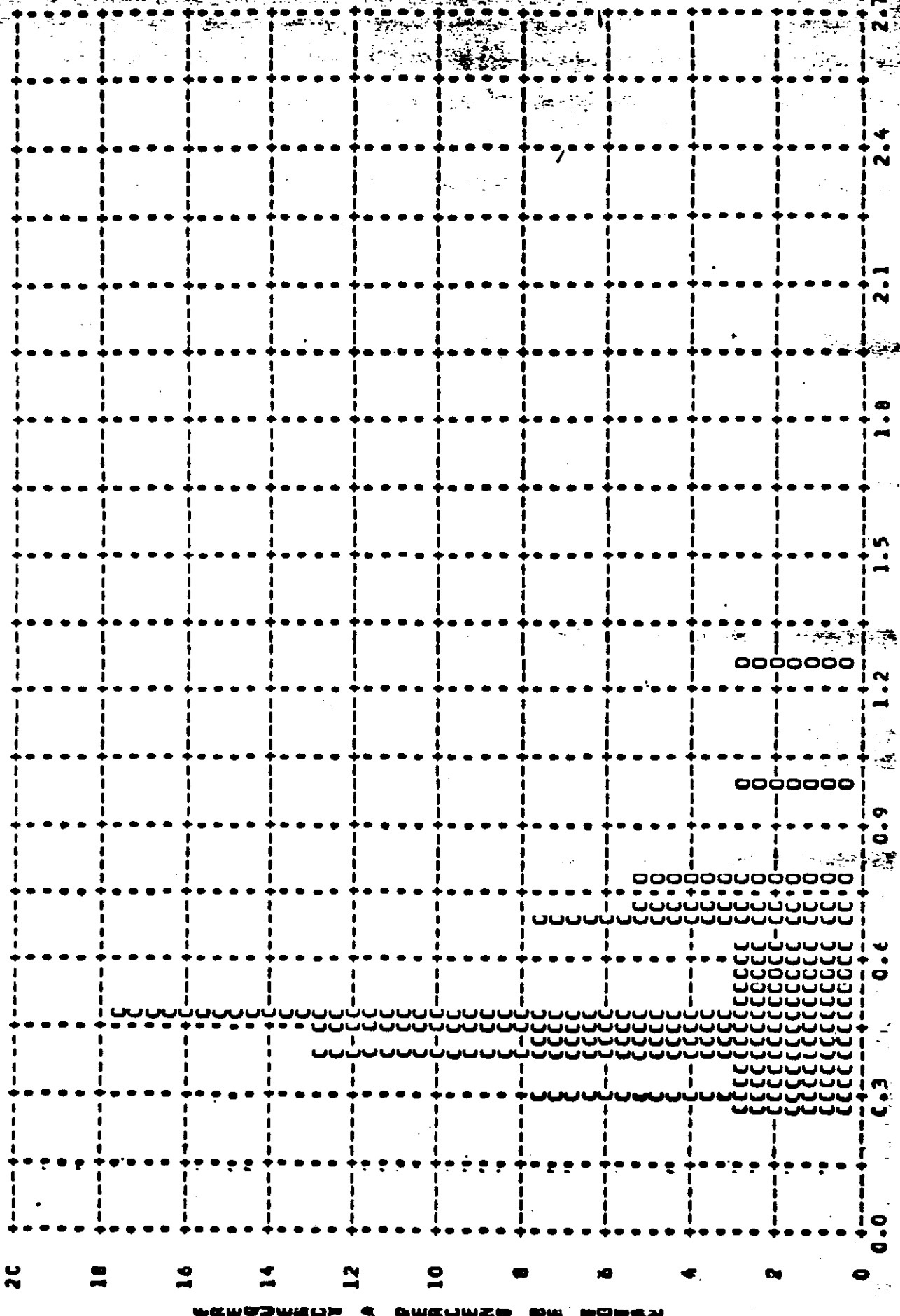
DENSITY VALUE	PRIMARY		INTERMEDIATE			FULL			ALL LEVELS			
	MIN	MAX LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	
2.51	C	C	C	0	0	0	0	0	0	0	0	
2.52	C	C	C	0	0	0	0	0	0	0	0	
2.53	C	C	C	0	0	0	0	0	0	0	0	
2.54	C	C	C	0	0	0	0	0	0	0	0	
2.55	C	C	C	0	0	0	0	0	0	0	0	
2.56	C	C	C	0	0	0	0	0	0	0	0	
2.57	C	C	C	0	0	0	0	0	0	0	0	
2.58	C	C	C	0	0	0	0	0	0	0	0	
2.59	C	C	C	0	0	0	0	0	0	0	0	
2.60	C	C	C	0	0	0	0	0	0	0	0	
2.61	C	C	C	0	0	0	0	0	0	0	0	
2.62	C	C	C	0	0	0	0	0	0	0	0	
2.63	C	C	C	0	0	0	0	0	0	0	0	
2.64	C	C	C	0	0	0	0	0	0	0	0	
2.65	C	C	C	0	0	0	0	0	0	0	0	
2.66	C	C	C	0	0	0	0	0	0	0	0	
2.67	C	C	C	0	0	0	0	0	0	0	0	
2.68	C	C	C	0	0	0	0	0	0	0	0	
2.69	C	C	C	0	0	0	0	0	0	0	0	
2.70	C	C	C	0	0	0	0	0	0	0	0	
SLBTCTAL	C	C	0	0	0	0	0	0	0	0	0	
TCTAL	C	C	0	40	40	35	215	215	209	255	255	244

MISSION 1010-1 INSTR - AFT 2-09-64 PROCESSING AND EXPOSURE ANA

PROCESS LEVEL	SAMPLE SIZE	UNCER EXPCSEC	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OV EXPOS
PRIMARY	C	C PC	0 PC	0 PC	0 PC	0
INTERMEDIATE	4C	C PC	27 PC	67 PC	5 PC	0
FULL	215	11 PC	0 PC	83 PC	6 PC	0
ALL LEVELS	255	9 PC	4 PC	81 PC	6 PC	0
PROCESS LEVEL	BASE + FCG	UNCER EXPCSEC	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OV EXPOS
PRIMARY	0.01-C.19	C.01-C.13	0.14-0.39	0.40-0.90	-----	0.91 AN
INTERMED	C.10-C.17	C.01-C.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AN
FULL	C.18 AND UP	C.01-C.35	-----	0.40-0.90	0.91-1.69	1.70 AN

TABLE 9-4

MIS61CN • ICIC-1 • INSTR • AFT • 2-09-64 PLOT OF D MIN • TERRAIN • PRCESSING • INTERMEDIATE
ARITH MEAN • 0.51 • PELTAN • C.47 • STD DEV • C.19 • RANGE • 0.27 TO 1.25 WITH 40 SAMPLES



MISSION • ICIC-1 • INSTR • AFT • 2-09-64 PLOT OF D MAX • TERRAIN • PROCESSING • INTERMEDIATE
ORITH PEAN • 1.63 • PECIAN • 1.61 • STD DEV • 0.25 • RANGE • 1.18 TO 2.26 WITH 40 SAMPLES

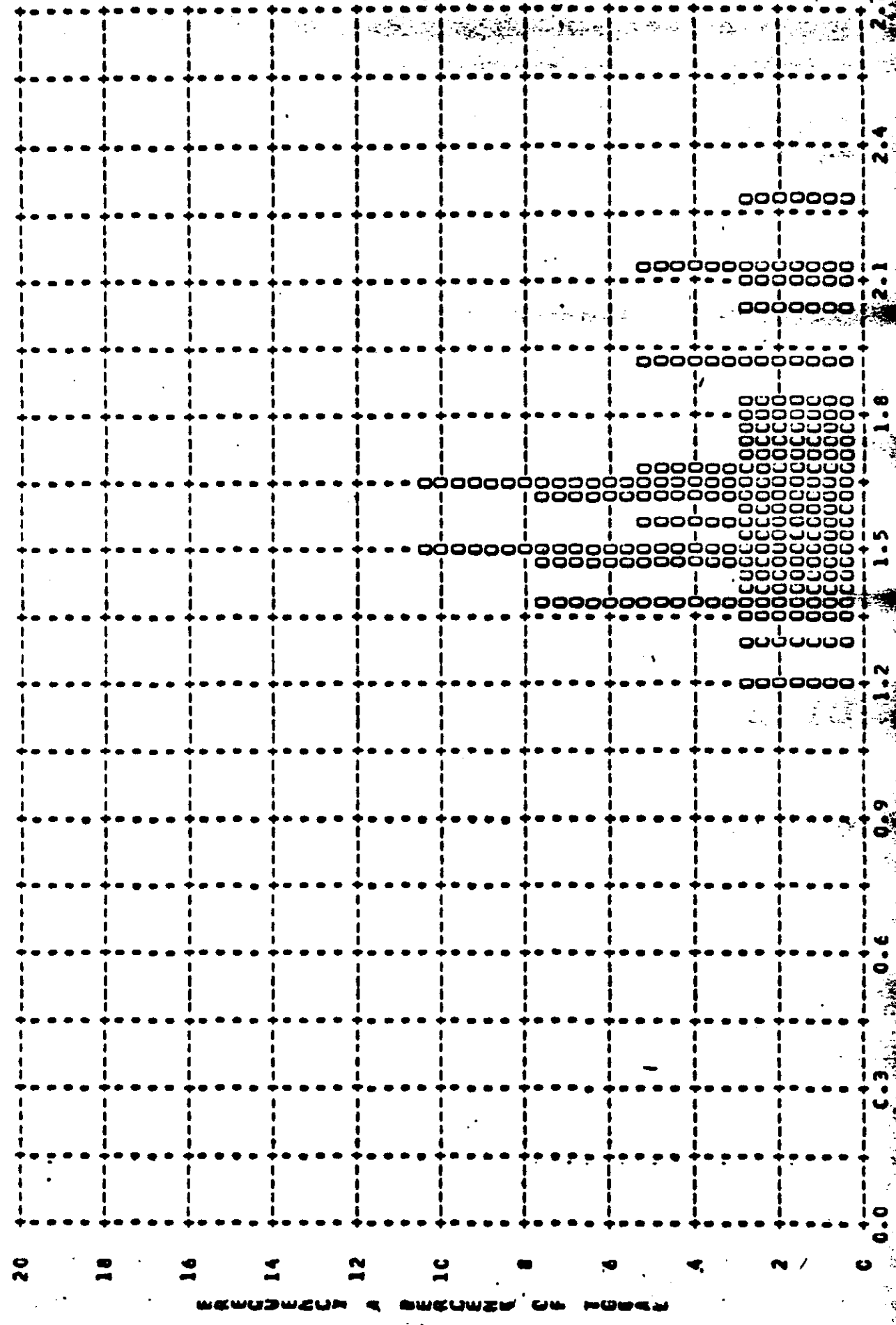


FIGURE 9-11

MISSICA • IC10-1 • INSIR • AFI • 2-09-64 PLOT OF D MAX • CLOUD • PROCESSING • INTERMEDIATE
#RITH PEAN • 2.15 • PECIAN • 2.18 • STD DEV • 0.19 • RANGE • 1.42 TO 2.40 WITH 35 SAMPLES

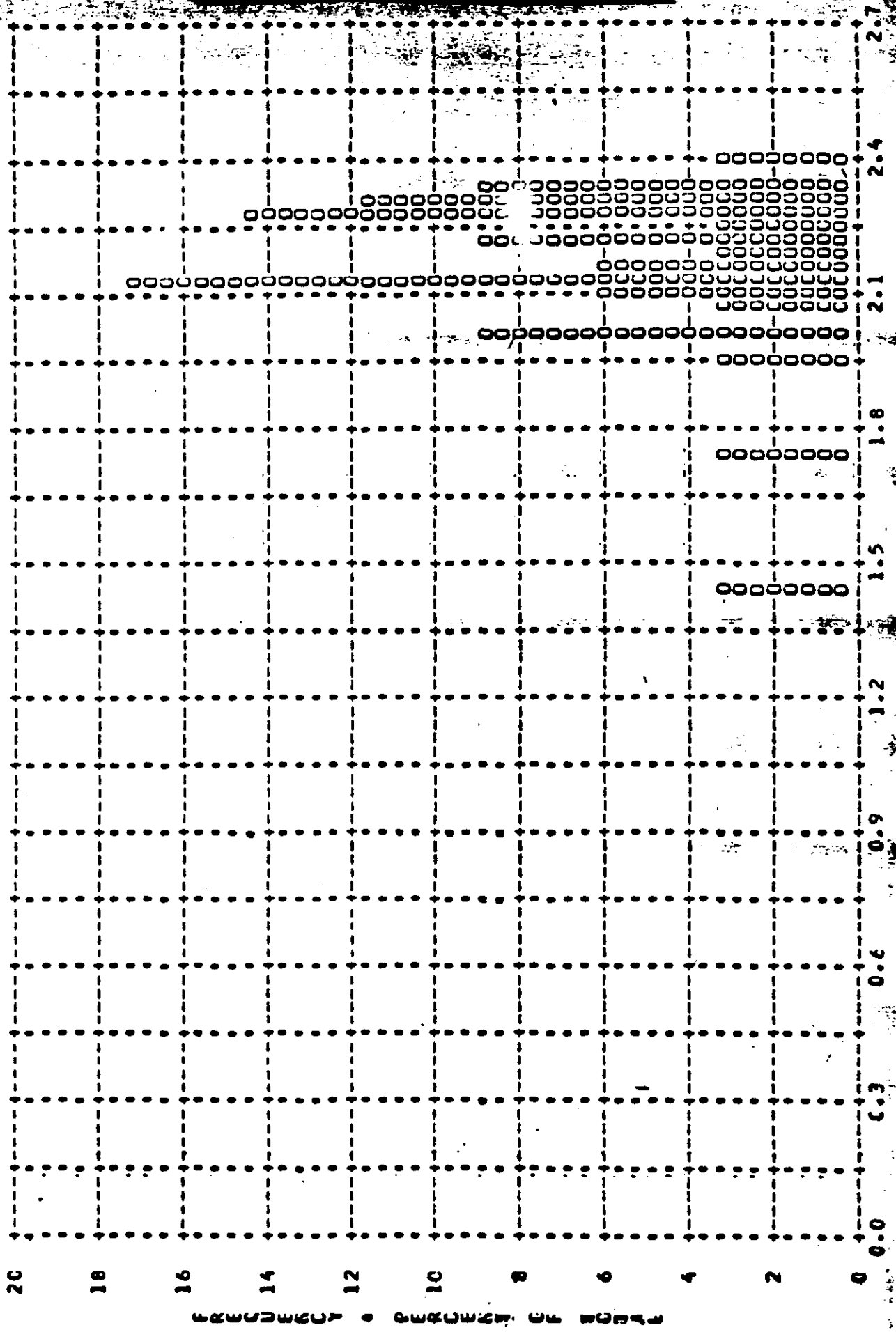
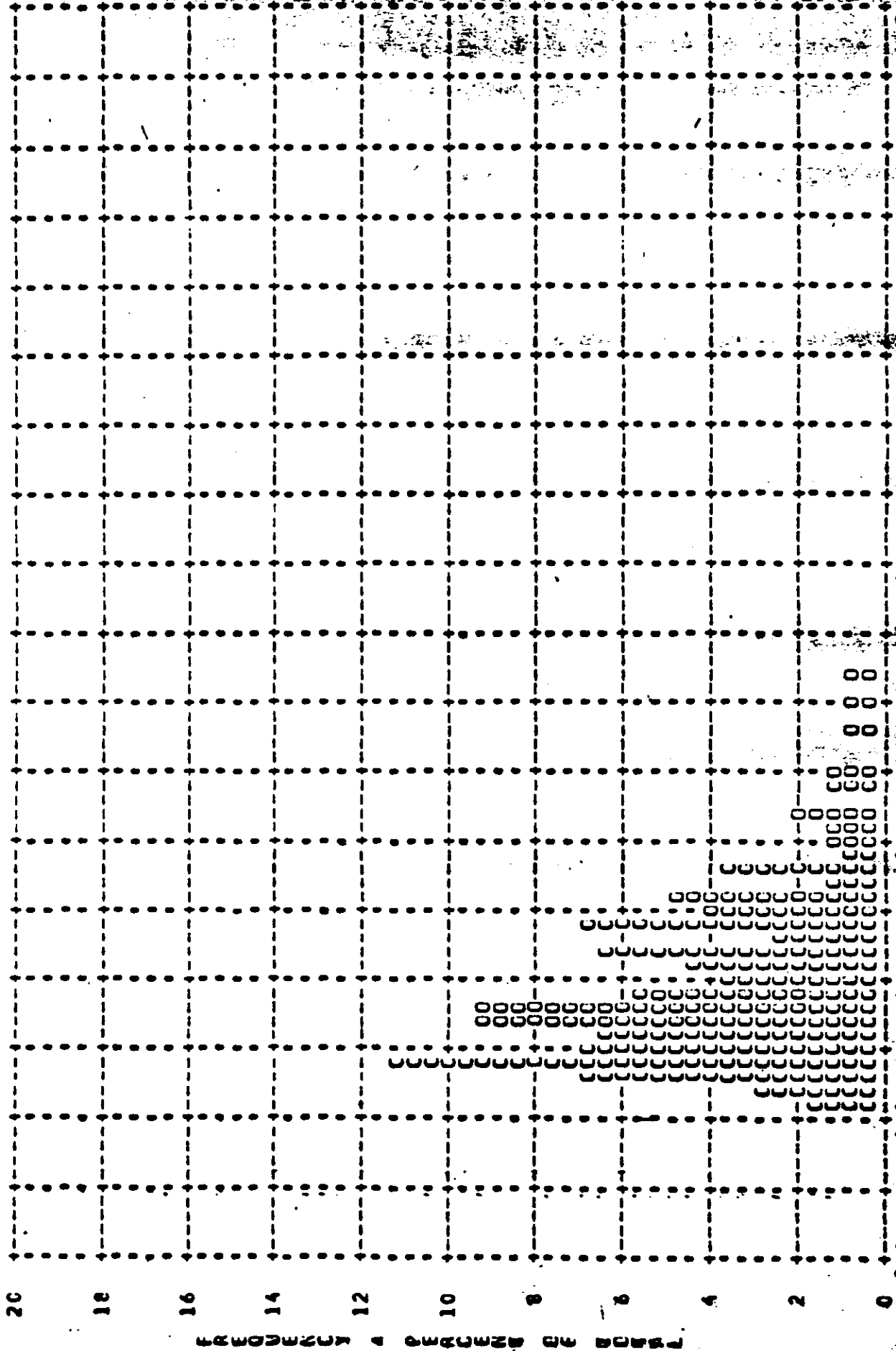
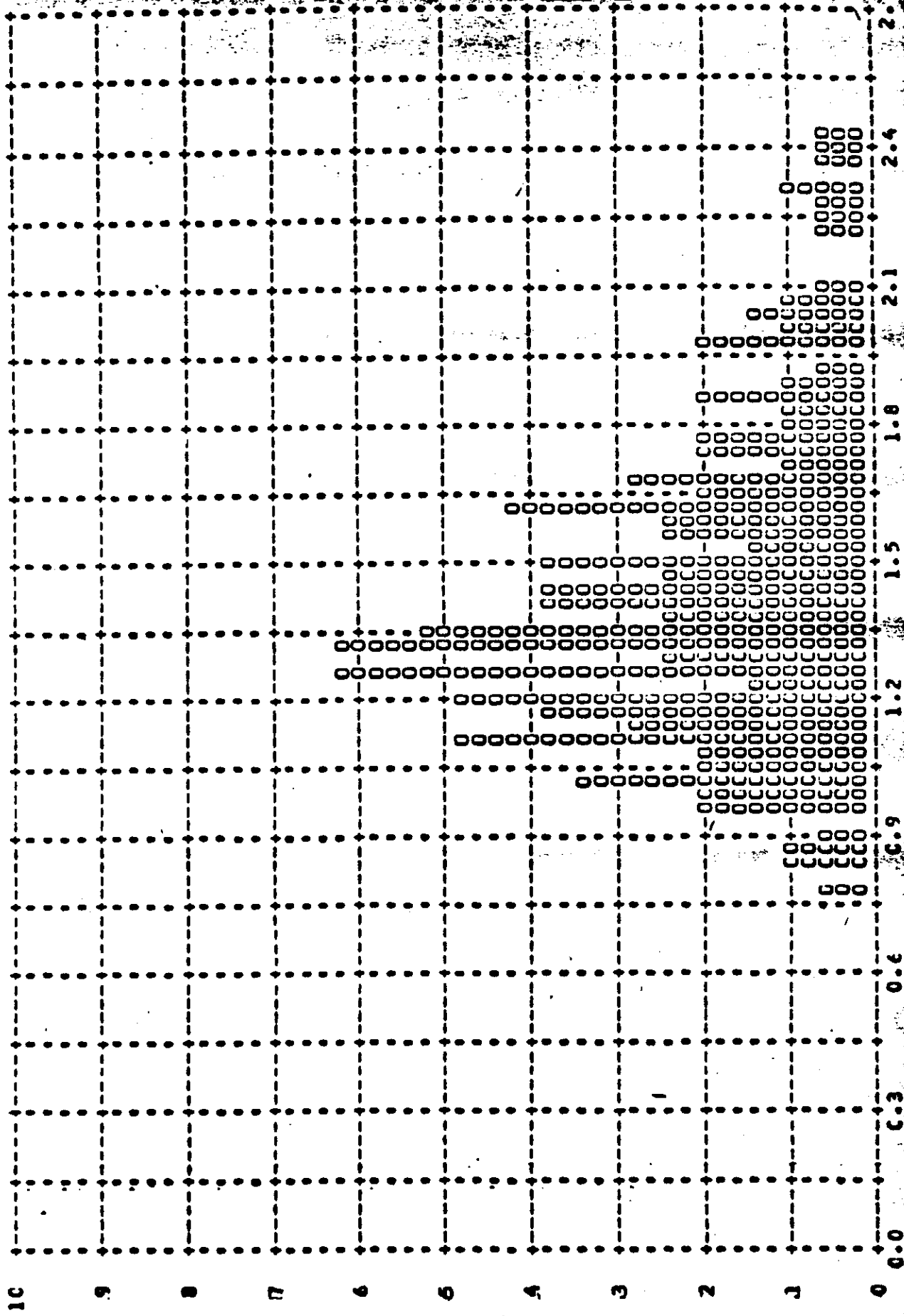


FIGURE 9-12

MISSIC • ICIC-1 • INSTR • AFT • 2-05-64 PLOT OF D PIN • TERRAIN • PROCESSING • FULL
BRITH MEAN • C.5E • MEDIAN • C.54 • STD DEV • 0.18 • RANGE • 0.31 TO 1.25 WITH 215 SAMPLES



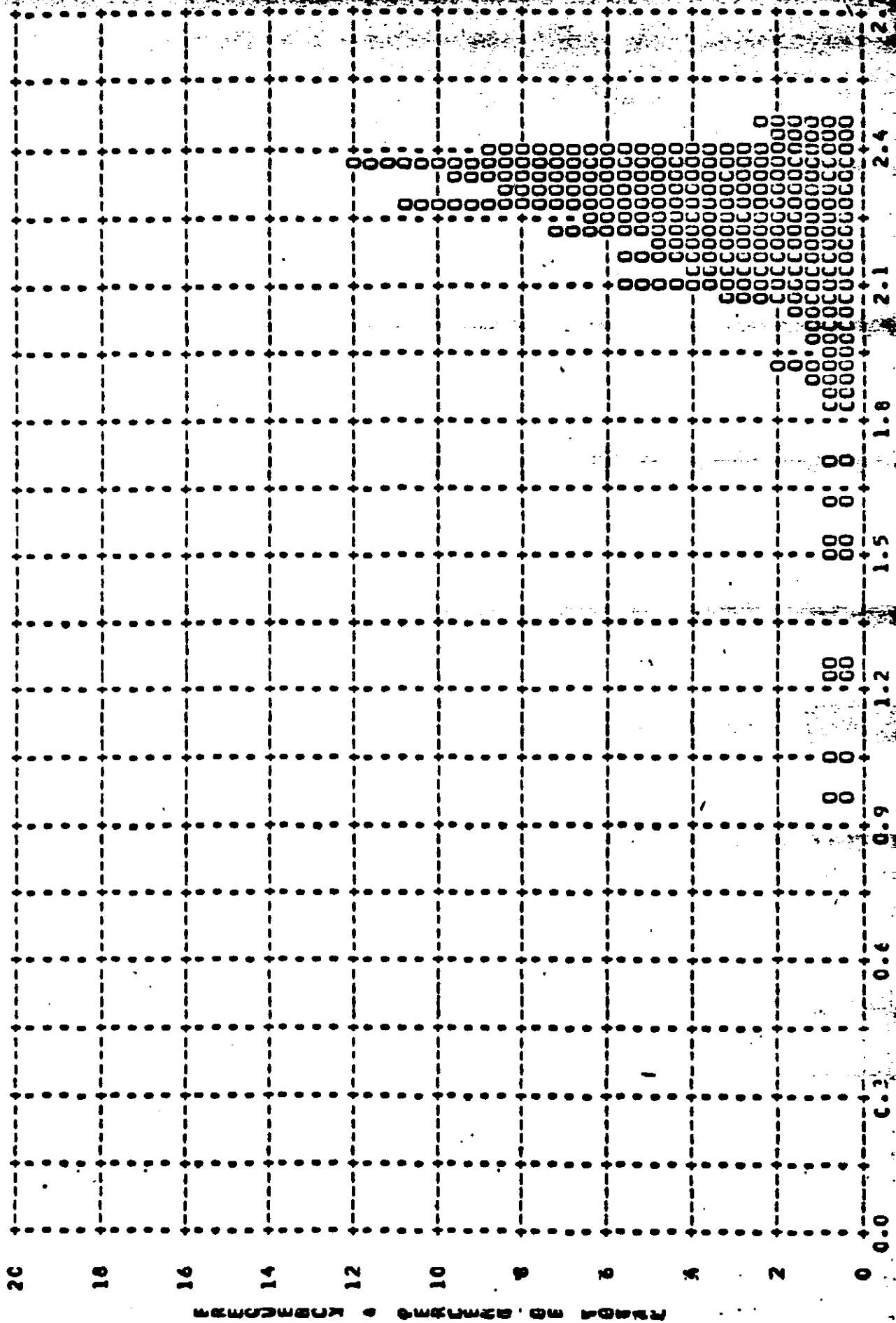
MISSION • ICIC-1 • INSTR • AFT • 2-09-64 PLOT OF D MAX • TERRAIN • PROCESSING • FULL
ARITH MEAN • 1.42 • MEDIAN • 1.35 • STD DEV • 0.34 • RANGE • 0.78 TO 2.42 WITH 215 SAMPLES



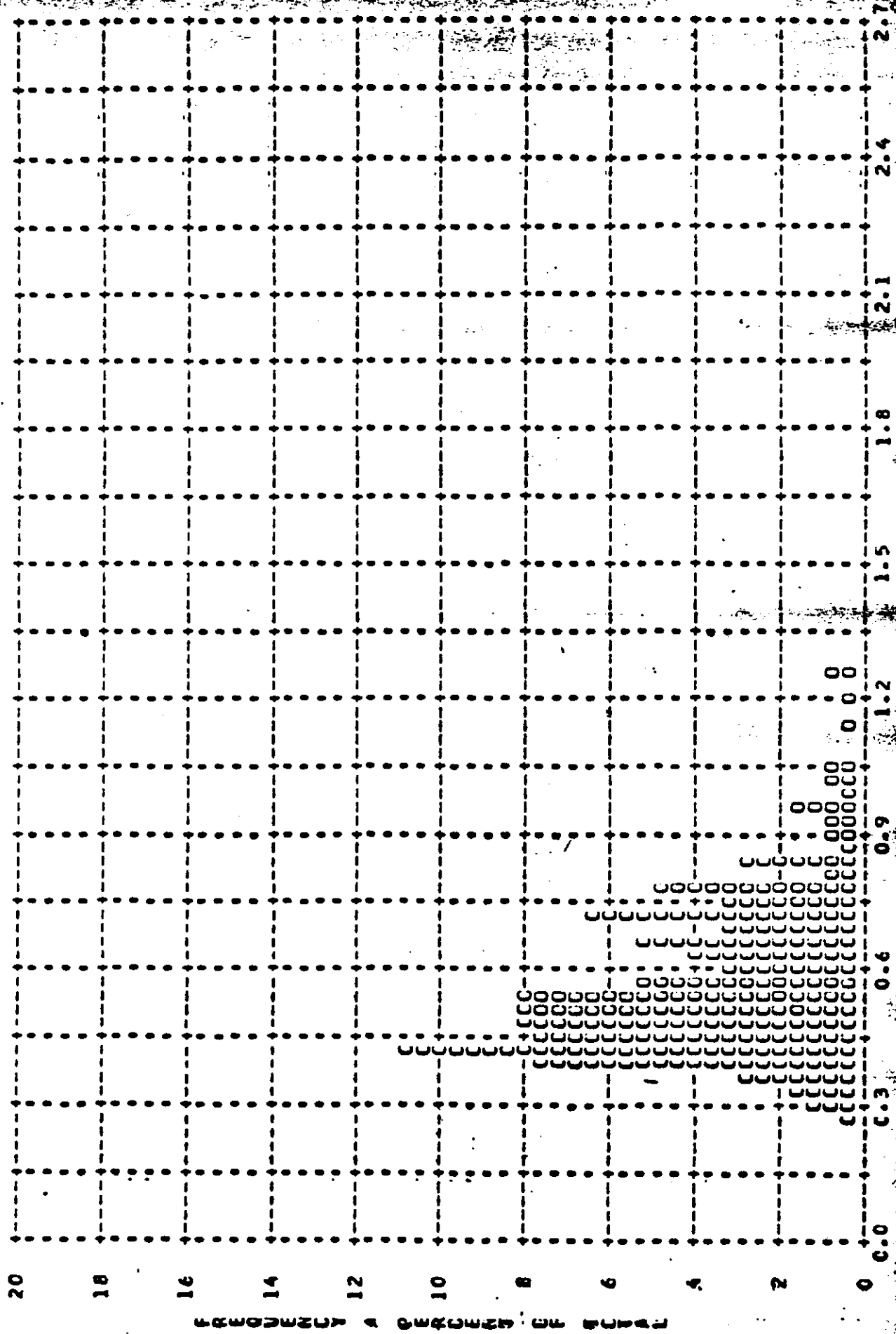
REPRODUCED FROM THE ORIGINAL SOURCE

FIGURE 9-14

MISSION • IOIC-1 • INSTR • AFT • 2-09-64 PLOT OF D MAX • CLOUD • PROCESSING • FULL
ARITH MEAN • 2.21 • MEDIAN • 2.26 • STD DEV • 0.22 • RANGE • 0.96 TO 2.46 WITH 209 SAMPLES



MISSICA • ICIC-1 • INSTR • ATI • 2-09-64 PLOT OF D MIN • TERRAIN • PROCESSING • ALL LEVELS
ARITH MEAN • 0.57 • MECHAN • C.52 • STD DEV • C.18 • RANGE • 0.27 TO 1.25 WITH 255 SAMPLES



MISSION • ICIC-1 • INSTR • AFT • 2-09-64 PLOT OF D MAX • TERRAIN • PROCESSING • ALL LEVELS
ARITH MEAN • 1.45 • PECIAN • 1.41 • STD DEV • 0.33 • RANGE • 0.78 TO 2.42 WITH 255 SAMPLES

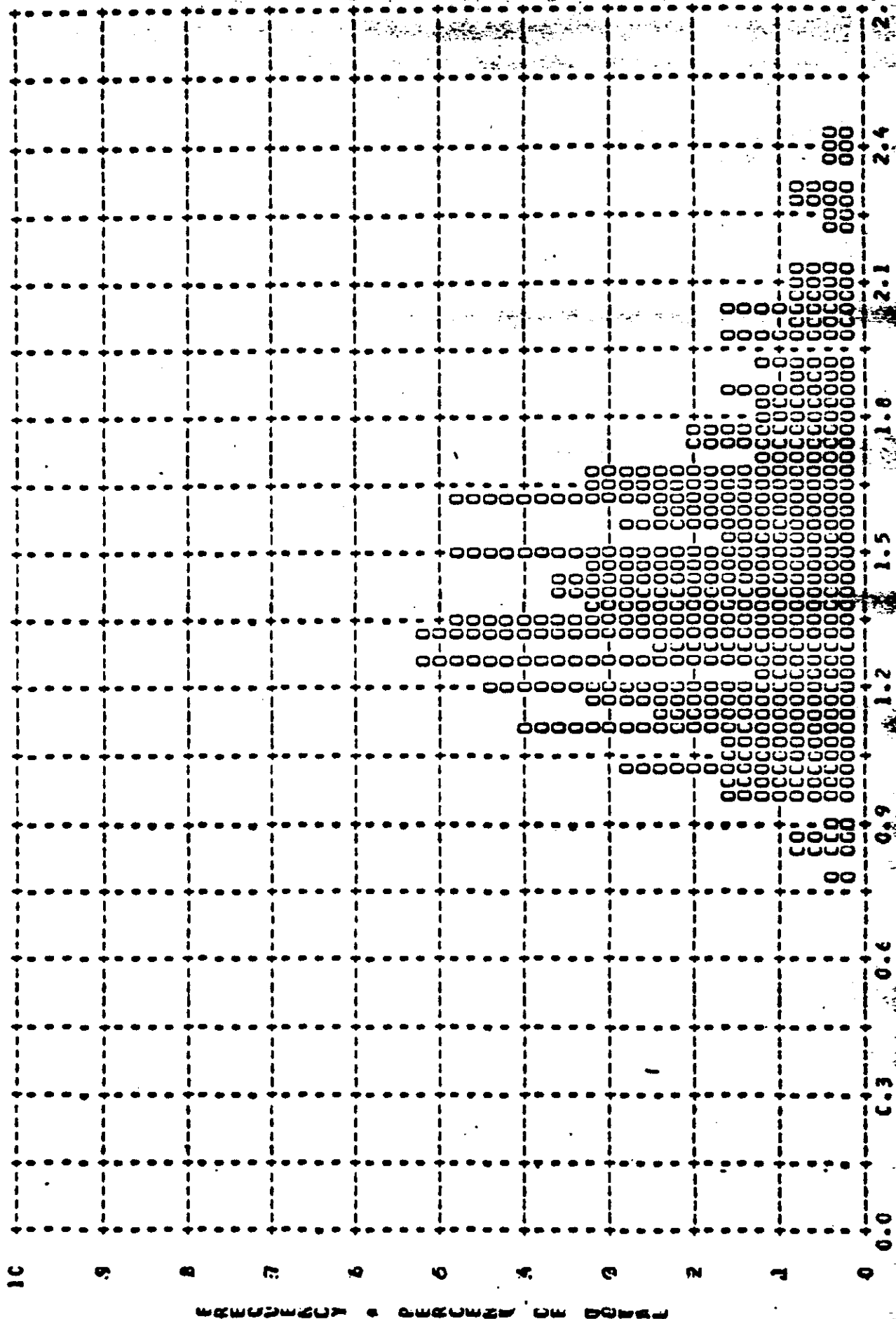
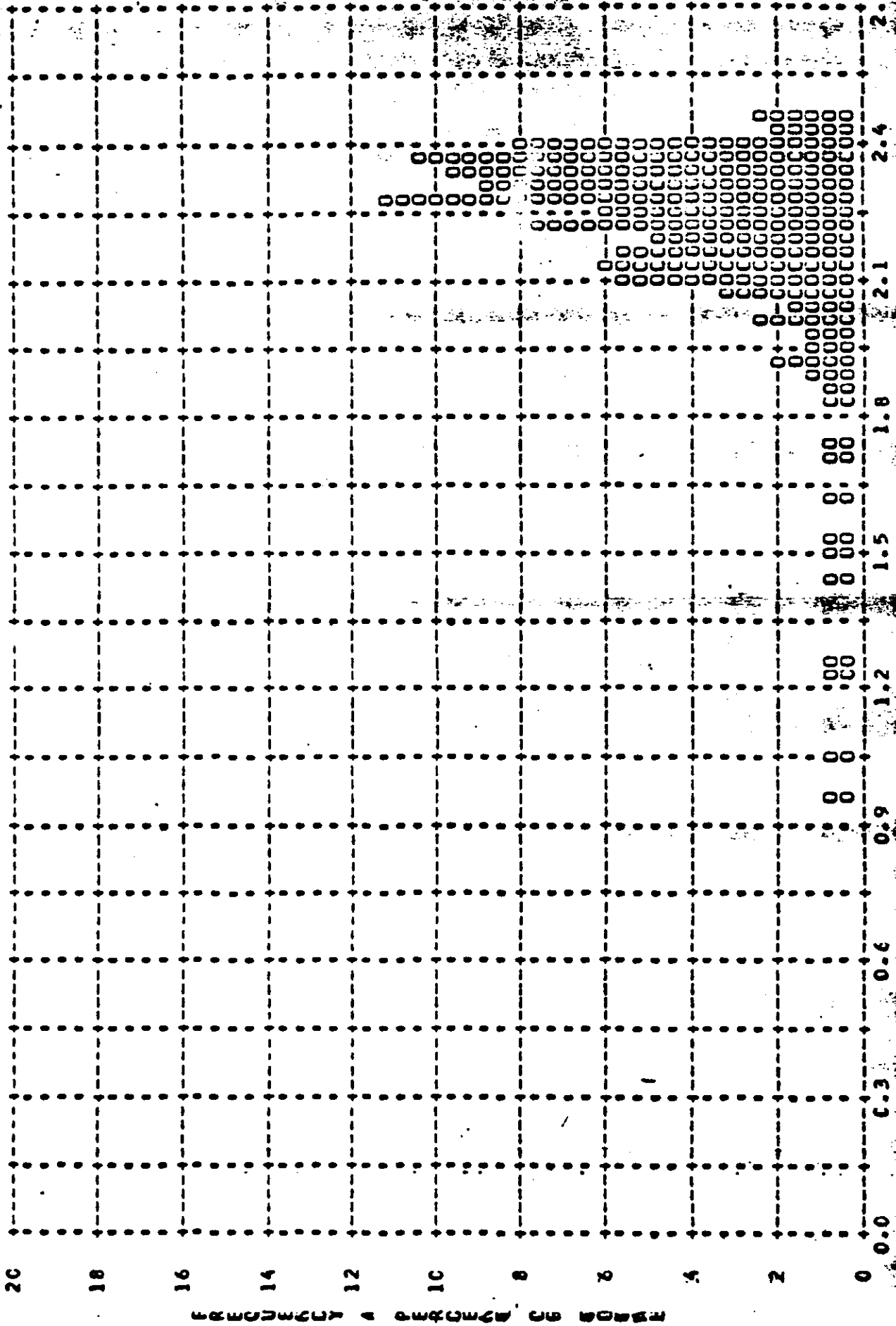


FIGURE 9-17

MISSION • 101C-1 • INSTR • AFT • 2-05-64 PLOT OF D MAX • CLOUD • PROCESSING • ALL LEVELS
WITH PEAR • 2.2C • MEDIAN • 2.26 • STD DEV • 0.22 • RANGE • 0.96 TO 2.46 WITH 244 SAMPLES



MISSION • 1010-2

• INSTRUMENT • FWD

2-09-64

DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
C.01	0	0	0	0	0	0	0	0	0	0	0	0
C.02	0	0	0	0	0	0	0	0	0	0	0	0
C.03	0	0	0	0	0	0	0	0	0	0	0	0
C.04	0	0	0	0	0	0	0	0	0	0	0	0
C.05	0	0	0	0	0	0	0	0	0	0	0	0
C.06	0	0	0	0	0	0	0	0	0	0	0	0
C.07	0	0	0	0	0	0	0	0	0	0	0	0
C.08	0	0	0	0	0	0	0	0	0	0	0	0
C.09	0	0	0	0	0	0	0	0	0	0	0	0
C.10	0	0	0	0	0	0	0	0	0	0	0	0
C.11	0	0	0	0	0	0	0	0	0	0	0	0
C.12	0	0	0	0	0	0	0	0	0	0	0	0
C.13	0	0	0	0	0	0	0	0	0	0	0	0
C.14	0	0	0	0	0	0	0	0	0	0	0	0
C.15	0	0	0	0	0	0	0	0	0	0	0	0
C.16	0	0	0	0	0	0	0	0	0	0	0	0
C.17	0	0	0	0	0	0	0	0	0	0	0	0
C.18	0	0	0	0	0	0	0	0	0	0	0	0
C.19	0	0	0	0	0	0	0	0	0	0	0	0
C.20	0	0	0	0	0	0	0	0	0	0	0	0
C.21	0	0	0	0	0	0	0	0	0	0	0	0
C.22	0	0	0	0	0	0	0	0	0	0	0	0
C.23	0	0	0	0	0	0	0	0	0	0	0	0
C.24	0	0	0	0	0	0	0	0	0	0	0	0
C.25	0	0	0	0	0	0	0	0	0	0	0	0
C.26	0	0	0	0	0	0	0	0	0	0	0	0
C.27	0	0	0	0	0	0	0	0	0	0	0	0
C.28	0	0	0	0	0	0	0	0	0	0	0	0
C.29	0	0	0	0	0	0	0	0	0	0	0	0
C.30	0	0	0	0	0	0	0	0	0	0	0	0
C.31	0	0	0	0	0	0	0	0	0	0	0	0
C.32	0	0	0	0	0	0	0	0	0	0	0	0
C.33	0	0	0	0	0	0	0	0	0	0	0	0
C.34	0	0	0	0	0	0	0	0	0	0	0	0
C.35	0	0	0	0	0	0	0	0	0	0	0	0
C.36	0	0	0	0	0	0	0	0	0	0	0	0
C.37	0	0	0	0	0	0	0	0	0	0	0	0
C.38	0	0	0	0	0	0	0	0	0	0	0	0
C.39	0	0	0	0	0	0	0	0	0	0	0	0
C.40	0	0	0	0	0	0	0	0	0	0	0	0
C.41	0	0	0	0	0	0	0	0	0	0	0	0
C.42	0	0	0	0	0	0	0	0	0	0	0	0
C.43	0	0	0	0	0	0	0	0	0	0	0	0
C.44	0	0	0	0	0	0	0	0	0	0	0	0
C.45	0	0	0	0	0	0	0	0	0	0	0	0
C.46	0	0	0	0	0	0	0	0	0	0	0	0
C.47	0	0	0	0	0	0	0	0	0	0	0	0
C.48	0	0	0	0	0	0	0	0	0	0	0	0
C.49	0	0	0	0	0	0	0	0	0	0	0	0
C.50	0	0	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	126	108	108	126	108	108	126	108	108	126	108	108

TABLE 9-5

MISSION • 1010-2

• INSTRUMENT • FWD

2-09-64

DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
C. 51	C	C	0	C	0	0	3	0	0	3	0	0
C. 52	C	C	0	C	0	0	1	1	0	5	1	0
C. 53	C	C	0	C	0	0	1	1	0	2	1	0
C. 54	C	C	0	C	0	0	2	2	0	2	1	0
C. 55	C	C	0	C	0	0	2	2	0	4	1	0
C. 56	C	C	0	C	0	0	7	7	0	6	1	0
C. 57	C	C	0	C	0	0	7	7	0	7	1	0
C. 58	C	C	0	C	0	0	7	7	0	7	1	0
C. 59	C	C	0	C	0	0	9	9	0	0	1	0
C. 60	C	C	0	C	0	0	9	9	0	4	1	0
C. 61	C	C	0	C	0	0	0	0	0	0	1	0
C. 62	C	C	0	C	0	0	0	0	0	2	1	0
C. 63	C	C	0	C	0	0	0	0	0	3	1	0
C. 64	C	C	0	C	0	0	1	1	0	6	1	0
C. 65	C	C	0	C	0	0	1	1	0	2	1	0
C. 66	C	C	0	C	0	0	1	1	0	3	1	0
C. 67	C	C	0	C	0	0	1	1	0	4	1	0
C. 68	C	C	0	C	0	0	1	1	0	4	1	0
C. 69	C	C	0	C	0	0	1	1	0	4	1	0
C. 70	C	C	0	C	0	0	1	1	0	4	1	0
C. 71	C	C	0	C	0	0	1	1	0	4	1	0
C. 72	C	C	0	C	0	0	1	1	0	2	1	0
C. 73	C	C	0	C	0	0	1	1	0	0	1	0
C. 74	C	C	0	C	0	0	1	1	0	1	1	0
C. 75	C	C	0	C	0	0	1	1	0	1	1	0
C. 76	C	C	0	C	0	0	1	1	0	1	1	0
C. 77	C	C	0	C	0	0	1	1	0	1	1	0
C. 78	C	C	0	C	0	0	1	1	0	4	1	0
C. 79	C	C	0	C	0	0	1	1	0	2	1	0
C. 80	C	C	0	C	0	0	1	1	0	2	1	0
C. 81	C	C	0	C	0	0	1	1	0	1	1	0
C. 82	C	C	0	C	0	0	1	1	0	0	1	0
C. 83	C	C	0	C	0	0	1	1	0	0	1	0
C. 84	C	C	0	C	0	0	1	1	0	0	1	0
C. 85	C	C	0	C	0	0	1	1	0	4	1	0
C. 86	C	C	0	C	0	0	1	1	0	1	1	0
C. 87	C	C	0	C	0	0	1	1	0	6	1	0
C. 88	C	C	0	C	0	0	1	1	0	3	1	0
C. 89	C	C	0	C	0	0	1	1	0	0	1	0
C. 90	C	C	0	C	0	0	1	1	0	3	1	0
C. 91	C	C	0	C	0	0	1	1	0	0	1	0
C. 92	C	C	0	C	0	0	1	1	0	1	1	0
C. 93	C	C	0	C	0	0	1	1	0	1	1	0
C. 94	C	C	0	C	0	0	1	1	0	4	1	0
C. 95	C	C	0	C	0	0	1	1	0	1	1	0
C. 96	C	C	0	C	0	0	1	1	0	1	1	0
C. 97	C	C	0	C	0	0	1	1	0	1	1	0
C. 98	C	C	0	C	0	0	1	1	0	1	1	0
C. 99	C	C	0	C	0	0	1	1	0	1	1	0
C. 00	C	C	0	C	0	0	1	1	0	1	1	0
SUBTOTAL			0			1			8		10	

TABLE 9-5

MISSION • 1010-2 • INSTRUMENT • FWD 2-09-64 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
1.01			0			0			0			0
1.02			0			0			0			0
1.03			0			0			0			0
1.04			0			0			0			0
1.05			0			0			0			0
1.06			0			0			0			0
1.07			0			0			0			0
1.08			0			0			0			0
1.09			0			0			0			0
1.10			0			0			0			0
1.11			0			0			0			0
1.12			0			0			0			0
1.13			0			0			0			0
1.14			0			0			0			0
1.15			0			0			0			0
1.16			0			0			0			0
1.17			0			0			0			0
1.18			0			0			0			0
1.19			0			0			0			0
1.20			0			0			0			0
1.21			0			0			0			0
1.22			0			0			0			0
1.23			0			0			0			0
1.24			0			0			0			0
1.25			0			0			0			0
1.26			0			0			0			0
1.27			0			0			0			0
1.28			0			0			0			0
1.29			0			0			0			0
1.30			0			0			0			0
1.31			0			0			0			0
1.32			0			0			0			0
1.33			0			0			0			0
1.34			0			0			0			0
1.35			0			0			0			0
1.36			0			0			0			0
1.37			0			0			0			0
1.38			0			0			0			0
1.39			0			0			0			0
1.40			0			0			0			0
1.41			0			0			0			0
1.42			0			0			0			0
1.43			0			0			0			0
1.44			0			0			0			0
1.45			0			0			0			0
1.46			0			0			0			0
1.47			0			0			0			0
1.48			0			0			0			0
1.49			0			0			0			0
1.50			0			0			0			0
SLBTCTAL			0			0			0			0

TABLE 9-5

MISSION • 1010-2

• INSTRUMENT • FWD

2-09-64

DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2												
3												
4												
5												
6												
7												
8												
9												
10												
11												
12												
13												
14												
15												
16												
17												
18												
19												
20												
21												
22												
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33												
34												
35												
36												
37												
38												
39												
40												
41												
42												
43												
44												
45												
46												
47												
48												
49												
50												
TOTAL												

TABLE 9-5

MISSION • 1010-2 • INSTRUMENT • FWD 2-09-64 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.51	C	C	0	C	0	0	0	0	0	0	0	0
2.52	C	C	0	C	0	0	0	0	0	0	0	0
2.53	C	C	0	C	0	0	0	0	0	0	0	0
2.54	C	C	0	C	0	0	0	0	0	0	0	0
2.55	C	C	0	C	0	0	0	0	0	0	0	0
2.56	C	C	0	C	0	0	0	0	0	0	0	0
2.57	C	C	0	C	0	0	0	0	0	0	0	0
2.58	C	C	0	C	0	0	0	0	0	0	0	0
2.59	C	C	0	C	0	0	0	0	0	0	0	0
2.60	C	C	0	C	0	0	0	0	0	0	0	0
2.61	C	C	0	C	0	0	0	0	0	0	0	0
2.62	C	C	0	C	0	0	0	0	0	0	0	0
2.63	C	C	0	C	0	0	0	0	0	0	0	0
2.64	C	C	0	C	0	0	0	0	0	0	0	0
2.65	C	C	0	C	0	0	0	0	0	0	0	0
2.66	C	C	0	C	0	0	0	0	0	0	0	0
2.67	C	C	0	C	0	0	0	0	0	0	0	0
2.68	C	C	0	C	0	0	0	0	0	0	0	0
2.69	C	C	0	C	0	0	0	0	0	0	0	0
2.70	C	C	0	C	0	0	0	0	0	0	0	0
SUBTOTAL	C	C	0	C	0	0	0	0	0	0	0	0
TOTAL	C	C	0	34	34	33	223	223	206	257	257	239

MISSION 1010-2		INSTR - FWD		2-09-64		PROCESSING AND EXPOSURE ANA				
PROCESS LEVEL	SAMPLE SIZE	UNCER EXPCSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OV EXPOS				
PRIMARY	C	C PC	0 PC	0 PC	0 PC	0				
INTERMEDIATE	34	C PC	32 PC	62 PC	6 PC	0				
FULL	223	26 PC	0 PC	68 PC	6 PC	0				
ALL LEVELS	257	22 PC	4 PC	67 PC	6 PC	0				
PROCESS LEVEL	BASE + FCG	UNCER EXPCSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OV EXPOS				
PRIMARY	C.01-C.15	C.01-C.13	0.14-0.39	0.40-0.90	-----	0.91 AN				
INTERMED	0.10-C.17	C.01-C.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AN				
FULL	C.18 ANC UP	C.01-C.35	-----	0.40-0.90	0.91-1.69	1.70 AN				

TABLE 9-5

MISSION • ICIC-2 • INSTR • FAD • 2-09-64 PLOT OF D M/H • TERRAIN • PROCESSING • INTERMEDIATE
BRITH PEAN • 0.58 • MECIAN • C.56 • STD DIV • 0.23 • RANGE • 0.28 TO 1.00 WITH 34 SAMPLES

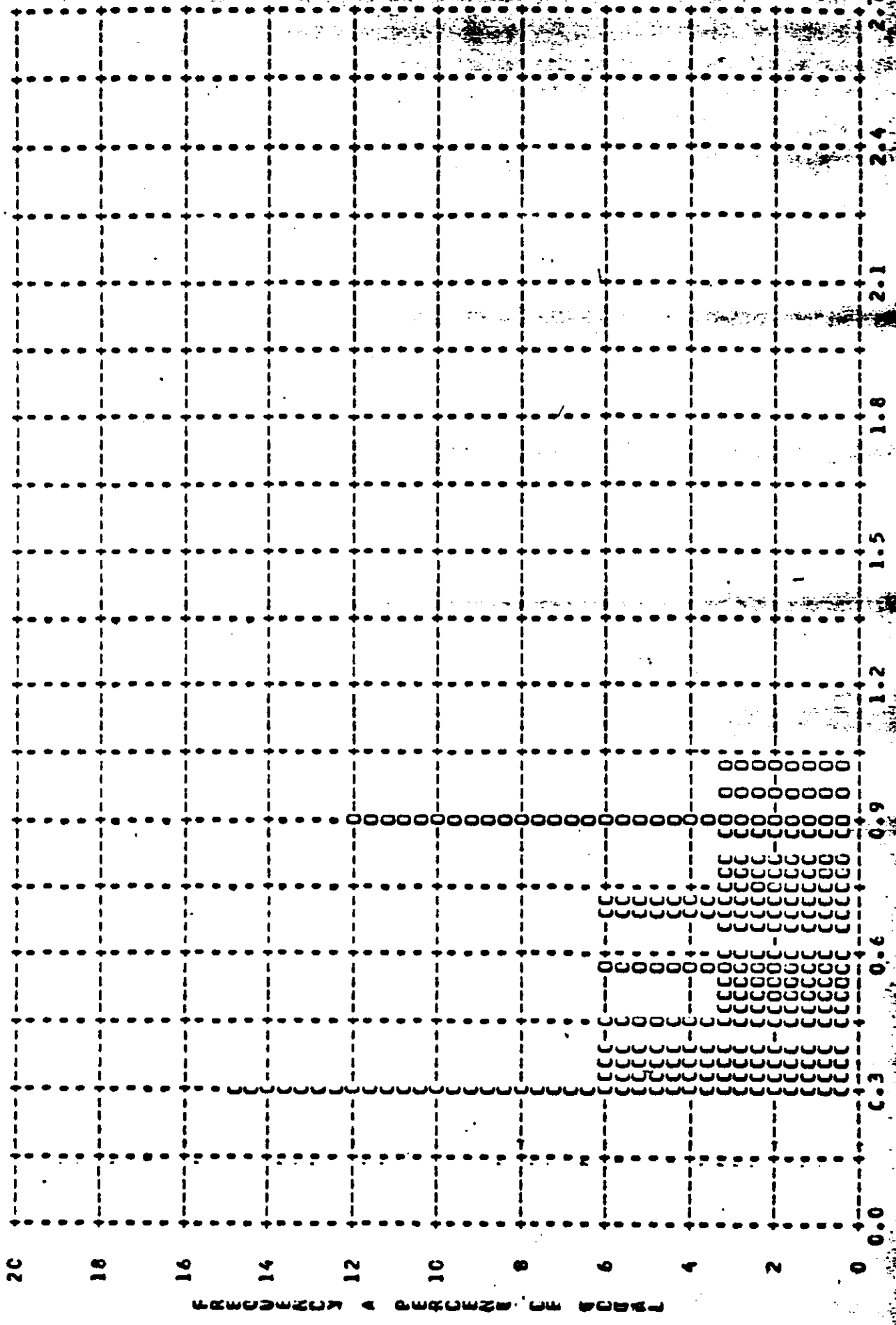


FIGURE 9-19

MISSION • ICIC-2 • INSTR • FND • 2-09-64 PLOT OF D MAX • TERRAIN • PROCESSING • INTERMEDIATE
WITH MEAN • 1.51 • MEDIAN • 1.44 • STD DEV • 0.44 • RANGE • 0.82 TO 2.32 WITH 34 SAMPLES

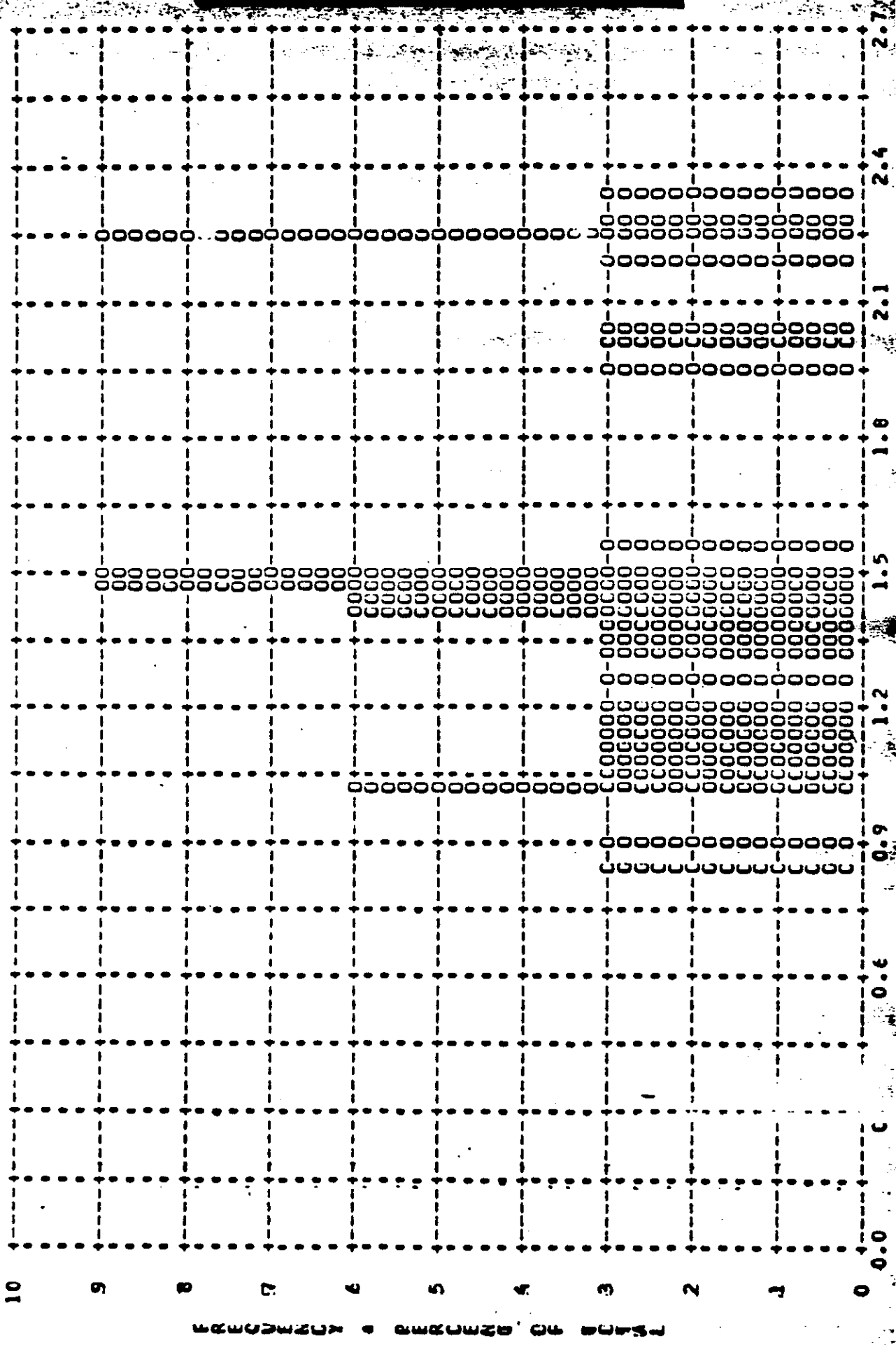


FIGURE 9-20

MISSION • 1010-2 • INSTR • FND • 2-09-64 PLCT OF D MAX • CLOUD • PROCESSING • INTERMEDIATE
DRITH PLAN • 2.12 • MEDIAN • 2.24 • STD DEV • 0.27 • RANGE • 1.14 TO 2.34 WITH 33 SAMPLES

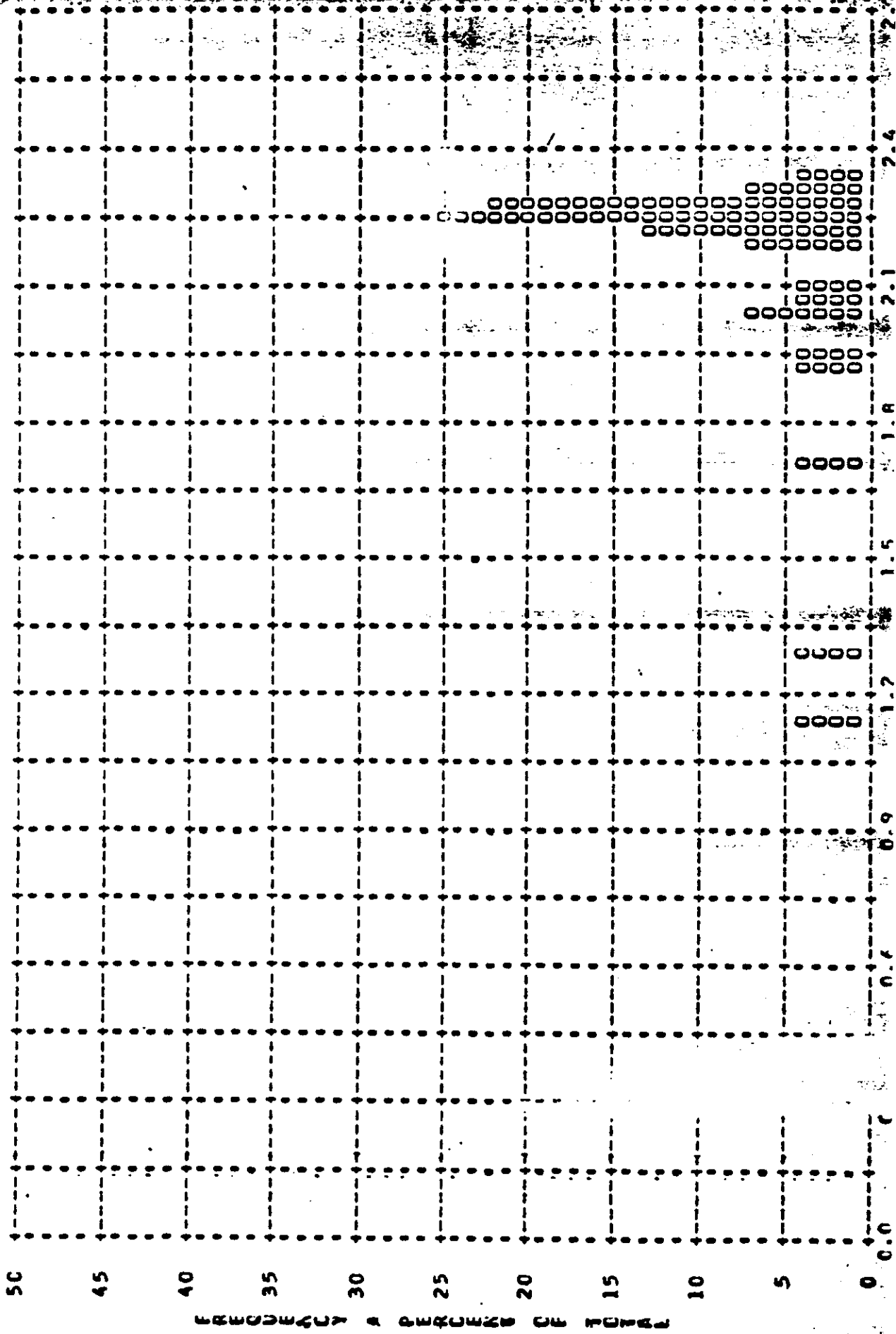


FIGURE 9-21

MISSION • ICIC-2 • INSTR • FND • 2-09-64 PLCT OF D MIN • TERRAIN • PROCESSING • FULL
ARITH MEAN • 0.54 • PECIAN • C.49 • STD DEV • 0.21 • RANGE • 0.26 TO 1.51 WITH 223 SAMPLES

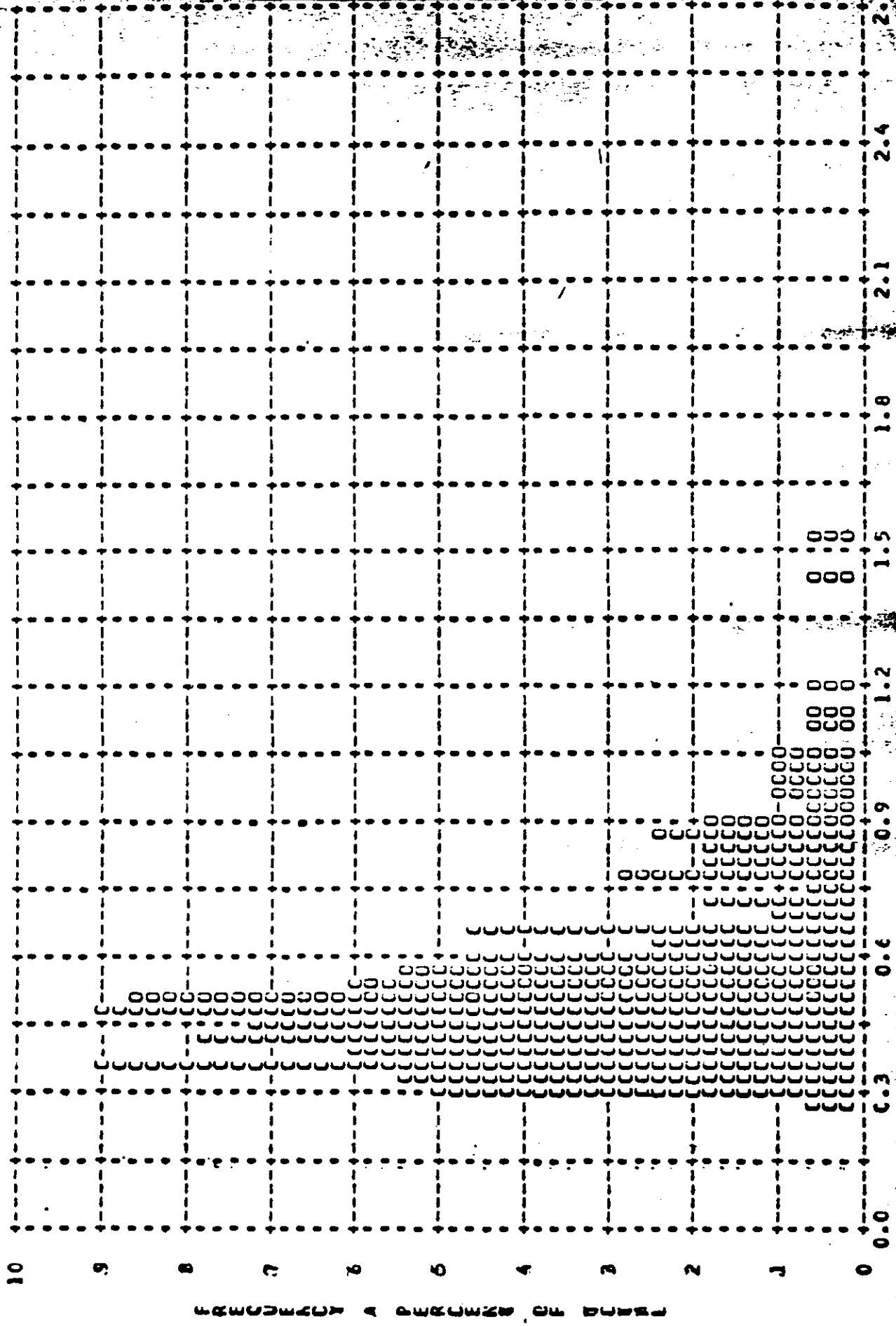
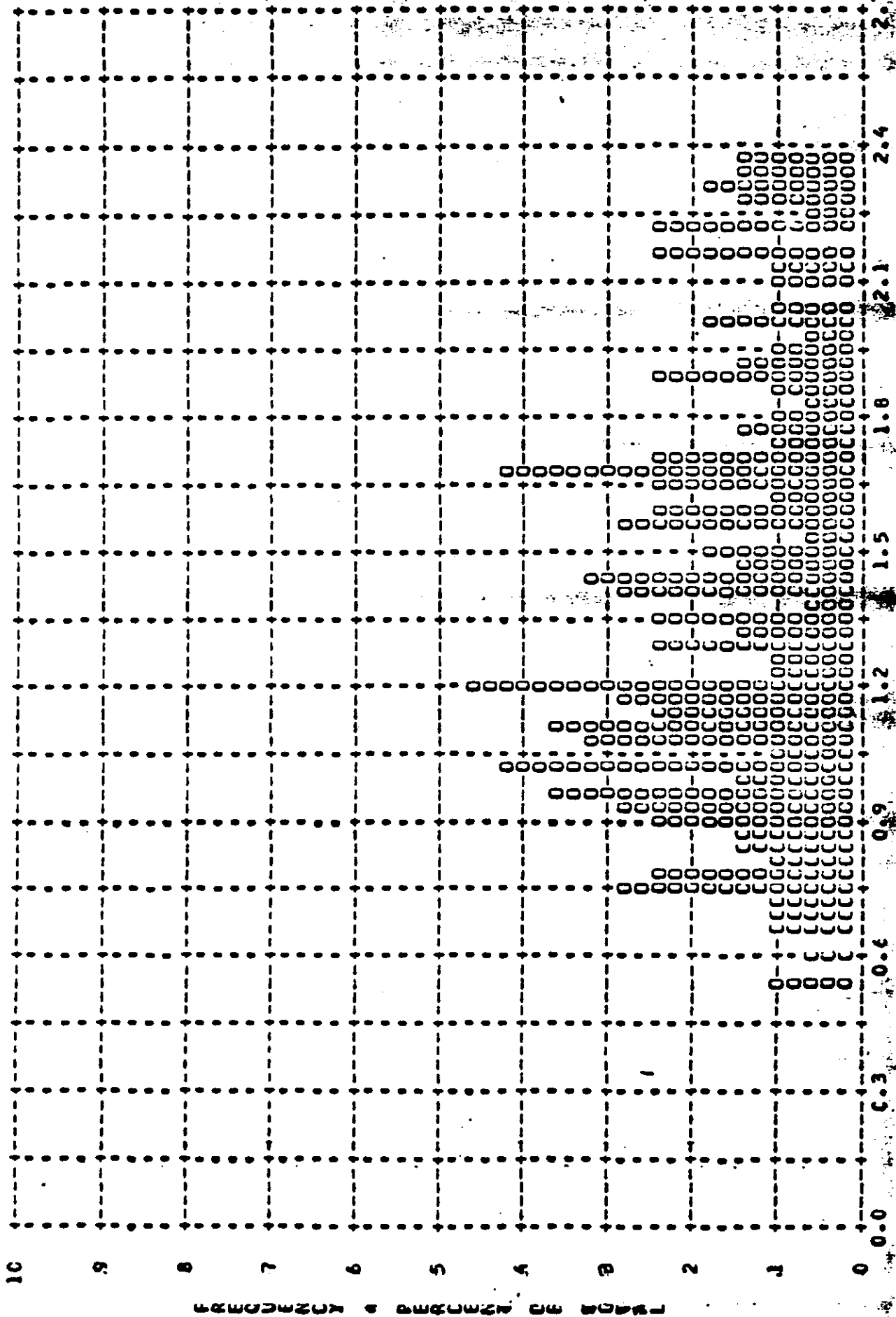


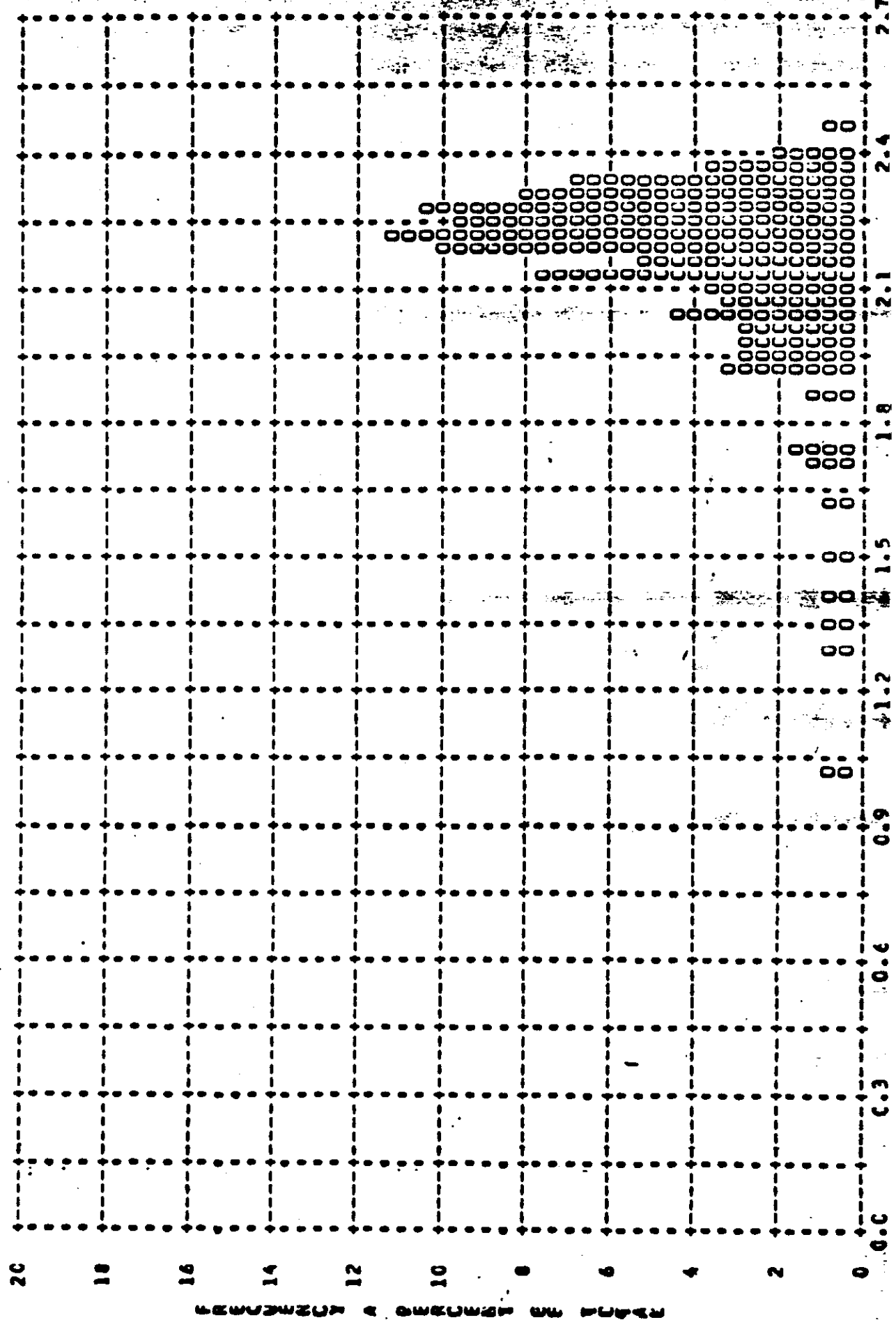
FIGURE 9-22

MISSICN • ICIC-2 • INSTR • FND • 2-09-64 PLOT OF D MAX • TERRAIN • PROCESSING • FULL
BRITH PEAN • 1.40 • PECIAN • 1.34 • STD DEV • C.47 • RANGE • 0.52 TO 2.36 WITH 223 SAMPLES





MISSION • ICIC-2 • INSTR • FND • 2-09-64 PLCT OF D MAX • CLOUD • PROCESSING • FULL
ORITH MEAN • 2.15 • MEDIAN • 2.20 • STD DEV • 0.20 • RANGE • 1.00 TO 2.44 WITH 206 SAMPLES



MISSICA • ICIC-2 • INSTR • FND • 2-09-64 PLOT OF D MIN • TERRAIN • PROCESSING • ALL LEVELS
ARITH MEAN • 0.55 • PECIAN • C.50 • STD DEV • 0.21 • RANGE • 0.26 TO 1.51 WITH 257 SAMPLES

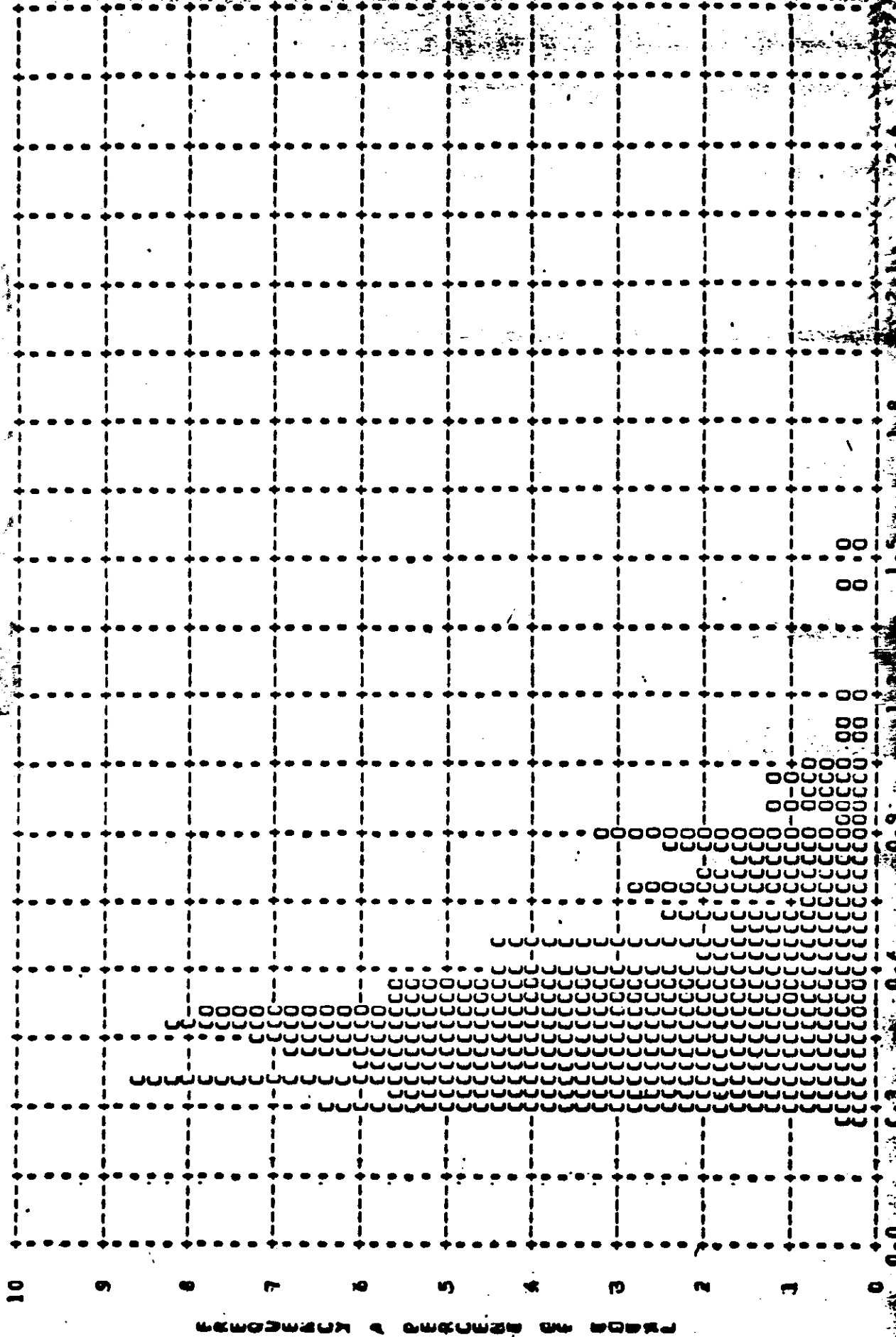


FIGURE 9-25

MISSION • ICIC-2 • INSTR • FWD • 2-09-64 PLOT OF D MAX • TERRAIN • PROCESSING • ALL LEVELS
 BRIT: PEAK • 1.41 • MEDIAN • 1.38 • STD DEV • 0.47 • RANGE • 0.52 TO 2.36 WITH 257 SAMPLES

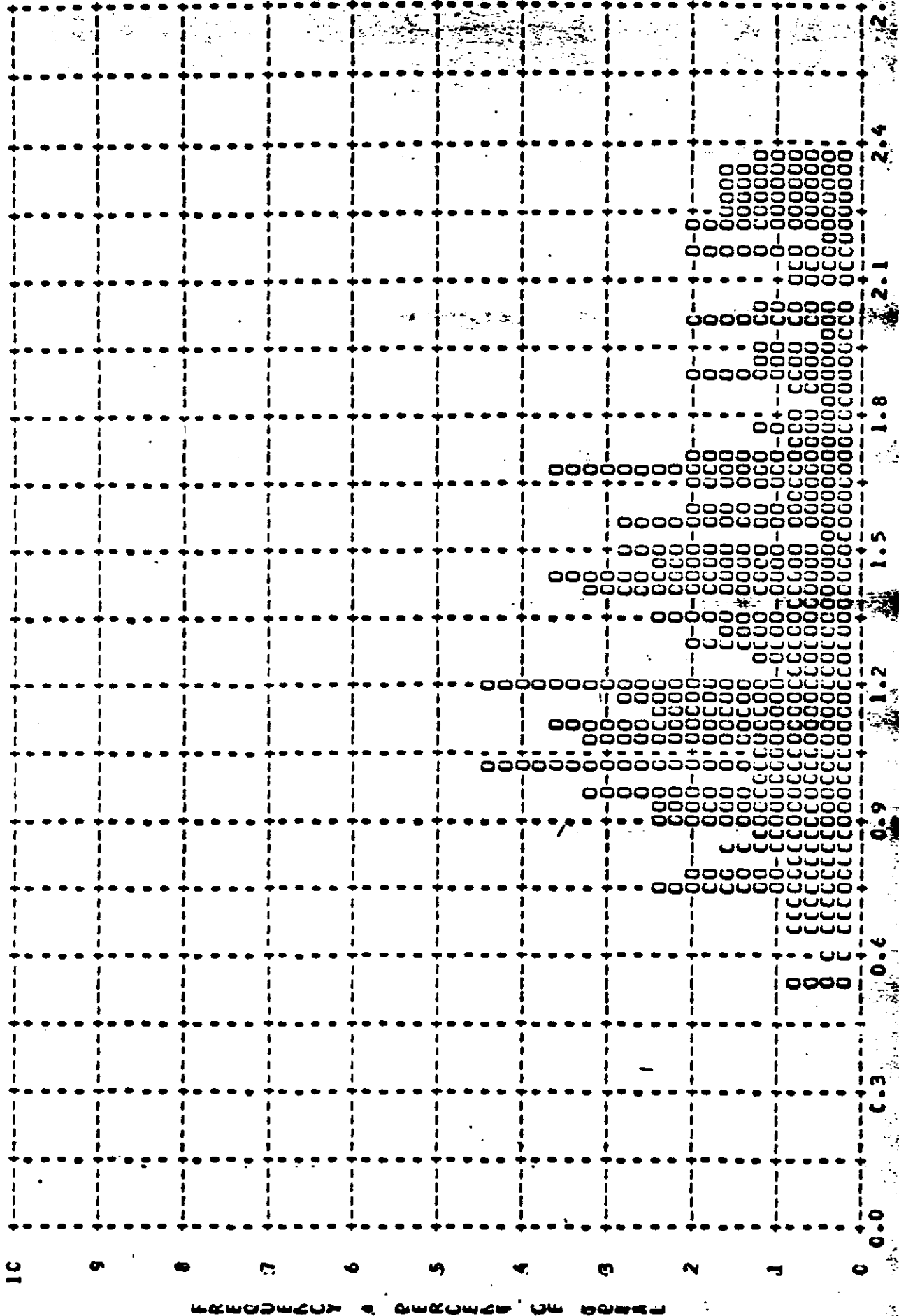
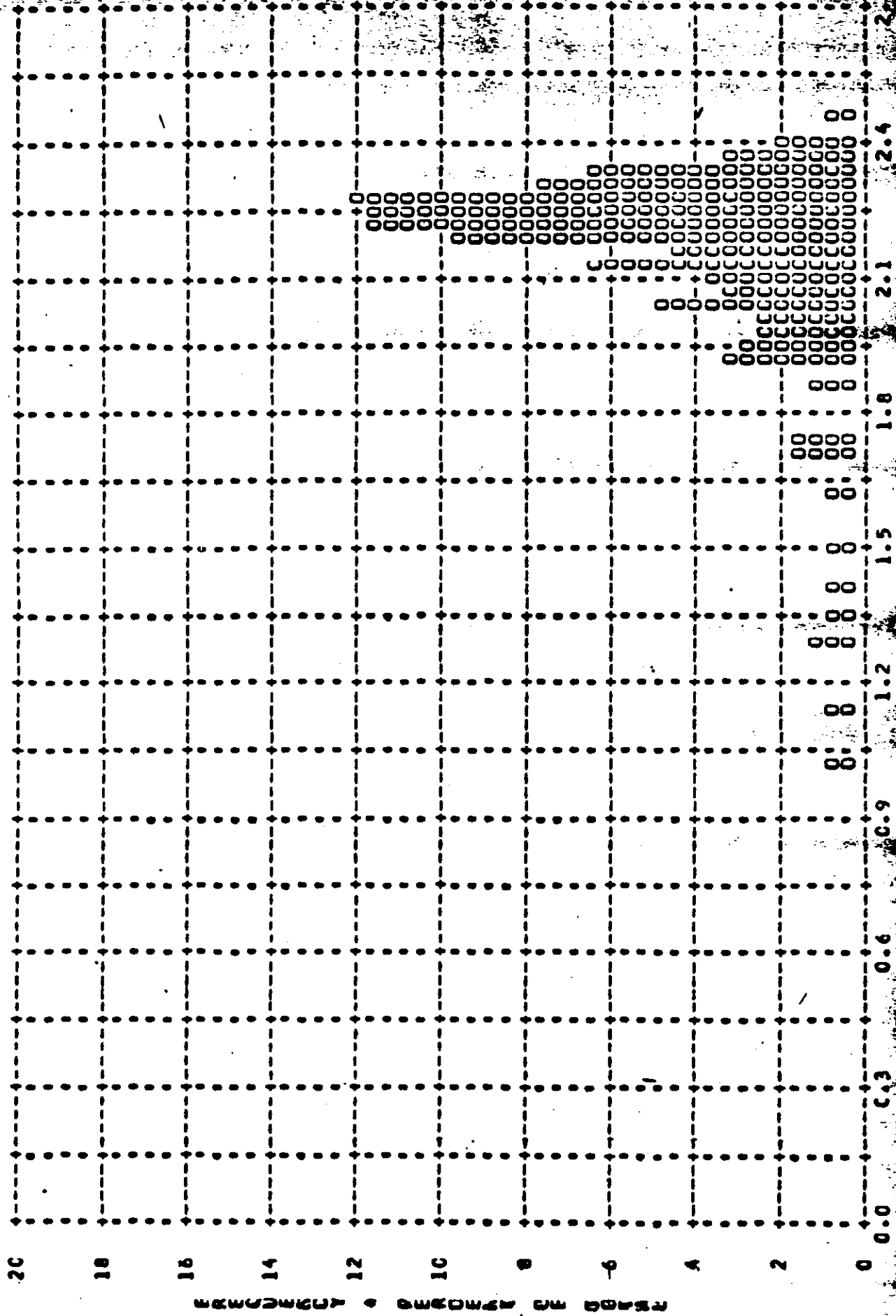


FIGURE 9-26

MISSICA • 1010-2 • INSTR • FWD • 2-09-64 PLOT OF D MAX • CLOUD • PROCESSING • ALL LEVELS
WITH PEAK • 2.14 • MEDIAN • 2.20 • STD DEV • 0.21 • RANGE • 1.00 TO 2.44 WITH 239 SAMPLES



MISSICA • 1010-2

• INSTRUMENT • AFT

2-09-64

DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY		INTERMEDIATE			FULL		ALL LEVELS		
	MIN	MAX LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX LIM
C.01	0	0	0	0	0	0	0	0	0	0
C.02	0	0	0	0	0	0	0	0	0	0
C.03	0	0	0	0	0	0	0	0	0	0
C.04	0	0	0	0	0	0	0	0	0	0
C.05	0	0	0	0	0	0	0	0	0	0
C.06	0	0	0	0	0	0	0	0	0	0
C.07	0	0	0	0	0	0	0	0	0	0
C.08	0	0	0	0	0	0	0	0	0	0
C.09	0	0	0	0	0	0	0	0	0	0
C.10	0	0	0	0	0	0	0	0	0	0
C.11	0	0	0	0	0	0	0	0	0	0
C.12	0	0	0	0	0	0	0	0	0	0
C.13	0	0	0	0	0	0	0	0	0	0
C.14	0	0	0	0	0	0	0	0	0	0
C.15	0	0	0	0	0	0	0	0	0	0
C.16	0	0	0	0	0	0	0	0	0	0
C.17	0	0	0	0	0	0	0	0	0	0
C.18	0	0	0	0	0	0	0	0	0	0
C.19	0	0	0	0	0	0	0	0	0	0
C.20	0	0	0	0	0	0	0	0	0	0
C.21	0	0	0	0	0	0	0	0	0	0
C.22	0	0	0	0	0	0	0	0	0	0
C.23	0	0	0	0	0	0	0	0	0	0
C.24	0	0	0	0	0	0	0	0	0	0
C.25	0	0	0	0	0	0	0	0	0	0
C.26	0	0	0	0	0	0	0	0	0	0
C.27	0	0	0	0	0	0	0	0	0	0
C.28	0	0	0	0	0	0	0	0	0	0
C.29	0	0	0	0	0	0	0	0	0	0
C.30	0	0	0	0	0	0	0	0	0	0
C.31	0	0	0	0	0	0	0	0	0	0
C.32	0	0	0	0	0	0	0	0	0	0
C.33	0	0	0	0	0	0	0	0	0	0
C.34	0	0	0	0	0	0	0	0	0	0
C.35	0	0	0	0	0	0	0	0	0	0
C.36	0	0	0	0	0	0	0	0	0	0
C.37	0	0	0	0	0	0	0	0	0	0
C.38	0	0	0	0	0	0	0	0	0	0
C.39	0	0	0	0	0	0	0	0	0	0
C.40	0	0	0	0	0	0	0	0	0	0
C.41	0	0	0	0	0	0	0	0	0	0
C.42	0	0	0	0	0	0	0	0	0	0
C.43	0	0	0	0	0	0	0	0	0	0
C.44	0	0	0	0	0	0	0	0	0	0
C.45	0	0	0	0	0	0	0	0	0	0
C.46	0	0	0	0	0	0	0	0	0	0
C.47	0	0	0	0	0	0	0	0	0	0
C.48	0	0	0	0	0	0	0	0	0	0
C.49	0	0	0	0	0	0	0	0	0	0
C.50	0	0	0	0	0	0	0	0	0	0
C.51	0	0	0	0	0	0	0	0	0	0
C.52	0	0	0	0	0	0	0	0	0	0
C.53	0	0	0	0	0	0	0	0	0	0
C.54	0	0	0	0	0	0	0	0	0	0
C.55	0	0	0	0	0	0	0	0	0	0
C.56	0	0	0	0	0	0	0	0	0	0
C.57	0	0	0	0	0	0	0	0	0	0
C.58	0	0	0	0	0	0	0	0	0	0
C.59	0	0	0	0	0	0	0	0	0	0
C.60	0	0	0	0	0	0	0	0	0	0
C.61	0	0	0	0	0	0	0	0	0	0
C.62	0	0	0	0	0	0	0	0	0	0
C.63	0	0	0	0	0	0	0	0	0	0
C.64	0	0	0	0	0	0	0	0	0	0
C.65	0	0	0	0	0	0	0	0	0	0
C.66	0	0	0	0	0	0	0	0	0	0
C.67	0	0	0	0	0	0	0	0	0	0
C.68	0	0	0	0	0	0	0	0	0	0
C.69	0	0	0	0	0	0	0	0	0	0
C.70	0	0	0	0	0	0	0	0	0	0
C.71	0	0	0	0	0	0	0	0	0	0
C.72	0	0	0	0	0	0	0	0	0	0
C.73	0	0	0	0	0	0	0	0	0	0
C.74	0	0	0	0	0	0	0	0	0	0
C.75	0	0	0	0	0	0	0	0	0	0
C.76	0	0	0	0	0	0	0	0	0	0
C.77	0	0	0	0	0	0	0	0	0	0
C.78	0	0	0	0	0	0	0	0	0	0
C.79	0	0	0	0	0	0	0	0	0	0
C.80	0	0	0	0	0	0	0	0	0	0
C.81	0	0	0	0	0	0	0	0	0	0
C.82	0	0	0	0	0	0	0	0	0	0
C.83	0	0	0	0	0	0	0	0	0	0
C.84	0	0	0	0	0	0	0	0	0	0
C.85	0	0	0	0	0	0	0	0	0	0
C.86	0	0	0	0	0	0	0	0	0	0
C.87	0	0	0	0	0	0	0	0	0	0
C.88	0	0	0	0	0	0	0	0	0	0
C.89	0	0	0	0	0	0	0	0	0	0
C.90	0	0	0	0	0	0	0	0	0	0
C.91	0	0	0	0	0	0	0	0	0	0
C.92	0	0	0	0	0	0	0	0	0	0
C.93	0	0	0	0	0	0	0	0	0	0
C.94	0	0	0	0	0	0	0	0	0	0
C.95	0	0	0	0	0	0	0	0	0	0
C.96	0	0	0	0	0	0	0	0	0	0
C.97	0	0	0	0	0	0	0	0	0	0
C.98	0	0	0	0	0	0	0	0	0	0
C.99	0	0	0	0	0	0	0	0	0	0
C.100	0	0	0	0	0	0	0	0	0	0
SUBTOTAL	0	0	0	0	0	0	0	0	0	0

TABLE 9-6

MISSICA • IC1C-2 • INSTRUMENT • AFT 2-09-64 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
1.001												
1.002												
1.003												
1.004												
1.005												
1.006												
1.007												
1.008												
1.009												
1.010												
1.011												
1.012												
1.013												
1.014												
1.015												
1.016												
1.017												
1.018												
1.019												
1.020												
1.021												
1.022												
1.023												
1.024												
1.025												
1.026												
1.027												
1.028												
1.029												
1.030												
1.031												
1.032												
1.033												
1.034												
1.035												
1.036												
1.037												
1.038												
1.039												
1.040												
1.041												
1.042												
1.043												
1.044												
1.045												
1.046												
1.047												
1.048												
1.049												
1.050												
1.051												
1.052												
1.053												
1.054												
1.055												
1.056												
1.057												
1.058												
1.059												
1.060												
1.061												
1.062												
1.063												
1.064												
1.065												
1.066												
1.067												
1.068												
1.069												
1.070												
1.071												
1.072												
1.073												
1.074												
1.075												
1.076												
1.077												
1.078												
1.079												
1.080												
1.081												
1.082												
1.083												
1.084												
1.085												
1.086												
1.087												
1.088												
1.089												
1.090												
1.091												
1.092												
1.093												
1.094												
1.095												
1.096												
1.097												
1.098												
1.099												
1.100												

SLBTICIAL

TABLE 9-6

MISSION • 1010-2

• INSTRUMENT • AFT

2-09-64

DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS			
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	
1.51	C	C	0	C	0	0	0	1	0	0	0	1	0
1.52	C	C	0	C	0	0	0	1	0	0	0	1	0
1.53	C	C	0	C	0	0	0	1	0	0	0	1	0
1.54	C	C	0	C	0	0	0	1	0	0	0	1	0
1.55	C	C	0	C	0	0	0	1	0	0	0	1	0
1.56	C	C	0	C	0	0	0	1	0	0	0	1	0
1.57	C	C	0	C	0	0	0	1	0	0	0	1	0
1.58	C	C	0	C	0	0	0	1	0	0	0	1	0
1.59	C	C	0	C	0	0	0	1	0	0	0	1	0
1.60	C	C	0	C	0	0	0	1	0	0	0	1	0
1.61	C	C	0	C	0	0	0	1	0	0	0	1	0
1.62	C	C	0	C	0	0	0	1	0	0	0	1	0
1.63	C	C	0	C	0	0	0	1	0	0	0	1	0
1.64	C	C	0	C	0	0	0	1	0	0	0	1	0
1.65	C	C	0	C	0	0	0	1	0	0	0	1	0
1.66	C	C	0	C	0	0	0	1	0	0	0	1	0
1.67	C	C	0	C	0	0	0	1	0	0	0	1	0
1.68	C	C	0	C	0	0	0	1	0	0	0	1	0
1.69	C	C	0	C	0	0	0	1	0	0	0	1	0
1.70	C	C	0	C	0	0	0	1	0	0	0	1	0
1.71	C	C	0	C	0	0	0	1	0	0	0	1	0
1.72	C	C	0	C	0	0	0	1	0	0	0	1	0
1.73	C	C	0	C	0	0	0	1	0	0	0	1	0
1.74	C	C	0	C	0	0	0	1	0	0	0	1	0
1.75	C	C	0	C	0	0	0	1	0	0	0	1	0
1.76	C	C	0	C	0	0	0	1	0	0	0	1	0
1.77	C	C	0	C	0	0	0	1	0	0	0	1	0
1.78	C	C	0	C	0	0	0	1	0	0	0	1	0
1.79	C	C	0	C	0	0	0	1	0	0	0	1	0
1.80	C	C	0	C	0	0	0	1	0	0	0	1	0
1.81	C	C	0	C	0	0	0	1	0	0	0	1	0
1.82	C	C	0	C	0	0	0	1	0	0	0	1	0
1.83	C	C	0	C	0	0	0	1	0	0	0	1	0
1.84	C	C	0	C	0	0	0	1	0	0	0	1	0
1.85	C	C	0	C	0	0	0	1	0	0	0	1	0
1.86	C	C	0	C	0	0	0	1	0	0	0	1	0
1.87	C	C	0	C	0	0	0	1	0	0	0	1	0
1.88	C	C	0	C	0	0	0	1	0	0	0	1	0
1.89	C	C	0	C	0	0	0	1	0	0	0	1	0
1.90	C	C	0	C	0	0	0	1	0	0	0	1	0
1.91	C	C	0	C	0	0	0	1	0	0	0	1	0
1.92	C	C	0	C	0	0	0	1	0	0	0	1	0
1.93	C	C	0	C	0	0	0	1	0	0	0	1	0
1.94	C	C	0	C	0	0	0	1	0	0	0	1	0
1.95	C	C	0	C	0	0	0	1	0	0	0	1	0
1.96	C	C	0	C	0	0	0	1	0	0	0	1	0
1.97	C	C	0	C	0	0	0	1	0	0	0	1	0
1.98	C	C	0	C	0	0	0	1	0	0	0	1	0
1.99	C	C	0	C	0	0	0	1	0	0	0	1	0
2.00	C	C	0	C	0	0	0	1	0	0	0	1	0
SUBTOTAL	C	C	0	C	27	10	0	48	25	1	0	75	31

TABLE 9-6

MISSICA • 1010-2

• INSTRUMENT • AFT

2-09-64

DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			FULL			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.01			0			0			0			0
2.02			0			0			0			0
2.03			0			0			0			0
2.04			0			0			0			0
2.05			0			0			0			0
2.06			0			0			0			0
2.07			0			0			0			0
2.08			0			0			0			0
2.09			0			0			0			0
2.10			0			0			0			0
2.11			0			0			0			0
2.12			0			0			0			0
2.13			0			0			0			0
2.14			0			0			0			0
2.15			0			0			0			0
2.16			0			0			0			0
2.17			0			0			0			0
2.18			0			0			0			0
2.19			0			0			0			0
2.20			0			0			0			0
2.21			0			0			0			0
2.22			0			0			0			0
2.23			0			0			0			0
2.24			0			0			0			0
2.25			0			0			0			0
2.26			0			0			0			0
2.27			0			0			0			0
2.28			0			0			0			0
2.29			0			0			0			0
2.30			0			0			0			0
2.31			0			0			0			0
2.32			0			0			0			0
2.33			0			0			0			0
2.34			0			0			0			0
2.35			0			0			0			0
2.36			0			0			0			0
2.37			0			0			0			0
2.38			0			0			0			0
2.39			0			0			0			0
2.40			0			0			0			0
2.41			0			0			0			0
2.42			0			0			0			0
2.43			0			0			0			0
2.44			0			0			0			0
2.45			0			0			0			0
2.46			0			0			0			0
2.47			0			0			0			0
2.48			0			0			0			0
2.49			0			0			0			0
2.50			0			0			0			0
SUBTOTAL			0			0			0			0
TOTAL			0			0			0			0

TABLE 9-6

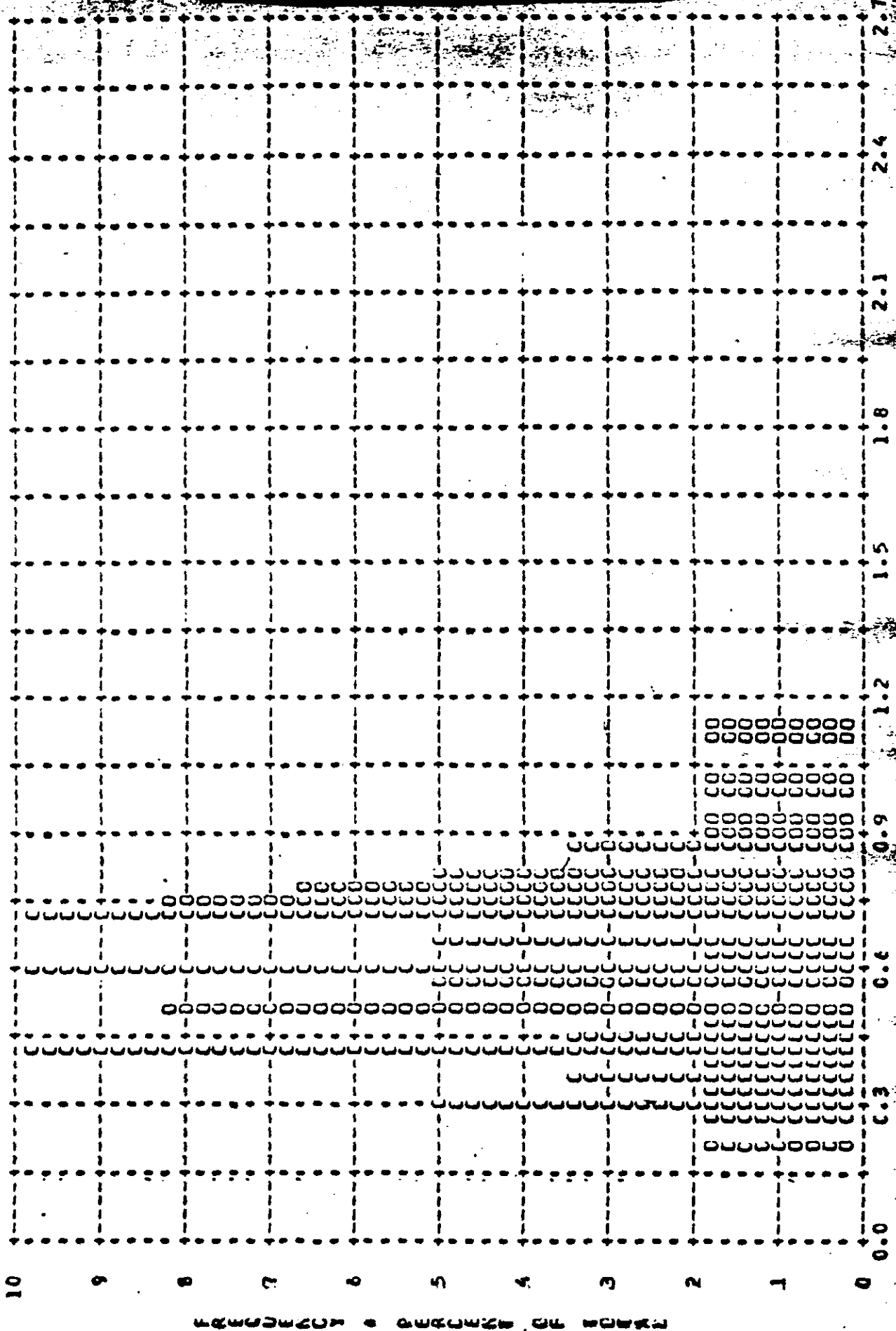
MISSION • 1010-2 • INSTRUMENT • AFT 2-C 64 DENSITY FREQ DISTR

DENSITY VALUE	PRIMARY			INTERMEDIATE			L			ALL LEVELS		
	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM	MIN	MAX	LIM
2.51	C	C	0	C	C	0	0		0	0	0	0
2.52	C	C	0	C	C	0	0		0	0	0	0
2.53	C	C	0	C	C	0	0		0	0	0	0
2.54	C	C	0	C	C	0	0		0	0	0	0
2.55	C	C	0	C	C	0	0		0	0	0	0
2.56	C	C	0	C	C	0	0		0	0	0	0
2.57	C	C	0	C	C	0	0		0	0	0	0
2.58	C	C	0	C	C	0	0		0	0	0	0
2.59	C	C	0	C	C	0	0		0	0	0	0
2.60	C	C	0	C	C	0	0		0	0	0	0
2.61	C	C	0	C	C	0	0		0	0	0	0
2.62	C	C	0	C	C	0	0		0	0	0	0
2.63	C	C	0	C	C	0	0		0	0	0	0
2.64	C	C	0	C	C	0	0		0	0	0	0
2.65	C	C	0	C	C	0	0		0	0	0	0
2.66	C	C	0	C	C	0	0		0	0	0	0
2.67	C	C	0	C	C	0	0		0	0	0	0
2.68	C	C	0	C	C	0	0		0	0	0	0
2.69	C	C	0	C	C	0	0		0	0	0	0
2.70	C	C	0	C	C	0	0		0	0	0	0
SUBTOTAL	C	C	0	C	C	0	0	0	0	0	0	0
TOTAL	C	C	0	62	62	62	190	190	180	252	252	242

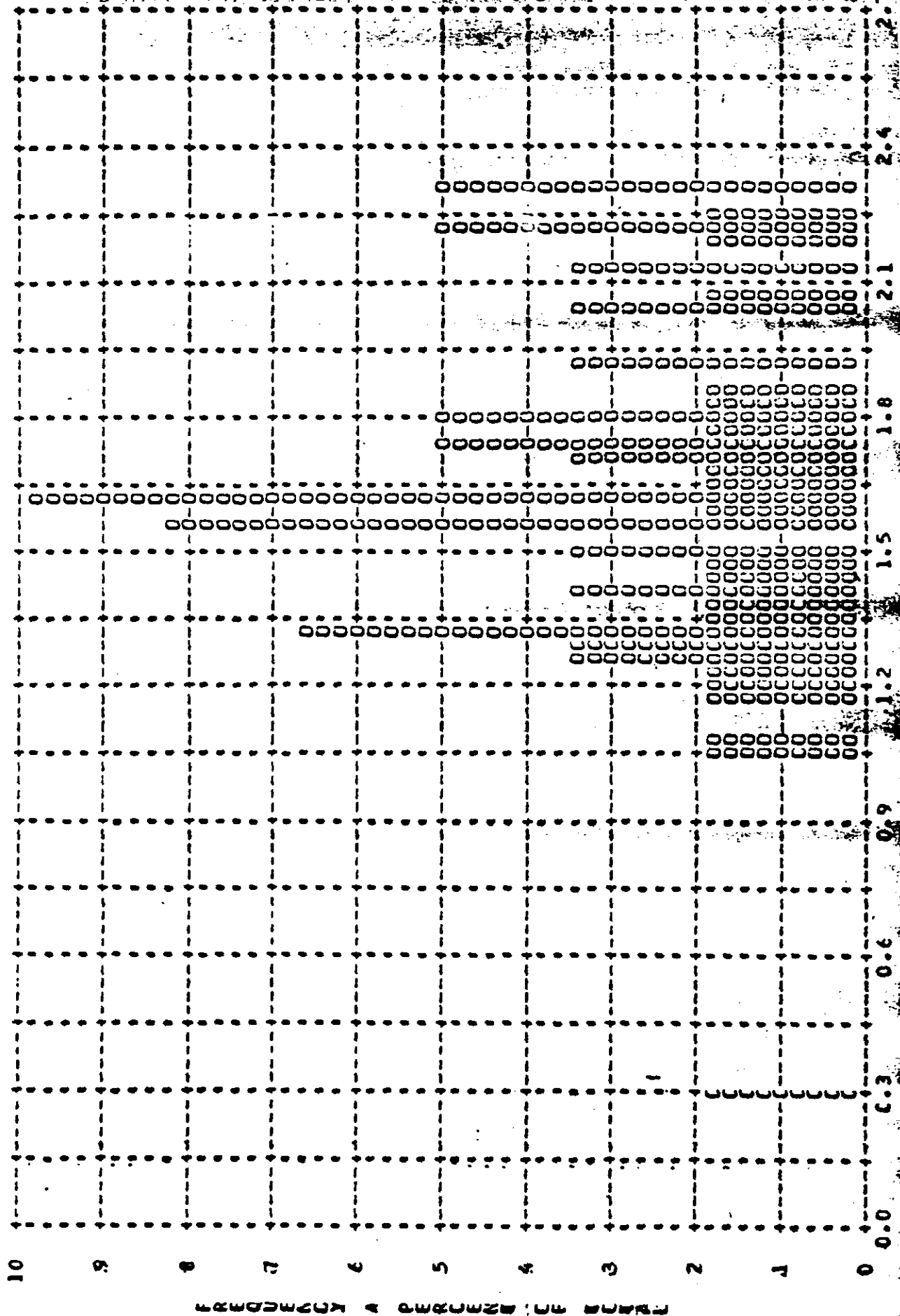
MISSION 1010-2		INSTR - AFT		2-09-64		PROCESSING AND EXPOSURE ANALYSIS				
PROCESS LEVEL	SAMPLE SIZE	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OV EXPOS				
PRIMARY	C	0 PC	0 PC	0 PC	0 PC	0				
INTERMEDIATE	62	2 PC	13 PC	77 PC	8 PC	0				
FULL	190	16 PC	0 PC	76 PC	8 PC	0				
ALL LEVELS	252	18 PC	3 PC	76 PC	8 PC	0				
PROCESS LEVEL	RANGE + PCG	UNDER EXPOSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OV EXPOS				
PRIMARY	C.01-C.15	C.01-C.13	0.14-0.39	0.40-0.90	-----	0.91 AN				
INTERMED	C.10-C.17	C.01-C.20	0.21-0.39	0.40-0.90	0.91-1.34	1.35 AN				
FULL	C.18 AND UP	C.01-C.39	-----	0.40-0.90	0.91-1.69	1.70 AN				

TABLE 9-6

MISSION • ICIG-2 • INSTR • AFI • 2-09-64 FLGT OF D MIN • TERRAIN • PROCESSING • INTERMEDIATE
 WITH PEAN • C.61 • PECIAL • C.60 • SID DLV • 0.2] • RANGE • 0.20 TO 1.14 WITH 62 SAMPLES



WIS61CN • ICIC-2 • INSTR • AIT • 2-09-64 PLOT OF D MAX • TERRAIN • PROCESSING • INTERMEDIATE
ARITH FEAR • 1.64 • FEELIAN • 1.60 • SID DEV • 0.38 • RANGE • 0.30 TO 2.30 WITH 62 SAMPLES



MISSION • ICIC-2 • INSTR • AFI • 2-09-64 PLOT OF D MAX • CLOUD • PROCESSING • INTERMEDIATE
 WRTIP PEAN • 2.14 • MEDIAN • 2.20 • STD DEV • 0.17 • RANGE • 1.56 TO 2.42 WITH 62 SAMPLES

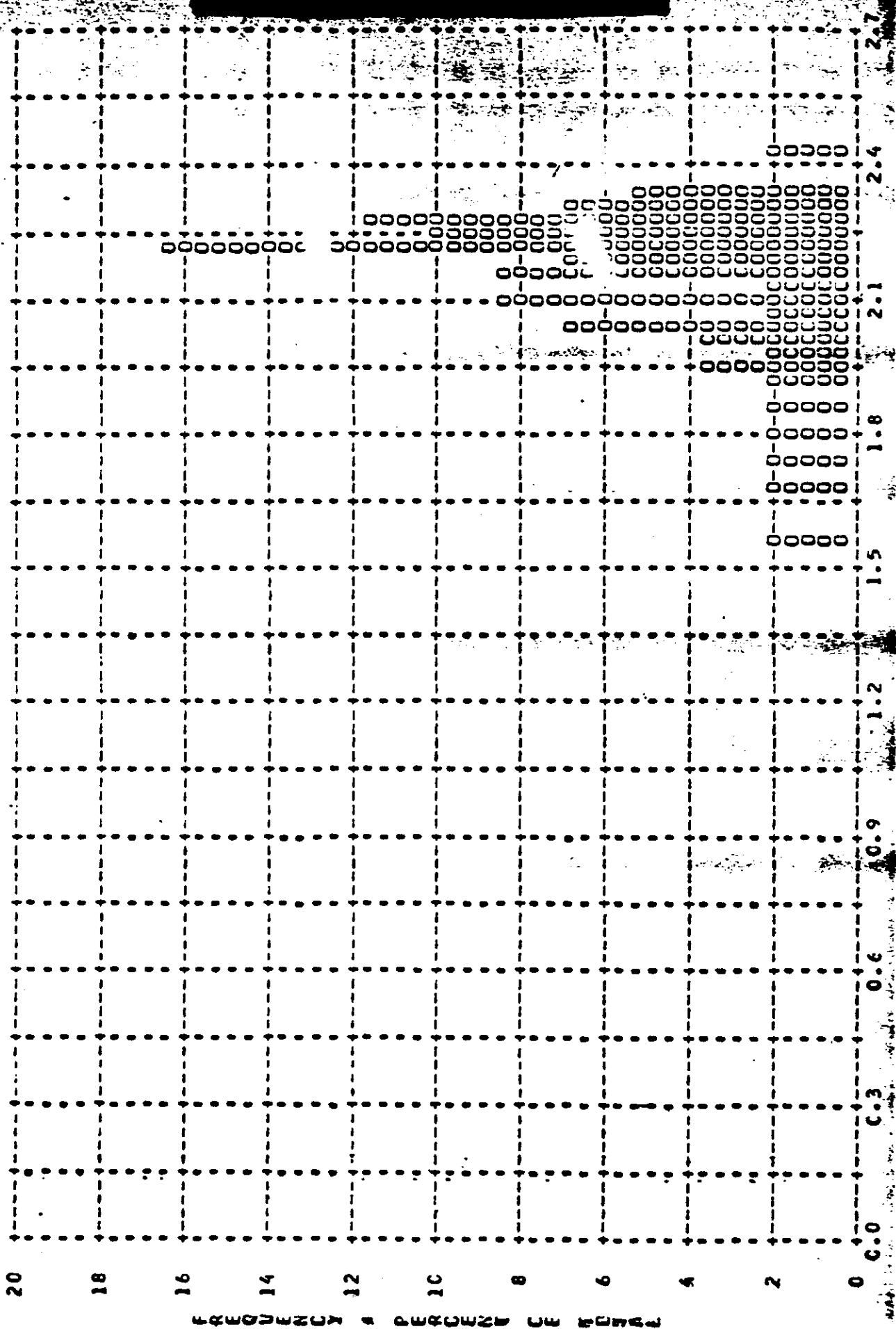


FIGURE 9-30

MISSICA • ICIC-2 • IASTR • AFT • 2-09-64 PLOT OF D MIN • TERRAIN • PROCESSING • FULL
WRITH PEAN • C.52 • PECIAN • C.55 • STD DEV • 0.21 • RANGE • 0.30 TO 1.48 WITH 190 SAMPLES

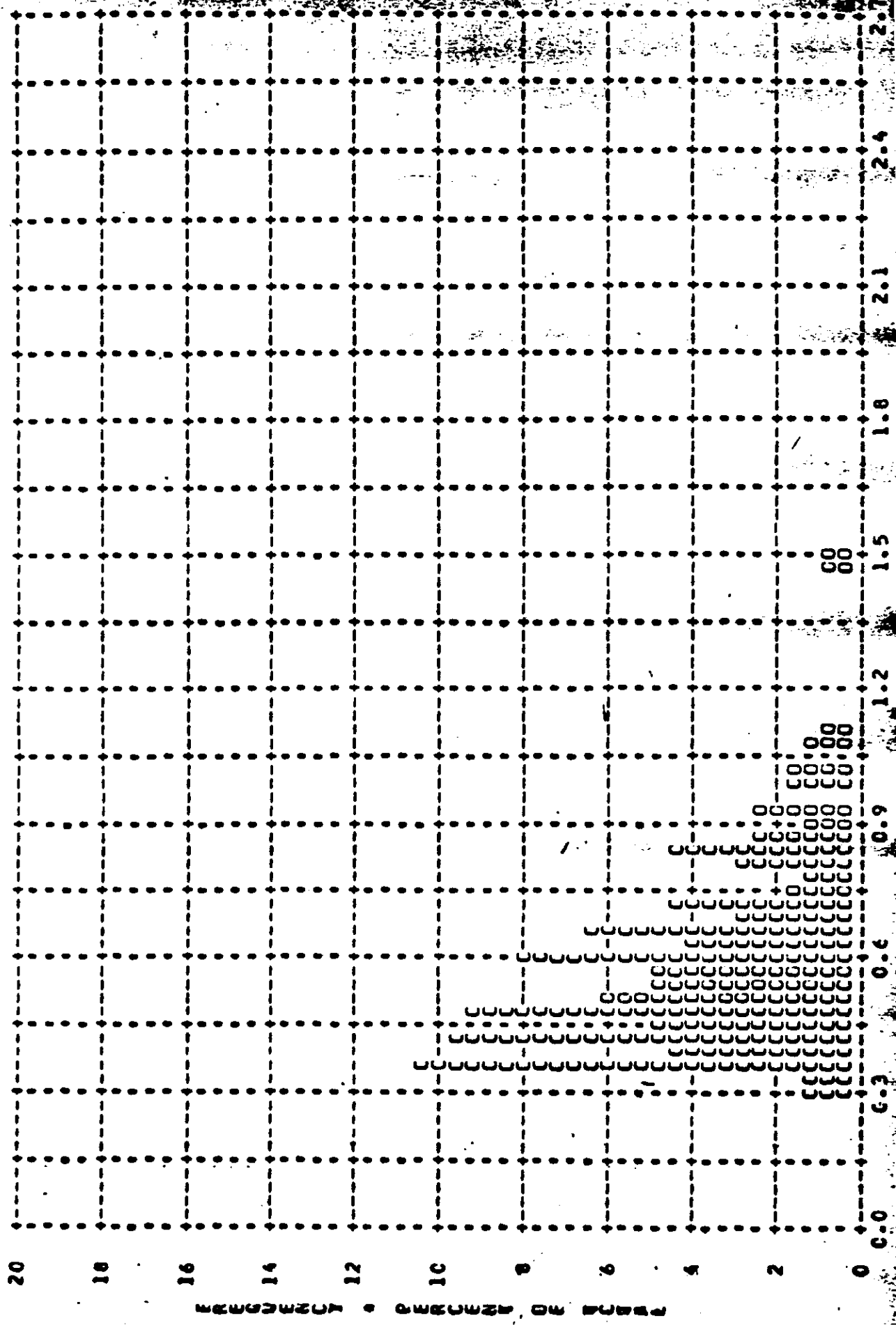
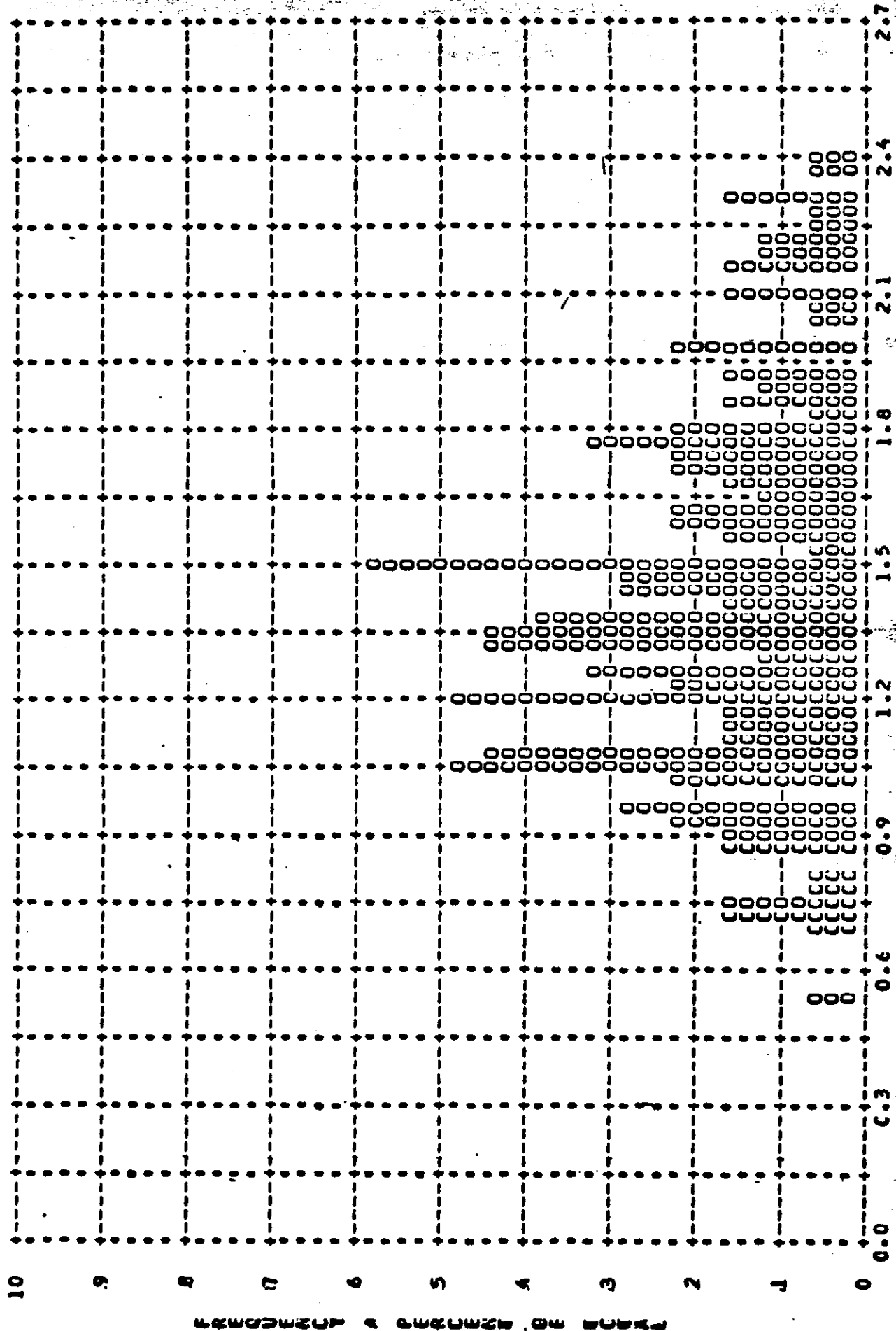


FIGURE 9-31

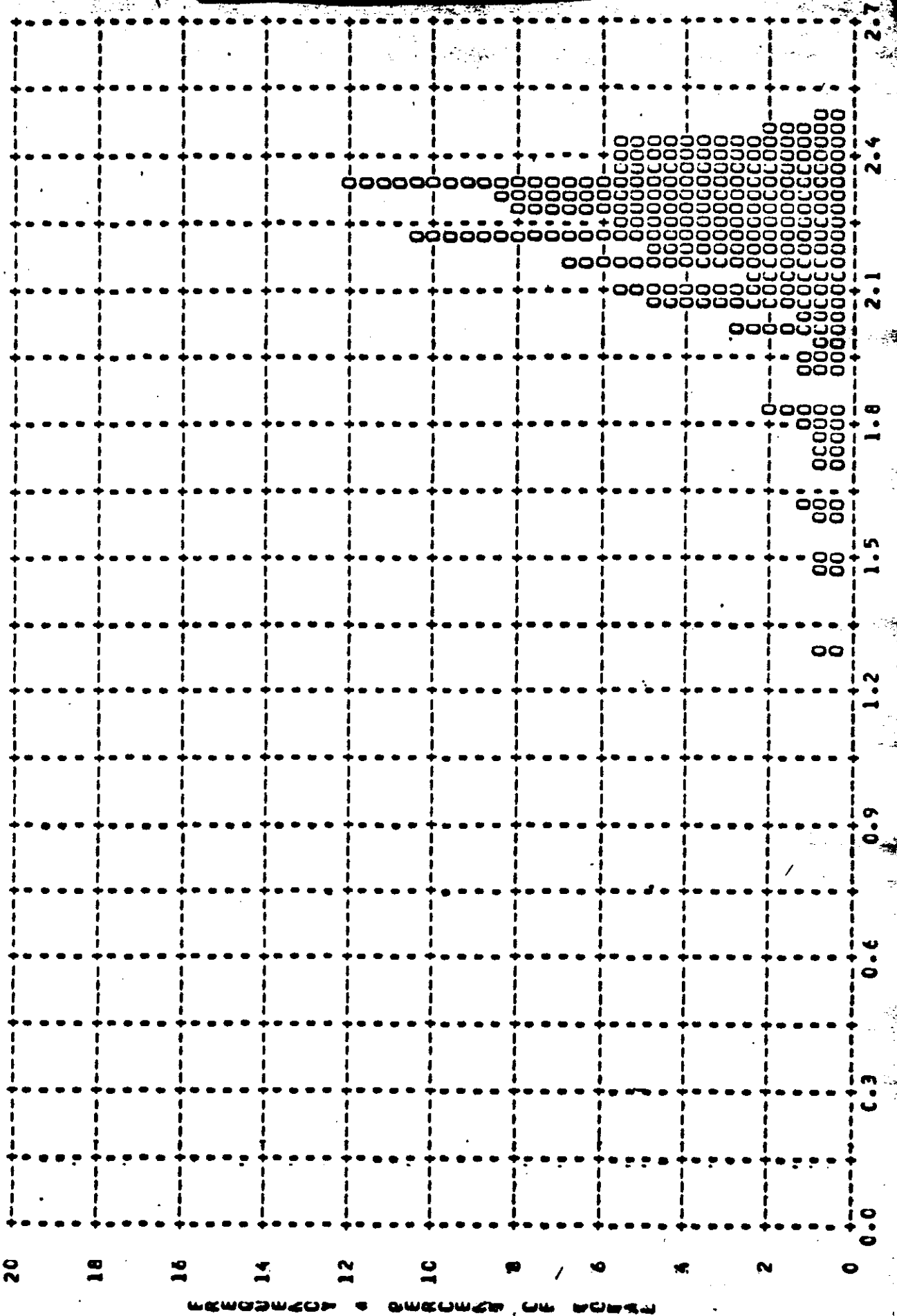
MIS61CN • IOIC-2 • INSTR • AFT • 2-09-64 PLOT OF D MAX • TERRAIN • PROCESSING • FULL
WRITH PEAN • 1.42 • PECIAN • 1.38 • STD DEV • 0.41 • RANGE • 0.52 TO 2.40 WITH 190 SAMPLES



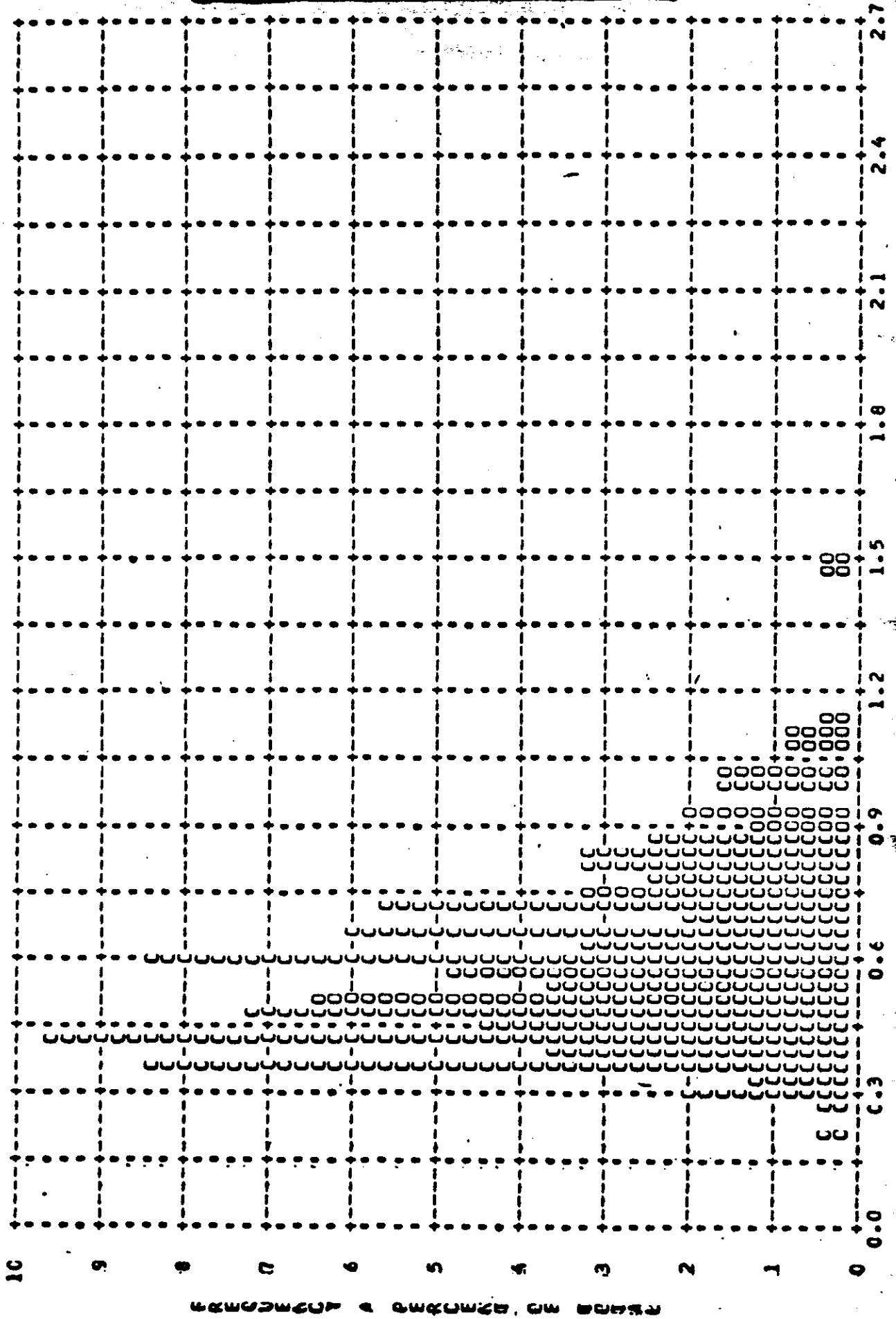
FREQUENCY • D MAX

FIGURE 9-32

MISSICA • ICIC-2 • INSTR • AFT • 2-09-64 PLCT OF D MAX • CLOUD • PROCESSING • FULL
ARITH MEAN • 2.15 • PECIAN • 2.24 • STD DEV • 0.20 • RANGE • 1.29 TO 2.48 WITH 180 SAMPLES



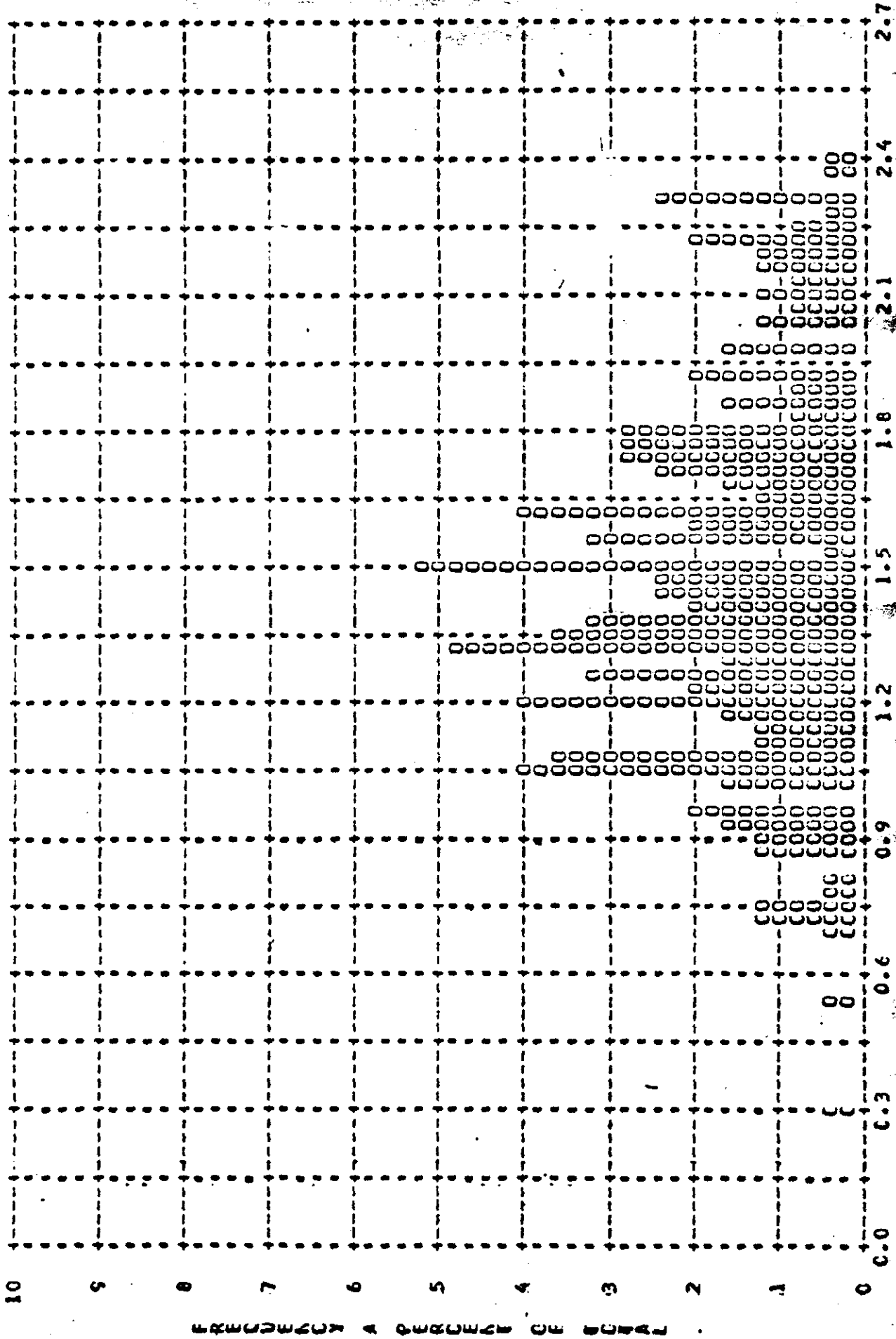
MIS61CN • ICIC-2 • INSTR • AFT • 2-09-64 PLOT OF 0 MIN • TERRAIN • PROCESSING • ALL LEVELS
MATH: PEAN • C.55 • MECIAN • C.56 • STD DEV • 0.21 • RANGE • 0.20 TO 1.48 WITH 252 SAMPLES



PLANTING AND GROWING OF TREES

FIGURE 9-34

MISSION • IOIC-2 • INSTR • AIT • 2-09-64 PLOT OF D MAX • TERRAIN • PROCESSING • ALL LEVELS
BRITH PEAK • 1.47 • PLECIAN • 1.45 • STD DEV • C.41 • RANGE • 0.30 TO 2.40 WITH 252 SAMPLES



MISSICA • ICIC-2 • INSTR • AFI • 2-09-64 PLOT OF D MAX • CLOUD • PROCESSING • ALL LEVELS
ARITH MEAN • 2.18 • MEDIAN • 2.22 • STD DEV • 0.19 • RANGE • 1.29 TO 2.48 WITH 242 SAMPLES

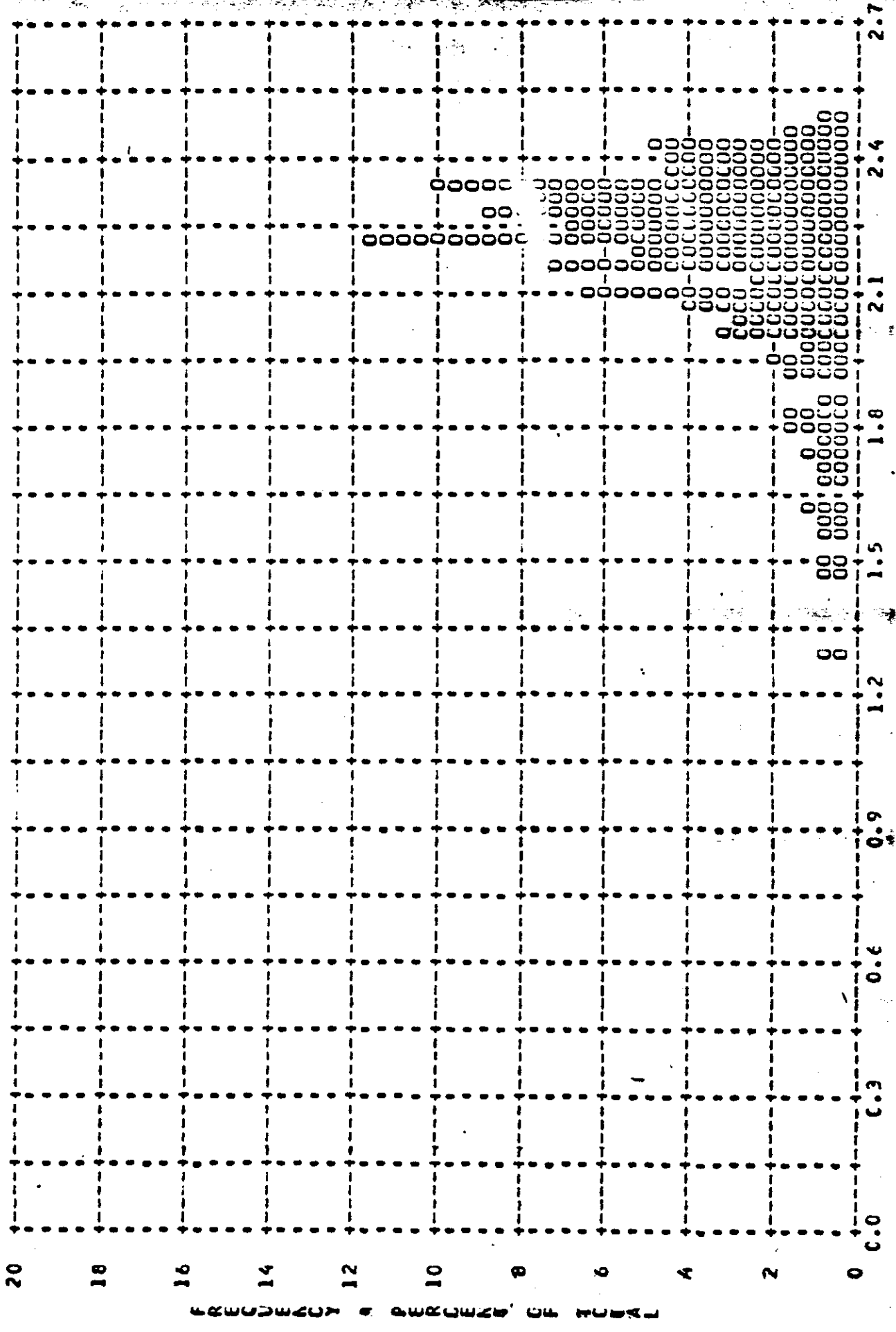


FIGURE 9-36

~~TOP SECRET~~

MISSION	ICIC-1	INSTR	- FWC	2-09-64	PROCESSING AND EXPOSURE ANALYSIS		
PROCESS LEVEL	SAMPLE SIZE	UNDER EXPCSEC	PRCESSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	C	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	23	0 PC	35 PC	0 PC	65 PC	0 PC	0 PC
FULL	224	20 PC	0 PC	0 PC	76 PC	4 PC	0 PC
ALL LEVELS	247	18 PC	3 PC	3 PC	75 PC	4 PC	0 PC

MISSION	ICIC-1	INSTR	- AFT	2-09-64	PROCESSING AND EXPOSURE ANALYSIS		
PROCESS LEVEL	SAMPLE SIZE	UNDER EXPCSEC	PRCESSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	C	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	4C	0 PC	27 PC	0 PC	67 PC	5 PC	0 PC
FULL	215	11 PC	0 PC	0 PC	83 PC	6 PC	0 PC
ALL LEVELS	255	5 PC	4 PC	4 PC	81 PC	6 PC	0 PC

MISSION	ICIC-2	INSTR	- FWC	2-09-64	PROCESSING AND EXPOSURE ANALYSIS		
PROCESS LEVEL	SAMPLE SIZE	UNDER EXPCSEC	PRCESSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	C	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	34	0 PC	32 PC	0 PC	62 PC	6 PC	0 PC
FULL	223	26 PC	0 PC	0 PC	68 PC	6 PC	0 PC
ALL LEVELS	257	22 PC	4 PC	4 PC	67 PC	6 PC	0 PC

MISSION	IOIO-2	INSTR	- AFT	2-09-64	PROCESSING AND EXPOSURE ANALYSIS		
PROCESS LEVEL	SAMPLE SIZE	UNDER EXPCSEC	PRCESSED	UNDER PROCESSED	CORRECT EXP+PROC	OVER PROCESSED	OVER EXPOSED
PRIMARY	C	0 PC	0 PC	0 PC	0 PC	0 PC	0 PC
INTERMEDIATE	62	2 PC	13 PC	0 PC	77 PC	8 PC	0 PC
FULL	15C	16 PC	0 PC	0 PC	76 PC	8 PC	0 PC
ALL LEVELS	252	13 PC	3 PC	3 PC	76 PC	8 PC	0 PC

TABLE 9-7

~~TOP SECRET~~

SECTION 10

PERFORMANCE MEASUREMENTS

The photography acquired by both panoramic cameras during Missions 1010-1 and 1010-2 received a MIP rating of 85. A summary is tabulated below of the average visual RES values and MTF/AIM resolution values measured by AFSPPL and the MTF/AIM resolution values made by [REDACTED]. The length of the microdensimeter slit used by AFSPPL was 350 and 80 microns whereas [REDACTED] used an 80 micron slit; both slits were one micron wide.

Mission	Camera	Visual RES	AFSPPL		[REDACTED]	
			350 μ	80 μ	All	High
1010-1	FWD	90	90	88	87	96
1010-1	AFT	88	86	80	92	103
1010-2	FWD	92	81	82	82	93
1010-2	AFT	90	82	85	87	98

The [REDACTED] data normally contains two readings of the same edge the tabulation shows both the average of all the readings and the average of the highest readings of each edge. The value of the average of all readings is questionable as no valid reason can be ascertained for a measurement being greater than the resolution recorded however many factors can reduce the reading.

The details of the measurement and computing techniques, targets measured and target locations are fully reported in the evaluation report published by AFSPPL and are not normally included in this report. [REDACTED] has recently completed the re-calculation of the MTF/AIM values from Mission 1007-2 and up. Since this data has not been published in a previous report the corrected measurements for Missions 1010-1 and 1010-2 are included in this report.

Analysis of Photographic Image to Evaluate System Performance

Mission 1010-1

Resolution in lines/mm based on the aerial image modulation - 4404 curve from edge trace data reduced by computer techniques.

Arithmetic Mean	89.4 l/mm
Standard Deviation	22.7 l/mm
Coefficient of Dispersion	25%
Number of Edges	119
M.I.P. Frame	134 l/mm

Spread function width at 50% amplitude in microns from edge trace data reduced by computer techniques.

Arithmetic Mean	9.8 μ
Standard Deviation	3.3 μ
Coefficient of Dispersion	33%
Number of Edges	119
M.I.P. Frame	5.3 μ

Analysis of Photographic Image to Evaluate System Performance

MISSION 1010-1

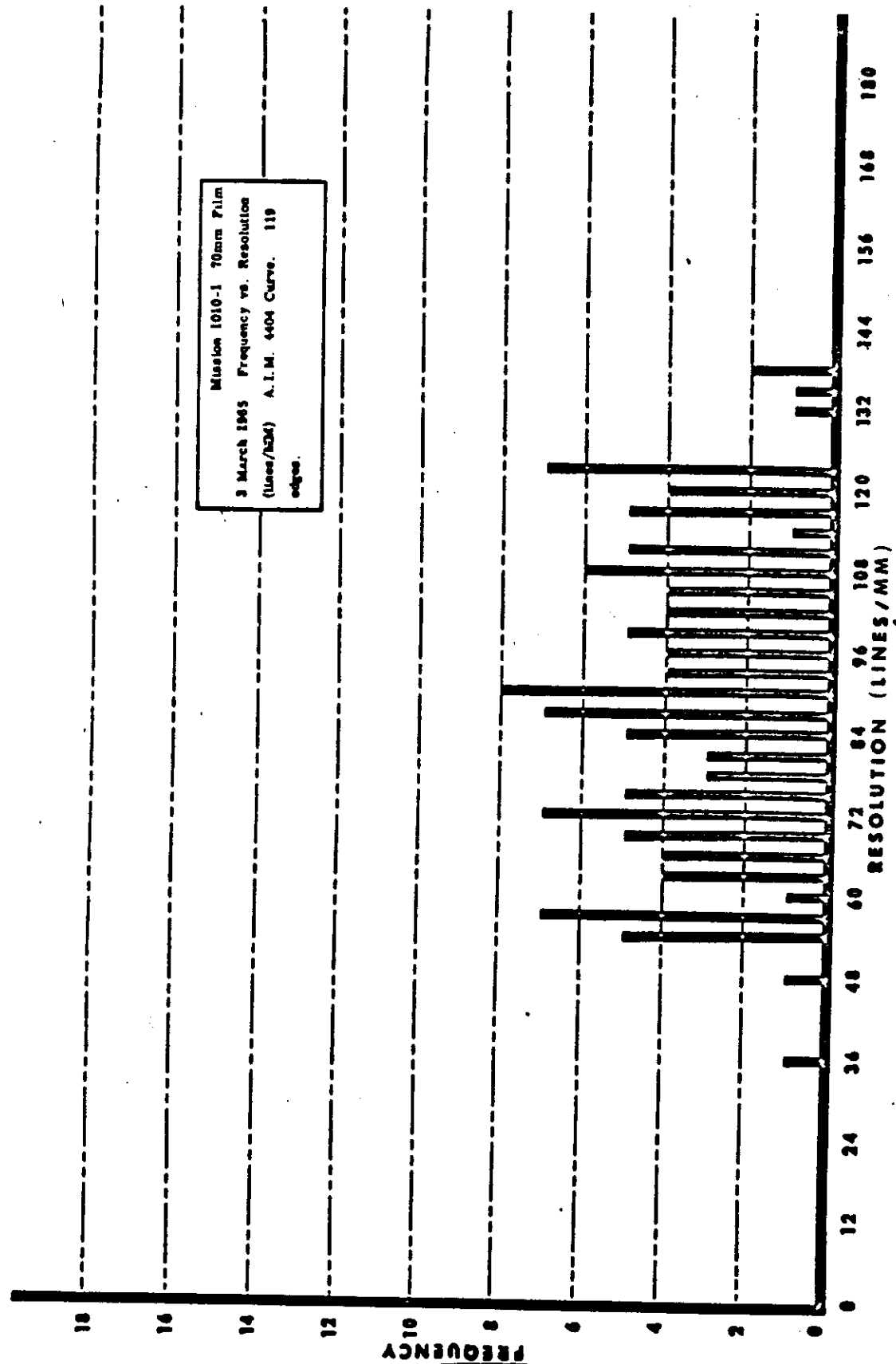
Resolution in lines/mm based on the aerial image modulation - 4404 curve from edge trace data reduced by computer techniques.

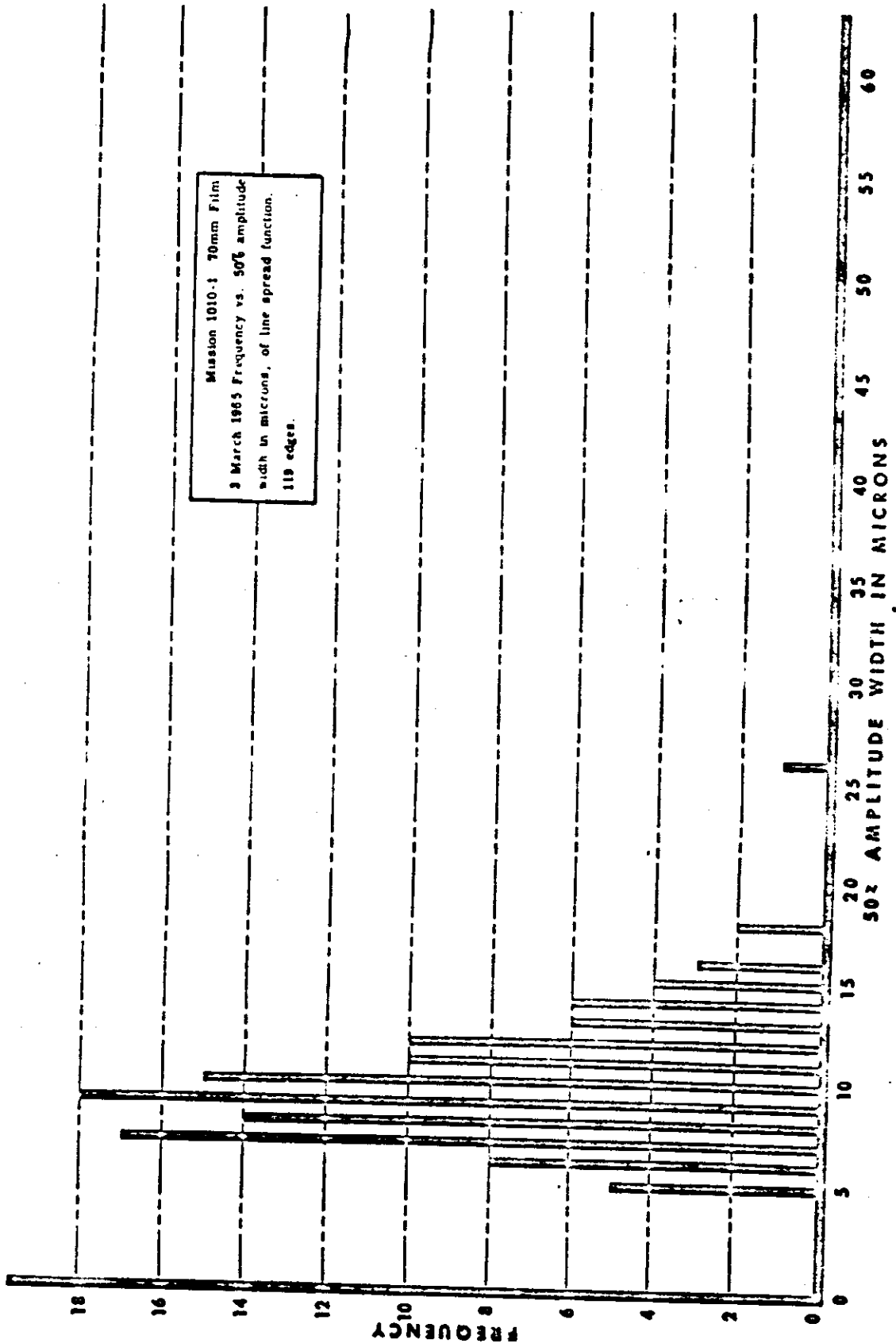
	FWD Camera	AFT Camera	Airfields	Buildings
Arithmetic Mean	87.1 l/mm	92.0 l/mm	87.6 l/mm	94.4 l/mm
Standard Deviation	21.4 l/mm	24.0 l/mm	23.0 l/mm	21.4 l/mm
Coefficient of Dispersion	25%	26%	26%	23%
Number of Edges	63	56	87	32

Spread function width at 50% amplitude in microns from edge trace data reduced by computer techniques.

	FWD Camera	AFT Camera	Airfields	Buildings
Arithmetic Mean	9.5 μ	10.2 μ	10.1 μ	9.3 μ
Standard Deviation	3.6 μ	2.8 μ	2.9 μ	4.1
Coefficient of Dispersion	38%	27%	29%	45%
Number of Edges	63	56	87	32

Mission 1010-1 70mm Film
3 March 1965 Frequency vs. Resolution
(Lines/MM) A.I.M. 4404 Curve. 119
edges.





Analysis of Photographic Image to Evaluate System Performance

Mission 1010-1

FORWARD CAMERA

<u>Pass</u>	<u>Frame</u>	<u>Location</u>	<u>Orientation</u>	<u>Subject</u>	<u>50% Amplitude Spread Function Width (Microns)</u>	<u>A. I. M. Resolution</u>
D-05	033	B-9	070	Dam	9.3	82
D-05	033	B-9	070	Dam	7.3	98
D-05	033	C-9	100	Building	7.1	118
D-05	033	C-9	100	Building	6.5	122
D-05	060	B-3	025	Airfield	8.0	90
D-05	060	B-3	025	Airfield	9.5	86
D-05	061	B-11	080	Airfield	7.4	102
D-05	062	C-5	110	Buildings next to Airfield	9.0	89
D-05	080	C-8	160	Buildings above Airfield	8.3	98
D-05	080	C-8	160	Buildings above Airfield	9.6	83
D-05	080	C-8	150	Airfield	7.7	90
D-05	080	C-8	150	Airfield	9.4	63
D-05	081	B-9	045	Airfield	5.3	118
D-05	081	B-9	045	Airfield	7.4	91
D-05	085	B-10	075	Airfield	10.6	72
D-05	085	B-10	075	Airfield	5.5	121
D-07	027	C-9	155	Airfield	5.8	122
D-07	027	C-9	155	Buildings	10.3	73
D-07	030	B-6	110	Buildings	6.0	116
D-07	030	B-6	110	Buildings	5.6	123

Mission 1010-1
FORWARD CAMERA

<u>Pass</u>	<u>Frame</u>	<u>Location</u>	<u>Orientation</u>	<u>Subject</u>	50% Amplitude Spread Function Width (Microns)	<u>A. I. M. Resolution</u>
D-07	114	B-5	060	Small Dam	18.0	54
D-09	056	B-11	100	Airfield	9.5	68
D-09	056	B-11	100	Airfield	7.6	99
D-09	061	B-11	110	Airfield	5.4	118
D-09	061	B-11	110	Airfield	6.6	105
D-09	084	A-8	075	Airfield	9.1	72
D-09	084	A-8	075	Airfield	6.8	86
D-09	087	C-6	080	Airfield	10.0	83
D-09	087	C-6	080	Airfield	15.7	55
D-09	097	C-3	092	Breakwater	25.9	37
D-09	111	B-9	120	Airfield	10.5	71
D-09	111	B-9	120	Airfield	9.0	95
D-21	114	A-9	100	Airfield	13.9	56
D-21	114	A-9	100	Airfield	6.1	109
D-41	086	A-8	065	Airfield	10.4	82
D-41	086	A-8	065	Airfield	8.1	89
D-41	090	A-2	075	Airfield	10.3	73
D-41	090	A-2	075	Airfield	10.4	70
D-41	090	A-6	030	Dam	7.1	115
D-56	065	C-6	075	Airfield	9.4	89
D-56	065	C-6	075	Airfield	9.7	79
D-56	066	A-8	100	Building	5.9	112
D-56	066	A-8	100	Building next to Airfield	6.9	101

Mission 1010-1
FORWARD CAMERA

<u>Pass</u>	<u>Frame</u>	<u>Location</u>	<u>Orientation</u>	<u>Subject</u>	50% Amplitude Spread Function Width (Microns)	<u>A. I. M. Resolution</u>
D-56*	067	C-8	050	Airfield	9.9	73
D-56*	067	C-8	050	Airfield	7.3	100
D-56*	067	C-6	170	Airfield	14.6	110
D-56	072	B-3	075	Airfield	10.7	76
D-56	087	B-3	170	Airfield	14.3	57
D-56	087	B-3	170	Airfield	11.5	66
D-56	093	C-4	030	Airfield	13.1	63
D-56	093	C-4	030	Airfield	17.8	47
D-56	105	B-11	085	Airfield	15.0	54
D-56	105	B-11	085	Airfield	13.0	63
D-56	122	B-9	020	Airfield	7.6	96
D-56	122	B-9	020	Airfield	8.3	102
D-56	125	B-11	140	Buildings	6.6	112
D-56	127	B-6	085	Airfield	6.3	106
D-56	127	B-6	085	Airfield	7.8	92
D-56	127	B-6	085	Airfield	11.8	63
D-56	127	B-6	085	Airfield	11.8	78
D-56	137	A-8	105	Buildings next to Airfield	10.0	74
D-56	137	A-8	105	Buildings next to Airfield	7.6	83
D-56	137	B-9	175	Dam	6.6	99

*M. I. P. Frame

Mission 1010-1
AFT CAMERA

<u>Pass</u>	<u>Frame</u>	<u>Location</u>	<u>Orientation</u>	<u>Subject</u>	50% Amplitude Spread Function Width (Microns)	<u>A. I. M. Resolution</u>
D-05	038	A-6	070	Dam	6.8	94
D-05	038	A-6	070	Dam	12.3	82
D-05	065	B-11	030	Airfield	12.2	70
D-05	065	B-11	030	Airfield	15.0	57
D-05	065	B-12	110	Buildings	6.8	121
D-05	066	B-4	065	Airfield	7.0	108
D-05	066	B-4	065	Airfield	8.5	122
D-05	067	A-9	130	Buildings next to Airfield	14.5	79
D-05	067	A-9	130	Buildings next to Airfield	13.8	58
D-05	069	A-7	100	Airfield	10.8	72
D-05	069	A-7	100	Airfield	9.3	119
D-05	073	B-5	155	Airfield	10.5	85
D-05	073	B-5	155	Airfield	11.3	110
D-05	077	A-5	055	Dam	7.4	108
D-05	077	A-5	055	Dam	9.1	93
D-05	077	B-C-2	060	Airfield	14.0	55
D-05	077	B-C-2	060	Airfield	9.9	92
D-05	077	B-C-2	060	Airfield	8.1	122
D-05	077	B-C-2	060	Airfield	12.4	58
D-05	085	A-7	140	Buildings near Airfield	12.2	95
D-05	086	B-5	045	Airfield	11.2	74
D-05	086	B-5	045	Airfield	14.4	59

Mission 1010-1

AFT Camera

<u>Pass</u>	<u>Frame</u>	<u>Location</u>	<u>Orientation</u>	<u>Subject</u>	<u>50% Amplitude Spread Function Width (Microns)</u>	<u>A. I. M. Resolution</u>
D-07	036	C-8	110	Buildings near Airfield	7.5	106
D-09	061	B-4	090	Airfield	11.6	103
D-09	061	B-4	090	Airfield	9.4	119
D-09	066	A-B 3-4	110	Airfield	9.2	88
D-09	066	A-B 3-4	110	Airfield	7.7	108
D-09	089	B-7	065	Airfield	12.7	70
D-09	089	B-7	065	Airfield	9.3	88
D-09	093	B-3	075	Airfield	13.2	65
D-09	093	B-3	075	Airfield	12.6	67
D-09	112	C-2	115	Airfield	11.7	57
D-09	112	C-2	115	Airfield	16.0	54
D-09	116	B-5	110	Airfield	9.5	107
D-09	116	B-5	110	Airfield	8.6	87
D-25	073	C-3	090	Airfield	7.3	116
D-25	073	C-3	090	Airfield	11.1	107
D-25	089	A-6	095	Airfield	9.0	97
D-25	089	A-6	095	Airfield	10.7	75
D-25	109	B-9	105	Airfield	5.6	137
D-25	109	B-9	105	Airfield	13.4	69
D-25	116	C-6	085	Airfield	11.4	66
D-25	116	C-6	085	Airfield	5.2	138
D-25	116	B-7	120	Building	8.3	112
D-25	116	B-7	120	Building	9.7	88

Mission 1010-1
AFT CAMERA

<u>Pass</u>	<u>Frame</u>	<u>Location</u>	<u>Orientation</u>	<u>Subject</u>	50% Amplitude Spread Function Width (Microns)	<u>A. I. M. Resolution</u>
D-56*	073	A-B-9	175	Airfield	9.4	89
D-56*	073	A-B-9	175	Airfield	5.3	134
D-56	073	B-6	040	Airfield	8.1	106
D-56	073	B-6	040	Airfield	9.2	122
D-56	085	C-7	165	Building	9.5	74
D-56	093	B-11	165	Airfield	11.8	84
D-56	093	B-11	165	Airfield	16.1	56
D-56	099	A-10	050	Airfield	8.5	122
D-56	099	A-10	050	Airfield	13.6	91
D-56	111	A-3	075	Airfield	8.9	87
D-56	111	A-3	075	Airfield	4.8	132

Analysis of Photographic Image to Evaluate System Performance

Mission 1010-2

Resolution in lines/mm based on the aerial image modulation - 4404 curve from edge trace data reduced by computer techniques.

Arithmetic Mean	84.3 l/mm
Standard Deviation	21.4 l/mm
Coefficient of Dispersion	25%
Number of Edges	110
M.I.P. Frame	136 l/mm

Spread function width at 50% amplitude in microns from edge trace data reduced by computer techniques.

Arithmetic Mean	9.8 μ
Standard Deviation	3.2 μ
Coefficient of Dispersion	32%
Number of Edges	110
M.I.P. Frame	5.0 μ

Analysis of Photographic Image to Evaluate System Performance

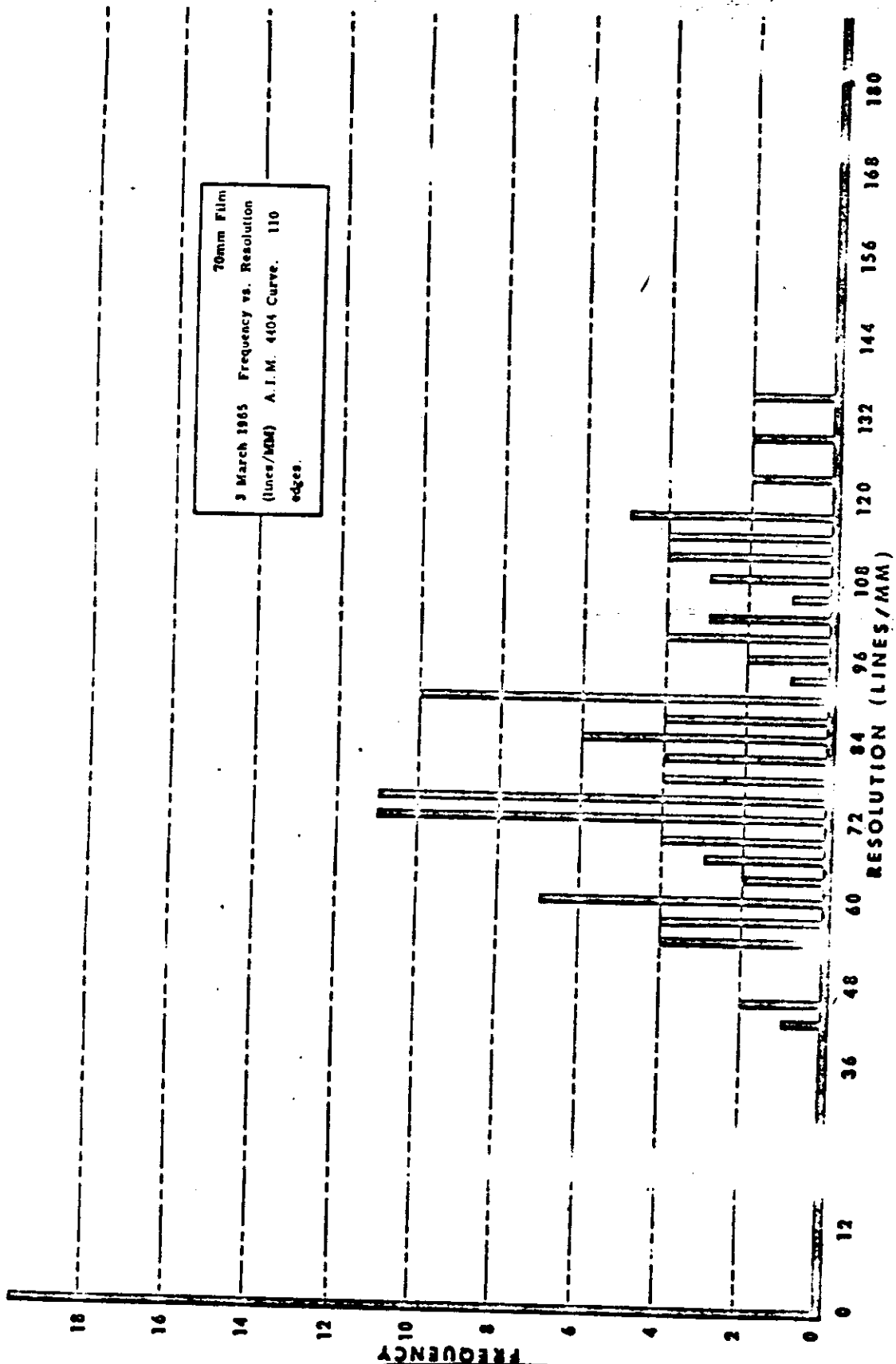
Mission 1010-2

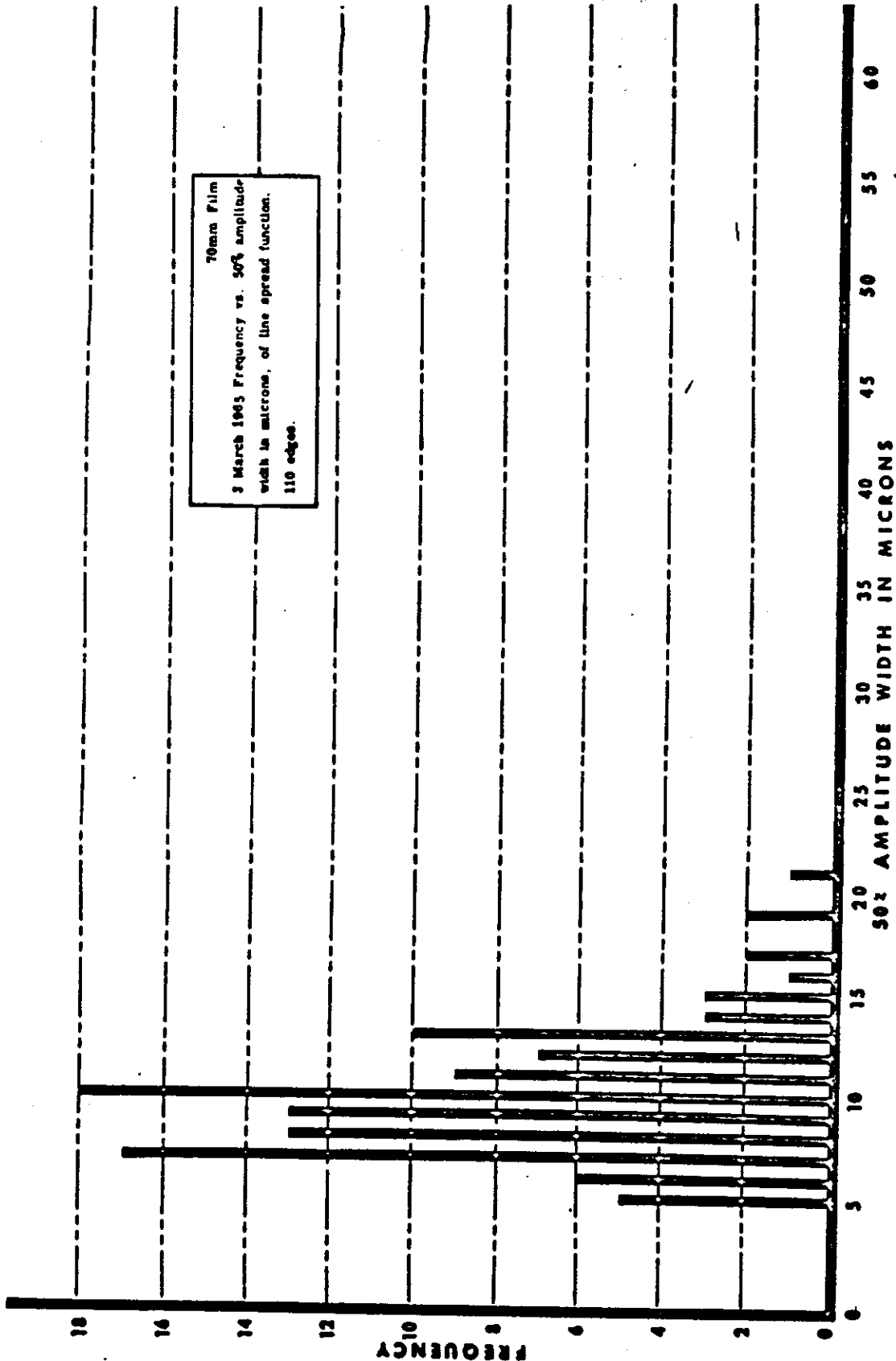
Resolution in lines/mm based on the aerial image modulation - 4404 curve from edge trace data reduced by computer techniques.

	FWD Camera	AFT Camera	Airfields	Buildings
Arithmetic Mean	82.3 l/mm	86.5 l/mm	81.4 l/mm	96.5 l/mm
Standard Deviation	20.5 l/mm	22.2 l/mm	21.2 l/mm	18.0 l/mm
Coefficient of Dispersion	25%	26%	26%	19%
Number of Edges	57	53	89	21

Spread function width at 50% amplitude in microns from edges trace data reduced by computer techniques.

	FWD Camera	AFT Camera	Airfields	Buildings
Arithmetic Mean	10.0 μ	9.7 μ	10.2 μ	8.2 μ
Standard Deviation	3.4 μ	2.9 μ	3.2 μ	2.3 μ
Coefficient of Dispersion	34%	30%	32%	28%
Number of Edges	57	53	89	21





Analysis of Photographic Image to Evaluate System Performance

Mission 1010-2

FORWARD CAMERA

<u>Pass</u>	<u>Frame</u>	<u>Location</u>	<u>Orientation</u>	<u>Subject</u>	50% Amplitude Spread Function Width (Microns)	<u>A. I. M. Resolution</u>
D-68	062	A-2	110	Airfield	7.2	90
D-68	062	A-2	110	Airfield	10.5	68
D-68	068	B-7	150	Buildings	6.5	113
D-68	068	B-7	150	Buildings	6.1	123
D-63	074	B-11	140	Airfield	9.6	81
D-63	074	B-11	140	Airfield	7.9	88
D-68	080	B-8	170	Airfield	10.3	74
D-68	080	B-8	170	Airfield	11.3	73
D-63	083	B-8	035	Airfield	8.3	89
D-68	083	B-8	035	Airfield	9.6	78
D-68	083	A-8	125	Buildings	13.3	61
D-68	083	A-8	125	Buildings	5.6	113
D-71	042	B-6	110	Airfield	19.2	53
D-84	094	C-6	075	Airfield	9.8	82
D-84	094	C-6	075	Airfield	7.6	89
D-84	101	B-12	115	Airfield	12.9	58
D-84	101	B-12	115	Airfield	10.2	86
D-84	106	C-3	085	Airfield	19.3	44
D-84	106	C-3	085	Airfield	12.9	68
D-84	106	C-3	150	Airfield	14.4	59
D-84	106	C-3	150	Airfield	11.7	57

Mission 1010-2

FORWARD CAMERA

<u>Pass</u>	<u>Frame</u>	<u>Location</u>	<u>Orientation</u>	<u>Subject</u>	<u>50% Amplitude Spread Function Width (Microns)</u>	<u>A. I. M. Resolution</u>
D-84	107	B-2	090	Airfield	8.5	91
D-84	107	B-2	090	Airfield	12.5	61
D-85	099	B-6	110	Buildings	7.8	90
D-85	099	B-6	110	Buildings	11.4	69
D-86	031	C-6	020	Airfield	14.6	59
D-86	031	C-6	020	Airfield	14.4	54
D-86	037	C-2	105	Buildings	7.0	98
D-86	037	C-2	105	Buildings	7.1	90
D-88	087	C-12	100	Airfield	6.7	100
D-88	087	C-12	100	Airfield	9.6	76
D-88	124	B-6	100	Airfield	12.9	62
D-88	124	B-6	100	Airfield	11.6	82
D-93	017	C-5	080	Ground Test Obj.	8.6	85
D-93	017	C-5	170	Ground Test Obj.	7.2	102
D-93	021	C-7	060	Airfield	10.0	83
D-93	021	C-7	060	Airfield	8.4	85
D-93	028	C-8	120	Airfield	10.0	116
D-93	028	C-8	120	Airfield	9.8	76
D-100	015	A-10	100	Airfield	9.9	79
D-100	015	A-10	100	Airfield	9.1	85
D-101	054	BC-7	025	Airfield	11.6	70
D-101	054	BC-7	025	Airfield	14.9	58
D-115	046	C-11	075	Airfield	6.7	96
D-115	046	C-11	075	Airfield	4.7	110
D-115	047	B-12	170	Airfield	11.6	64
D-115	047	B-12	170	Airfield	6.9	107

~~TOP SECRET~~

Mission 1010-2
FORWARD CAMERA

<u>Pass</u>	<u>Frame</u>	<u>Location</u>	<u>Orientation</u>	<u>Subject</u>	50% Amplitude Spread Function Width (Microns)	<u>A. I. M. Resolution</u>
D-115	050	C-11	045	Airfield	8.1	84
D-115	050	C-11	045	Airfield	6.4	117
D-115	051	A-12	065	Airfield	6.8	114
D-115	051	A-12	065	Airfield	8.6	84
D-115	051	C-11	070	Airfield	8.6	75
D-115	051	C-11	070	Airfield	5.8	111
D-115*	053	B-8	060	Airfield	10.6	74
D-115*	053	B-8	060	Airfield	5.2	129
D-131	028	C-3	105	Airfield	11.0	66
D-131	028	C-3	105	Airfield	20.7	42

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Mission 1010-2

AFT CAMERA

<u>Pass</u>	<u>Frame</u>	<u>Location</u>	<u>Orientation</u>	<u>Subject</u>	50% Amplitude Spread Function Width (Microns)	<u>A. I. M. Resolution</u>
D-68	067	A-12	125	Airfield	10.9	77
D-68	067	A-12	125	Airfield	12.6	66
D-68	074	B-8	150	Buildings	5.9	116
D-68	080	B-3	125	Airfield	12.5	75
D-68	080	B-3	125	Airfield	12.8	58
D-68	086	B-6	175	Airfield	7.0	105
D-68	086	B-6	175	Airfield	7.8	89
D-68	089	C-7	035	Airfield	9.6	90
D-68	089	C-7	035	Airfield	5.1	112
D-68	089	C-7	120	Buildings	8.7	100
D-71	048	BC-8	115	Airfield	5.4	129
D-71	048	BC-8	115	Airfield	8.2	86
D-84	101	C-9	070	Airfield	12.0	71
D-84	101	C-9	070	Airfield	5.5	135
D-84	104	BC-7	110	Airfield	8.4	76
D-84	104	BC-7	110	Airfield	9.3	76
D-84	107	A-2	115	Airfield	9.0	109
D-84	107	A-2	115	Airfield	9.8	72
D-84	112	B-12	080	Airfield	12.8	59
D-84	112	B-12	080	Airfield	11.9	71
D-84	113	B-11	095	Airfield	17.4	76
D-84	113	B-11	095	Airfield	16.6	54
D-85	035	B-7	140	Buildings	7.3	109
D-85	035	B-7	140	Buildings	8.0	101
D-86	037	B-9	020	Airfield	8.1	97
D-86	037	B-9	020	Airfield	7.4	117

Mission 1010-2

AFT Camera

<u>Pass</u>	<u>Frame</u>	<u>Location</u>	<u>Orientation</u>	<u>Subject</u>	50% Amplitude Spread Function Width (Microns)	<u>A. I. M. Resolution</u>
D-86	043	B-12	105	Buildings	8.1	116
D-86	043	B-12	105	Buildings	7.0	102
D-86	108	B-7	155	Dam	10.6	78
D-86	108	B-7	155	Dam	9.0	89
D-93	014	C-5	150	Airfield	10.7	72
D-93	014	C-5	150	Airfield	11.6	66
D-93	023	B-9	070	Ground Test Obj.	6.6	113
D-93	023	B-9	160	Ground Test Obj.	14.0	60
D-93	027	A-7	070	Airfield	6.7	124
D-93	027	A-7	070	Airfield	9.1	91
D-100	020	A-4	100	Airfield	10.4	72
D-100	020	A-4	100	Airfield	10.4	81
D-101	060	B-8	025	Airfield	13.2	60
D-101	060	B-8	025	Airfield	10.0	74
D-115	052	B-3	065	Airfield	15.9	45
D-115	052	B-3	065	Airfield	9.2	75
D-115	053	C-2	140	Airfield	10.3	71
D-115	053	C-2	140	Airfield	8.5	94
D-115	056	B-4	035	Airfield	10.1	73
D-115	056	B-4	035	Airfield	7.8	87
D-115	057	AB-3	170	Airfield	6.7	111
D-115	057	AB-3	170	Airfield	10.3	71
D-115	058	B-3	035	Dock	7.3	99
D-115*	059	C-7	045	Airfield	9.2	73
D-115*	059	C-7	045	Airfield	5.0	136

*M.I.P. Frame

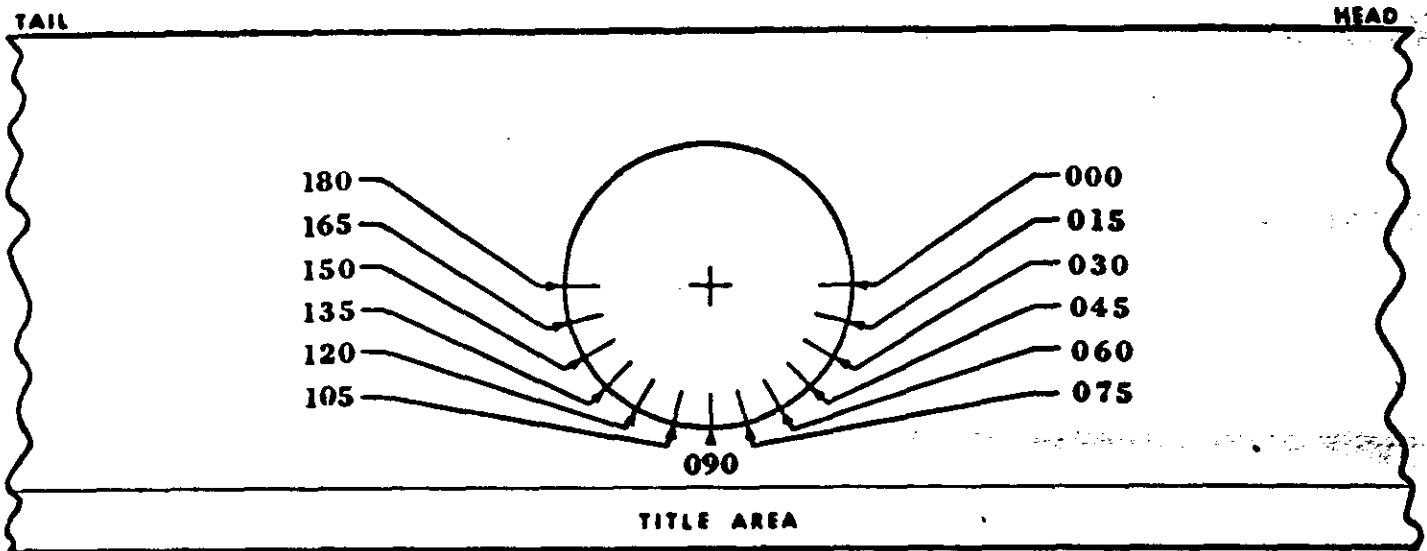
Mission 1010-2

AFT CAMERA

<u>Pass</u>	<u>Frame</u>	<u>Location</u>	<u>Orientation</u>	<u>Subject</u>	50% Amplitude Spread Function Width (Microns)	<u>A. I. M. Resolution</u>
D-131	034	B-11	105	Airfield	10.7	71
D-131	034	B-11	105	Airfield	14.8	55

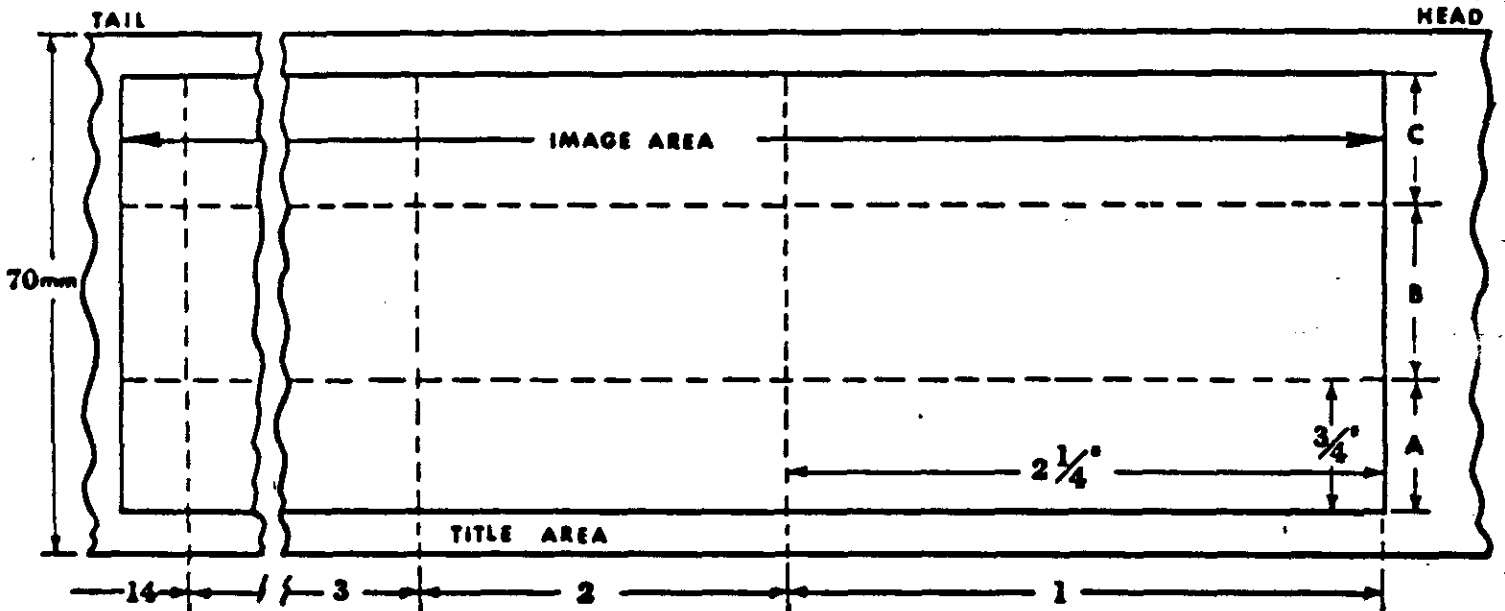
Reference System For Orientation Of C/M/J Mission Edges

original negative - - emulsion up



Grid For Position Of C/M/J Mission Edges

original negative - - emulsion up



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SECTION 11

OBSERVED DATA

Photography over the United States was acquired on descending passes 31, 47, 61 and 93. Clouds and haze degraded more than 60% of the total area covered. There was no appreciable difference in quality between fore and aft photography.

Pass D-31 over western New Mexico and eastern Arizona presented a very bright scene with low contrast ground detail. Scattered clouds and haze were present. Even so, numerous ordnance bunkers and pertinent transportation facilities at Fort Wingate, N. M. were easily identified. Individual cars in a parking lot were observed as well as cars and trucks on U.S. Route 66.

Pass 47 over Nevada was very hazy. Indian Springs fixed target was located 12" west of C/F and the largest group could not be resolved. Further south, in the Colorado River Basin, the haze lessened and ground detail in the 10 to 12 foot range could be isolated.

Pass 61 over eastern New York and Pennsylvania was very hazy, starting with 75% cloud cover at the start and 100% by the time it reached central New Jersey. Some holes in the cloud cover and partial clearing yielded some interesting data. Excellent system performance was demonstrated by coverage of the Tappan-Zee Bridge. The entire superstructure of this fabricated steel cantilever bridge could be seen in great detail.

At the Verrazano Narrows Bridge, the suspension cables could be easily seen. These cables are twin 36 inch supports spaced about 3 feet apart. They could not be seen as individual strands. Also some of the hanger cables could be seen, however each hanger is actually a group of 4 cables of unknown size, but probably less than 6 inches, each arranged in a one to two foot square array. It is also interesting to note that the main cables of the Manhattan Bridge with 2 pairs of 21 1/4 inch cables, The Williamsburg Bridge with 2 pairs of 18 3/8 inch cables and the Brooklyn Bridge's single outside cables of 15 3/4 inch diameter could be distinguished.

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At NAS Johnsville, clouds and haze rendered the fixed targets unresolvable. However, on the portable target, Group 3 was resolved in the forward unit and Group 2 in the Aft. Due to target orientation, these represent cross track resolution only in the 8 - 12 foot range.

Pass 93, centered on western Ohio and Kentucky, had heavy cloud cover with some hazy holes. Such a hole opened up over WPAFB and the portable T Bar target could be resolved to Group 2. At Frankfort, Kentucky, Capitol City Airport's all weather runway numbers "6" and "24", which seem to conform to FAA standard markings, the 5 foot wide vertical arms were clearly seen even though the visual contrast was low.

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SECTION 12

MISSION 1010-1 STELLAR-INDEX CAMERA

A. COMPONENT ASSIGNMENT

<u>Component</u>	<u>Serial Number</u>
Camera	D 41
Index Reseau	41
Stellar Reseau	41

B. CAMERA DATA AND FLIGHT SETTINGS

Stellar Camera:

Lens	85mm f/1.8
Exposure Time	2 seconds
Filter Type	None
Film Type	Eastman Type 3401

Index Camera:

Lens	38mm f/4.5
Exposure Time	1/500 second
Filter Type	Wratten 21
Film Type	Eastman Type 3400

C. POST FLIGHT EVALUATION

The camera functioned properly throughout the mission with no observed equipment or photographic anomalies. Approximately twenty star images were recorded during the mission. One Stellar camera fiducial was over-exposed but usable.

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Emulsion cracking was observed in most Stellar frames. It was minor at the start of the mission and became very heavy near the end of the mission. Occasional minor edge static was noted on the camera number edge throughout the mission. The last twenty-two frames were slightly fogged; from frame #412 to #420 the film appeared to be fogged by corona discharge while frame #421 and #422 was probably fogged by light. The fogging is attributed to the camera slew mode and is normally observed in this area of the Stellar film.

Foreign objects in space were imaged in frames #1 through #24 and are attributed to Agena fuel venting. Objects of unknown origin were also noted in frame numbers 31, 39, 40, 42, 46, 52, 68, 81, 84, 87, 142, 167, 231, 242, 258 and 283.

Double stellar imagery was present intermittently throughout the mission. The magnitude of the separation appeared to be cyclic. Frame #12 contained several foreign objects, assumed to be fuel particles, which were not in the straight line pattern normally observed but were in a broken line pattern indicating vehicle roll motion during photography. Double star images were also present in this frame. A sketch of this frame is shown in Figure 12-1. Computer data shows that the Slave camera was lagging the Master camera by 104 degrees. Approximations show that the time base, shown by the broken line, and the displacement, as measured from the double imagery, correspond to a roll rate of $233^{\circ}/\text{hr}$. and a corresponding cross track IMC error of 2.7%. The rate lasted for about one second in each direction. It is apparent that in cases where this roll rate motion is additive to earth rotation a total IMC error could result that would limit the system performance. A report covering the detailed analysis of this anomaly has been published by A/P.

The quality of the Index camera was considered to be the best obtained during a Corona mission. All camera functions operated properly throughout the mission.

The frame corners on the camera number edge were slightly distorted outward from the proper position. The reseau line image gave the impression that the film was not flat on the reseau plate.

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MISSION 1010-1 STELLAR FORMAT

FRAME #12

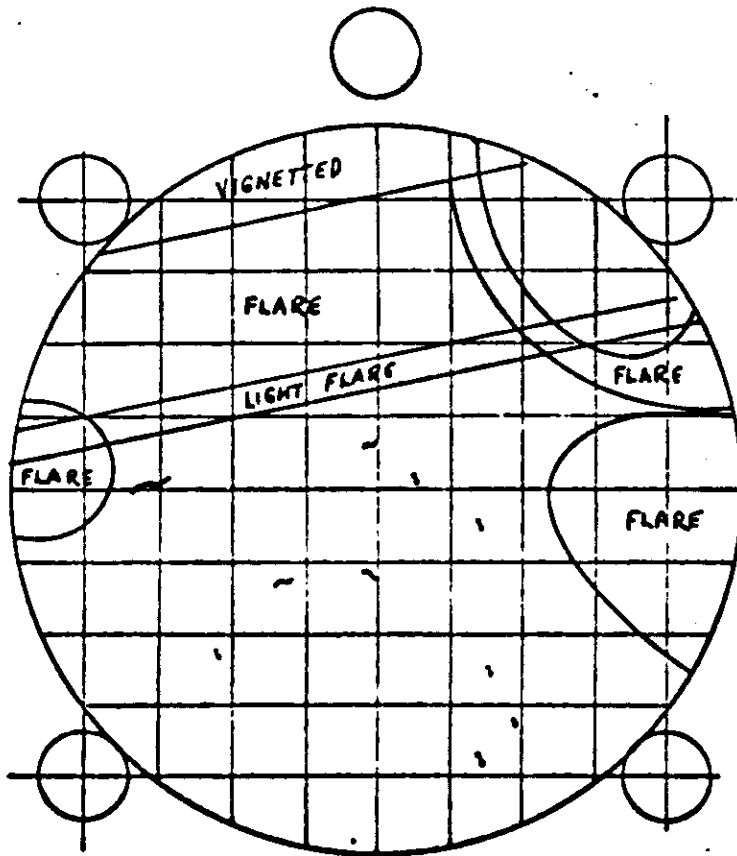


FIGURE 12-1

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SECTION 13

MISSION 1010-2 STELLAR-INDEX CAMERA

A. COMPONENT ASSIGNMENT

Component	Serial Number
Camera	D 44
Index Reseau	46
Stellar Reseau	44

B. CAMERA DATA AND FLIGHT SETTINGS

Stellar Camera:

Lens	85mm f/1.8
Exposure Time	2 seconds
Filter Type	None
Film Type	Eastman Type 3401

Index Camera:

Lens	38mm f/4.5
Exposure Time	1/500 second
Filter Type	Wratten 21
Film Type	Eastman Type 3400

C. POST FLIGHT EVALUATION

All camera functions operated properly throughout the mission. Cyclic, double star images were observed on the photography.

Two separate fog patterns produced by light leaks were observed on the stellar film. The first pattern was associated with camera sit time and produced a fog pattern starting at each edge of the film extending into the format area. The location of the fog pattern correlates with the interface of the camera and chute. The second pattern was a faint band of fog

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across the entire format about 1.1 inches wide every 5 inches the entire length of the film. This pattern could be detected through frame 92 however it was not considered degrading. The pattern was present but barely detectable after frame 92. The cause of this second pattern is unknown. It is very possible that it is not associated with camera operations.

The stellar film emulsion was cracked throughout the mission; minor near the start and quite heavy near the end. One crack pattern had a 1.6 inch pitch during the entire mission and appears to be associated with camera operations. This problem has been investigated and is attributed to foreign material on the camera platen.

The last ten frames of stellar film were fogged by corona discharge. This is attributed to the film slew at the completion of the mission.

A small light leak within the Index camera produced a fogged area on all frames nowever image degradation was only encountered at camera sit times. The fogged frames show that the leak was at the interface of the camera body and the film chute.

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SECTION 14

VEHICLE ATTITUDE

The vehicle attitude errors for both Mission 1010-1 and 1010-2 were derived from the reduction of the Stellar camera photography. This attitude data is supplied to A/P by NPIC.

The attitude errors for each frame and the attitude control rates are calculated at the A/P computer facility. The computer also plots the frequency distribution of the rates and errors. Figures 14-1 through 14-6 show these distributions for Mission 1010-1 and Figures 14-7 through 14-12 for Mission 1010-2.

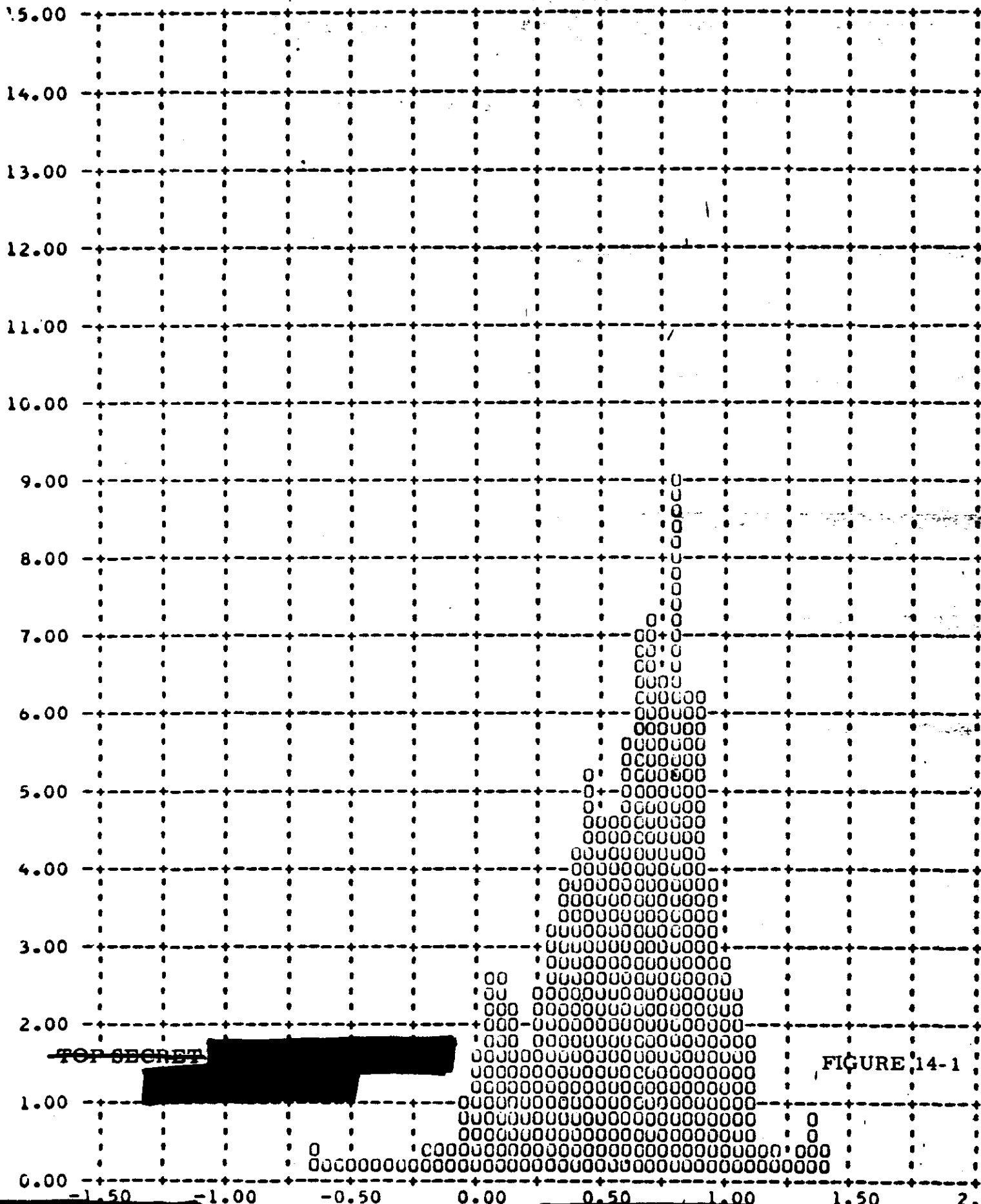
The summary table below lists the maximum attitude errors and rates that were experienced during 90% of the photographic operations, excluding the first six frames of each operation, and the total range of the errors and rates.

<u>Value</u>	<u>Mission 1010-1</u>		<u>Mission 1010-2</u>	
	<u>90%</u>	<u>Range</u>	<u>90%</u>	<u>Range</u>
Pitch Error ($^{\circ}$)	0.93	-0.65 to +1.40	0.59	-2.50 to +0.60
Roll Error ($^{\circ}$)	0.30	-0.38 to +0.54	0.70	+0.34 to +1.04
Yaw Error ($^{\circ}$)	0.87	-0.35 to +1.60	1.21	-0.15 to +2.60
Pitch Rate ($^{\circ}$ /hr)	39.1	- 80 to + 65	45.4	- 95 to + 90
Roll Rate ($^{\circ}$ /hr)	23.6	- 95 to + 65	23.6	- 70 to + 58
Yaw Rate ($^{\circ}$ /hr)	30.8	- 70 to + 70	30.7	- 56 to + 46

The performance of the attitude control system is comparable to the control systems used on recent missions. Yaw error was somewhat larger than usual. The panoramic photography was not degraded by the attitude control system.

INST 1 J11A V1178 L 9-14-64 FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 0.9

Y PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



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FIGURE 14-1

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INST 1 J11A V1178 L 9-14-64 FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 0.3

Y ROLL ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

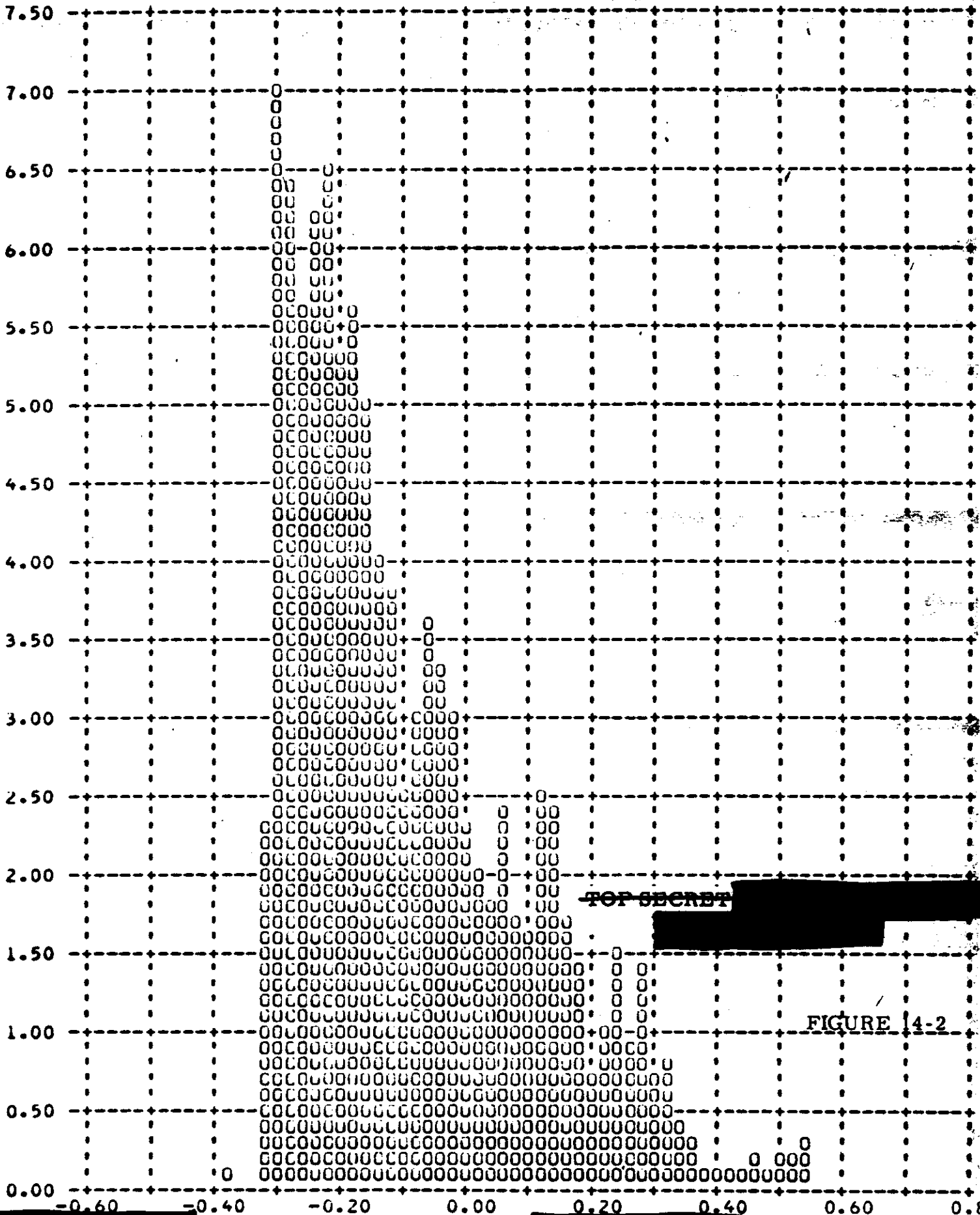
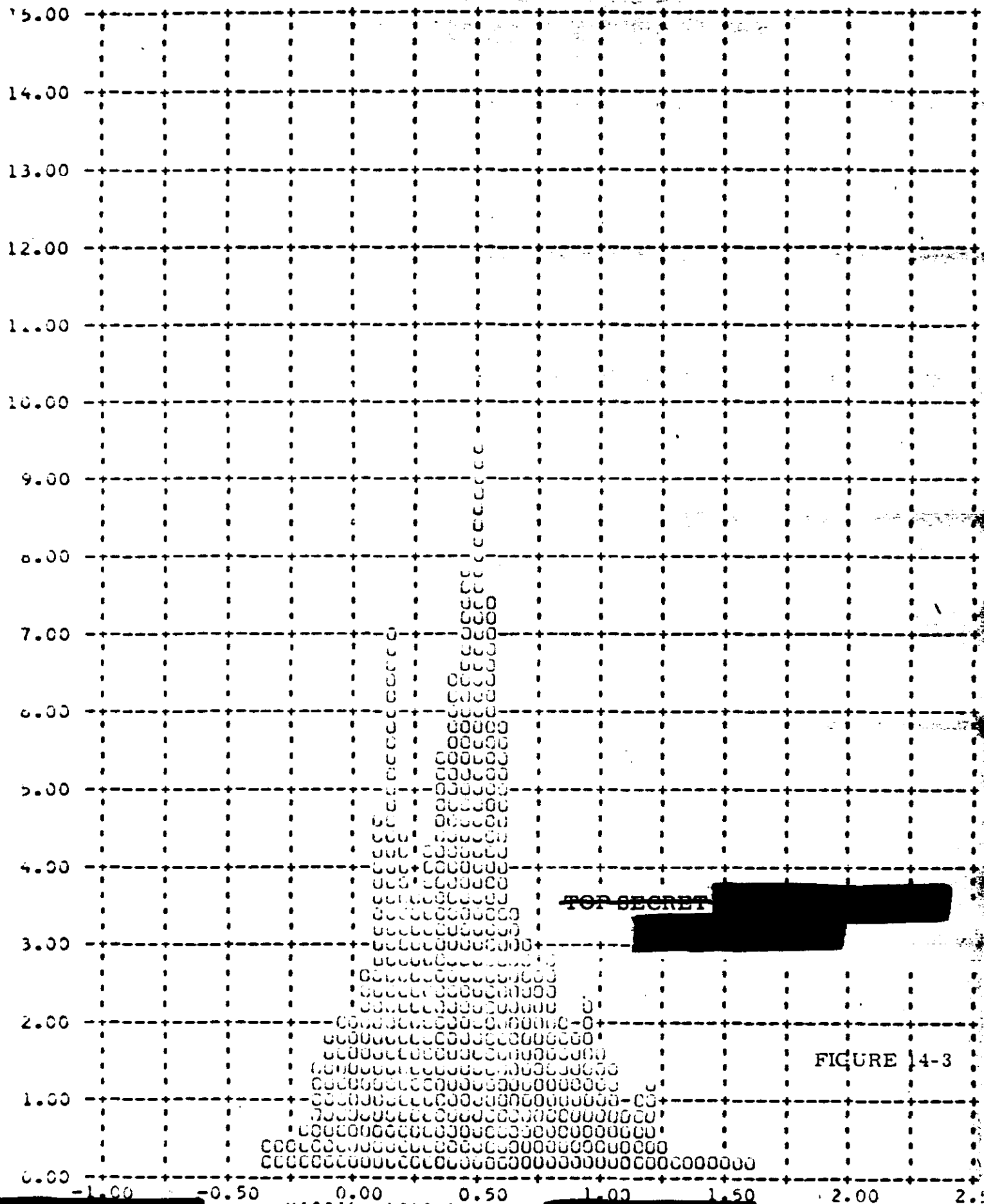


FIGURE 14-2

INST 1 J11A V1178 L 9-14-64 FRAMES 1-6 OF EACH OP UNITED 90 PERCENT = 0.8

Y YAW ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

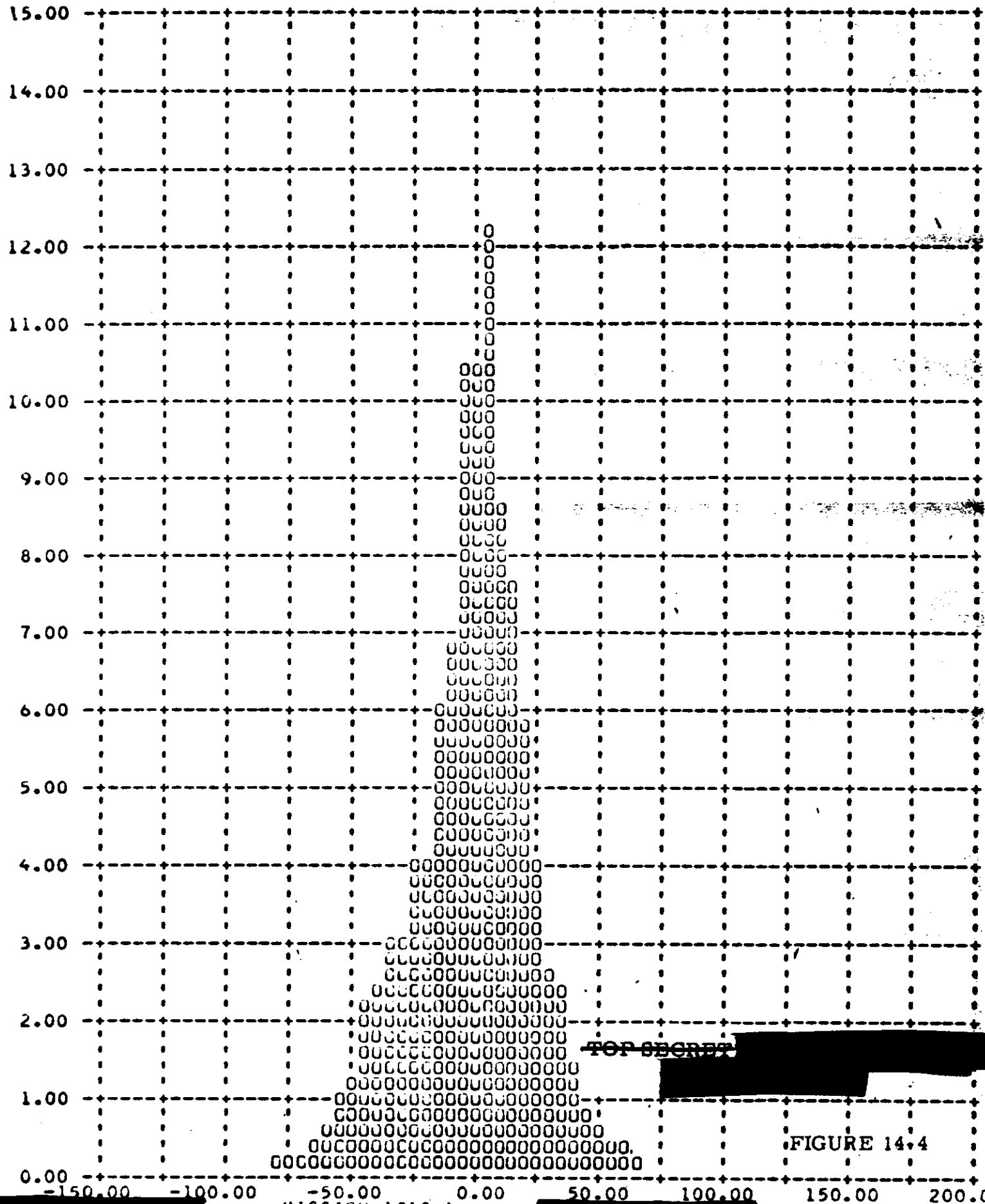


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FIGURE 14-3

TEST 1 J11A V1178 L 9-14-64 FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 39.0

Y PITCH RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

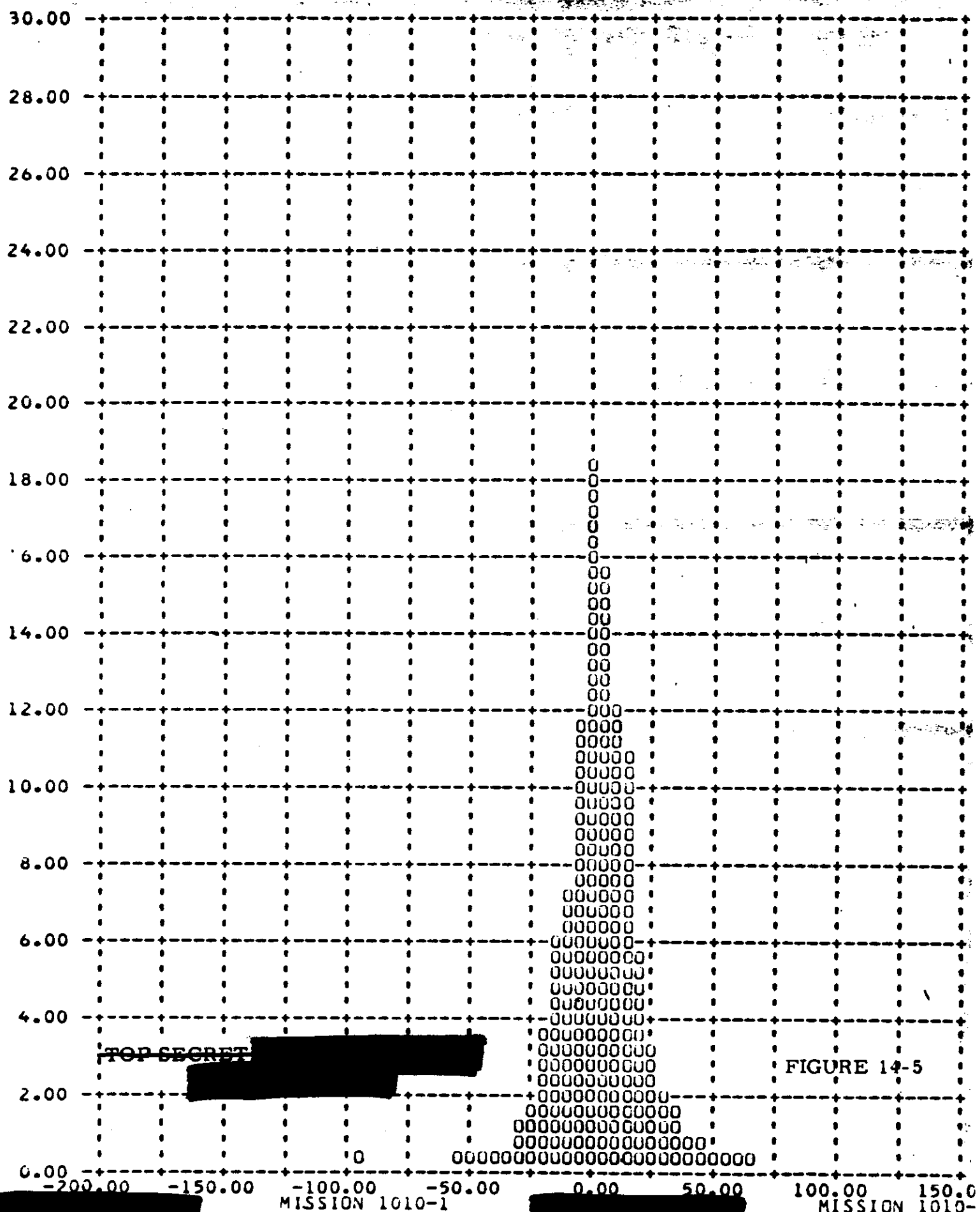


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FIGURE 14.4

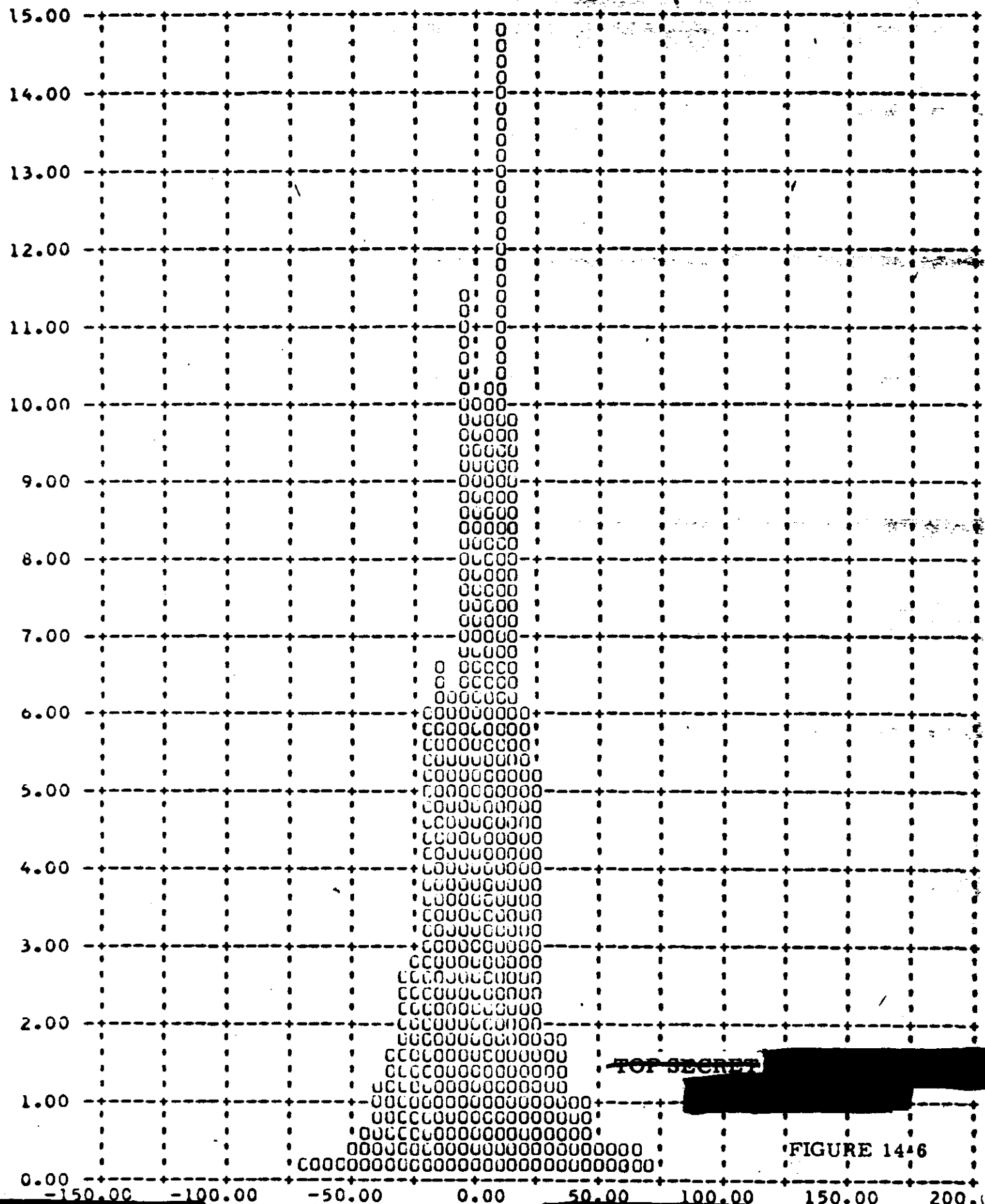
INST 1 - J11A - V1178 L 9-14-64 FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 23.6%

Y ROLL RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



INST 1 J11A V1178 L 9-14-64 FRAMES 1-6 OF EACH OF OMITTED 90 PERCENT = 30-85

Y YAW RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

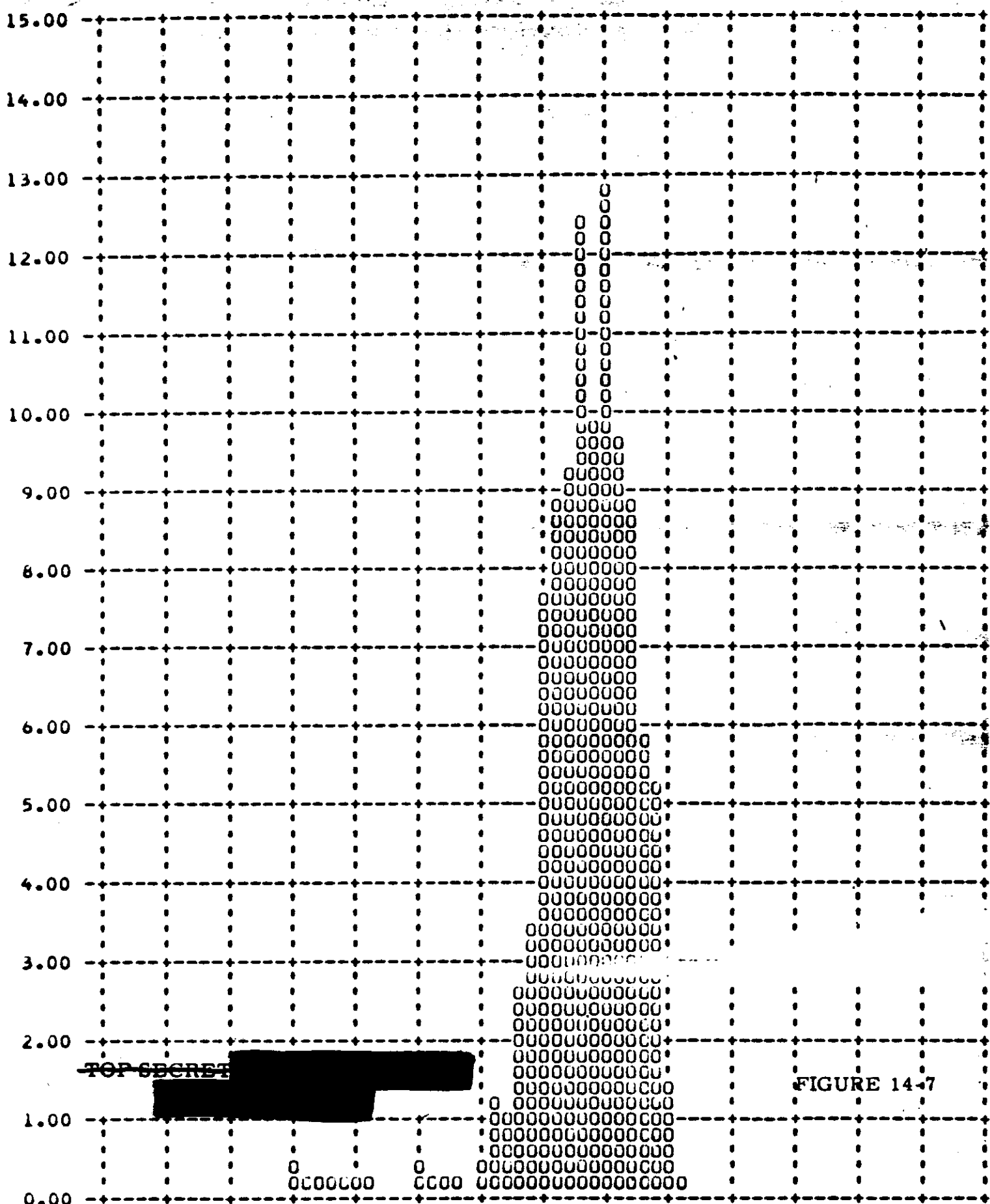


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FIGURE 14-6

INST 1 J11B V1178 L 9-14-64 FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 0.5

Y PITCH ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



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FIGURE 14-7

INST 1 J118 V1178 L 9-14-64 FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 0.

Y ROLL ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)

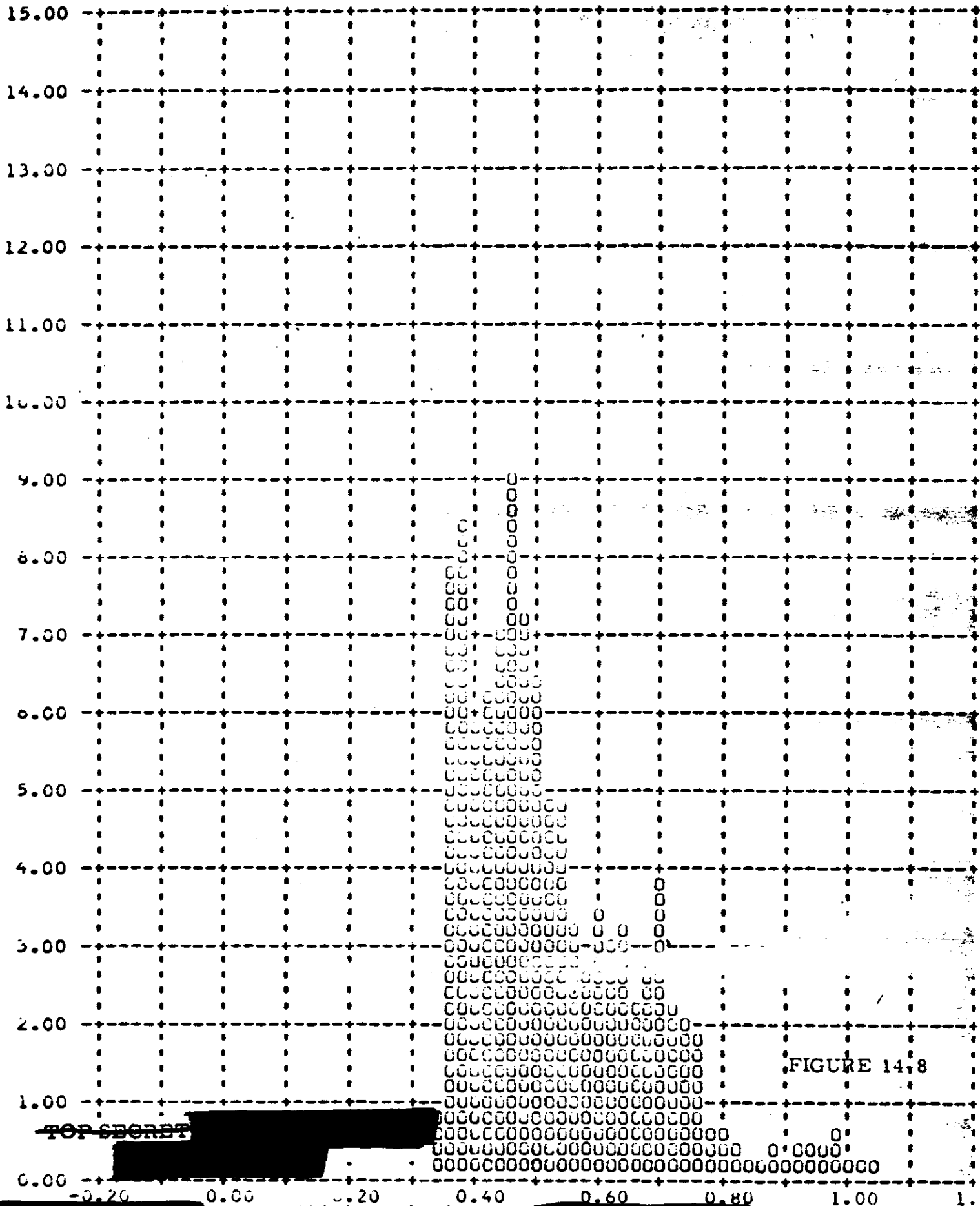
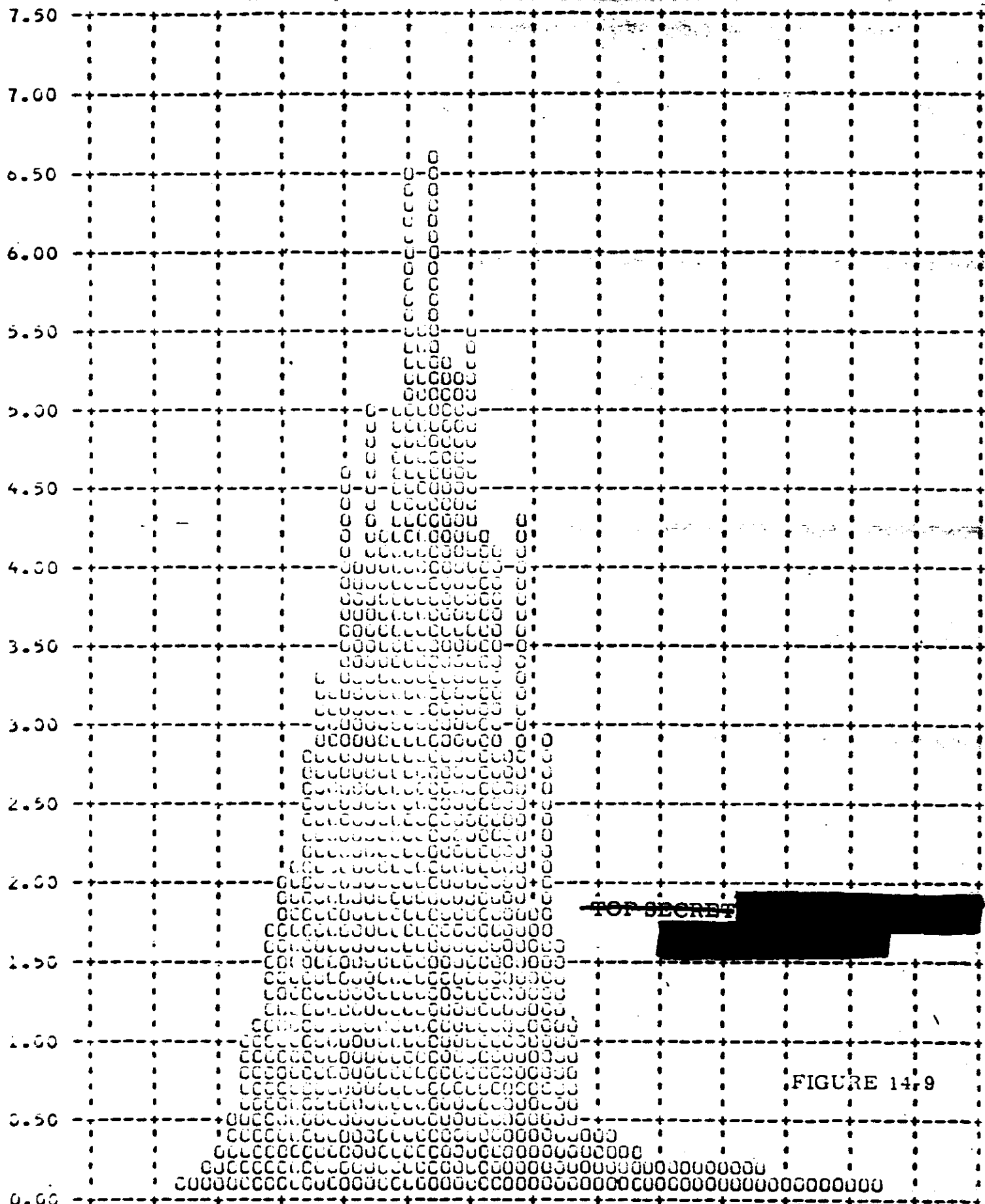


FIGURE 14.8

INST 1 J118 V1178 L 9-14-64 FRAMES 1-8 OF EACH OP OMITTED 90 PERCENT = 1.2

Y YAW ANGLE ERROR - DEGREES (X) VERSUS FREQUENCY - PERCENT (Y)



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FIGURE 14.9

INST 1 J11B V1178 L 9-14-64 FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 45.4

Y PITCH RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

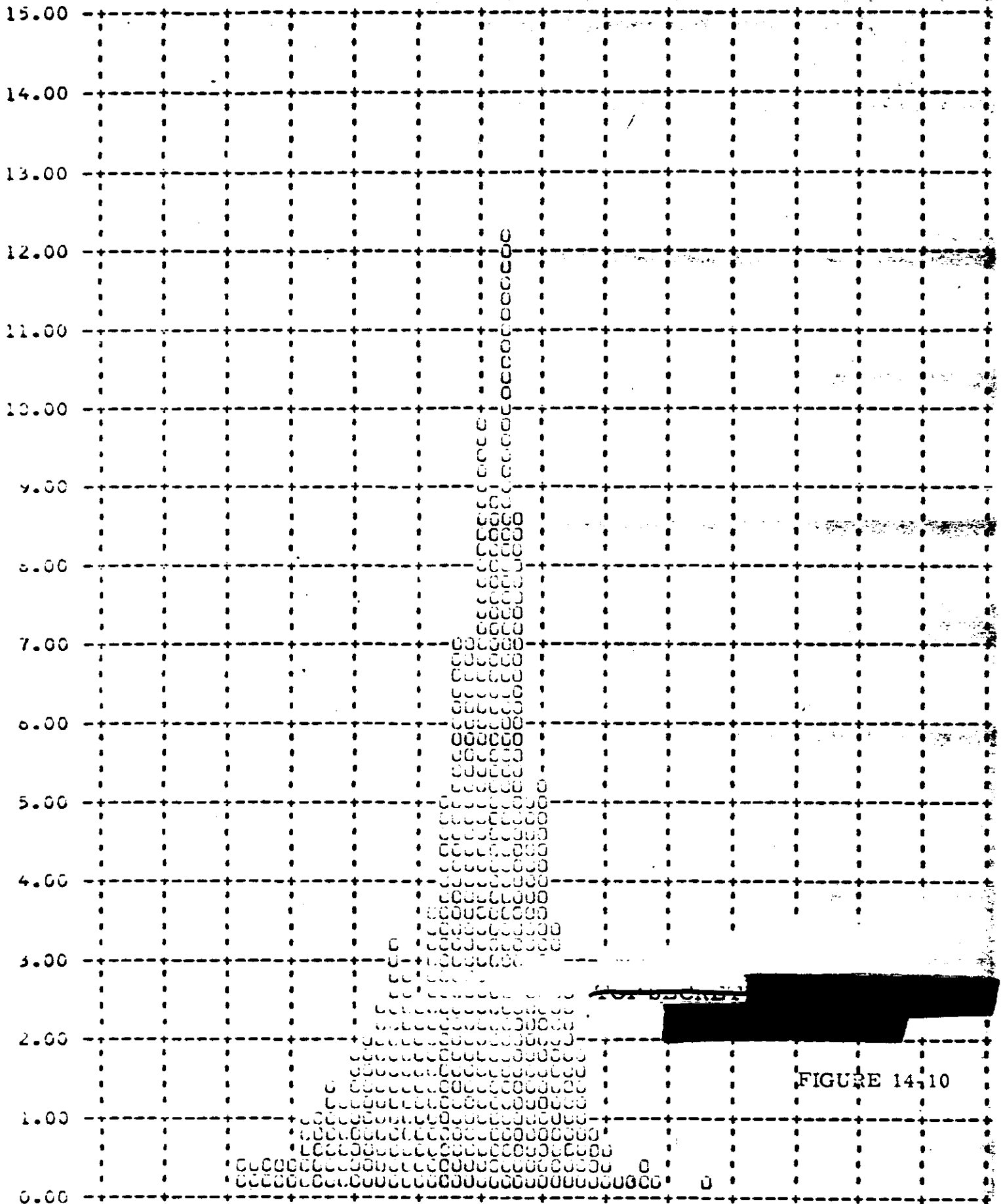
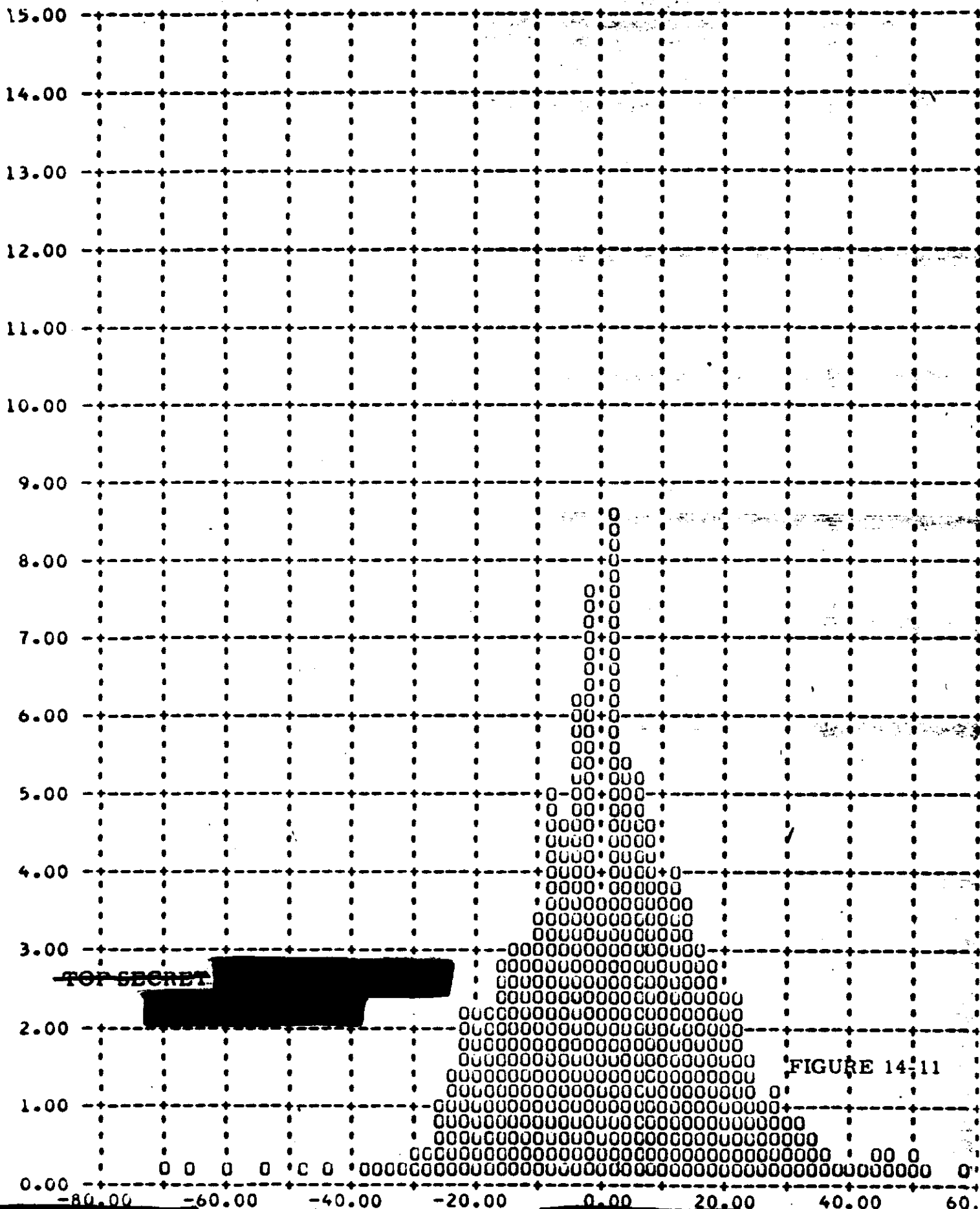


FIGURE 14.10

INST 1 J118 V1178 L 9-14-64 FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 23.5

Y ROLL RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)

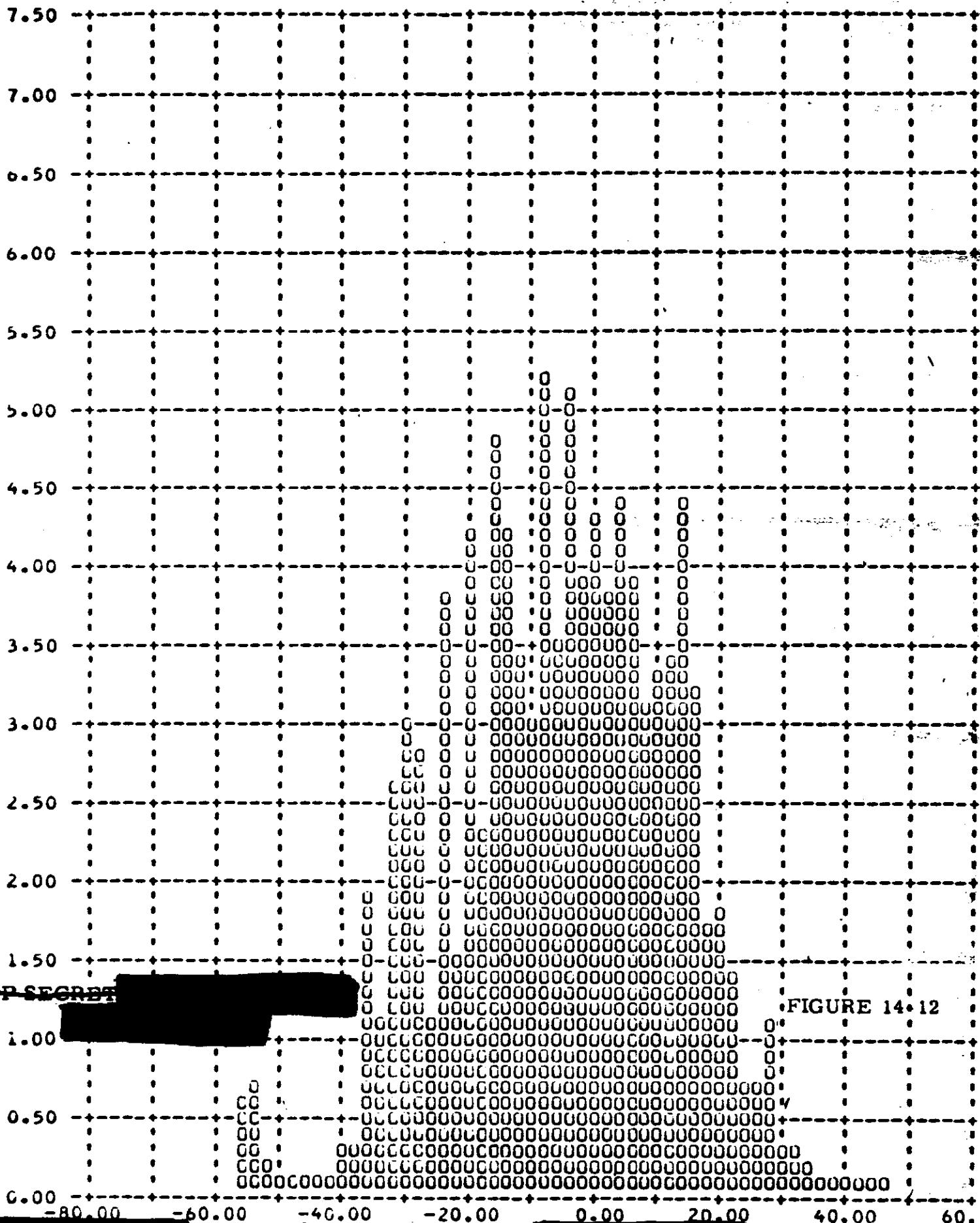


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FIGURE 14-11

INST 1 J11B V1178 L 9-14-64 FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 30.74

Y YAW RATE ERROR - DEG/HOUR (X) VERSUS FREQUENCY - PERCENT (Y)



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FIGURE 14.12

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SECTION 15

IMAGE SMEAR ANALYSIS

The frame correlation tape supplied to A/P by NPIC contains the binary time word of each frame of photography. A computer program has been assembled at A/P which calculates the exposure time of each frame and compares the camera cycle rate with the ephemeris to calculate the V/h mismatch. This data is combined with the vehicle attitude error and rate values of each frame and the crab error caused by earth rotation at the latitude of each frame. The program outputs the total along track and cross track IMC error and the limit of ground resolution that can be acquired by a camera regardless of focal length and system capabilities.

The computer rejects the first six frames of all operations as the large V/h error induced by camera start-up is not representative of the overall system operations. The frequency distribution of the V/h errors and resolution limits are computer plotted and are shown in Figures 15-1 through 15-6.

The summary table below presents the maximum V/h ratio errors and resolution limits that existed during 90% of the photographic operations and the total range of values during all operations that were computed.

<u>Value</u>	<u>Mission 1010-1</u>		<u>Mission 1010-2</u>	
	<u>90%</u>	<u>Range</u>	<u>90%</u>	<u>Range</u>
V/h Ratio Error (%)	4.5	-8.6 to +1.2	4.6	-5.6 to +6.2
Along Track				
Resolution Limit (ft.)	2.3	0 to 6.6	7.5	0 to 9.6
Cross Track				
Resolution Limit (ft.)	4.4	1.1 to 5.9	3.8	0 to 5.6

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INST 1 J11A V1178 L 9-14-64 FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 4.5

Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)

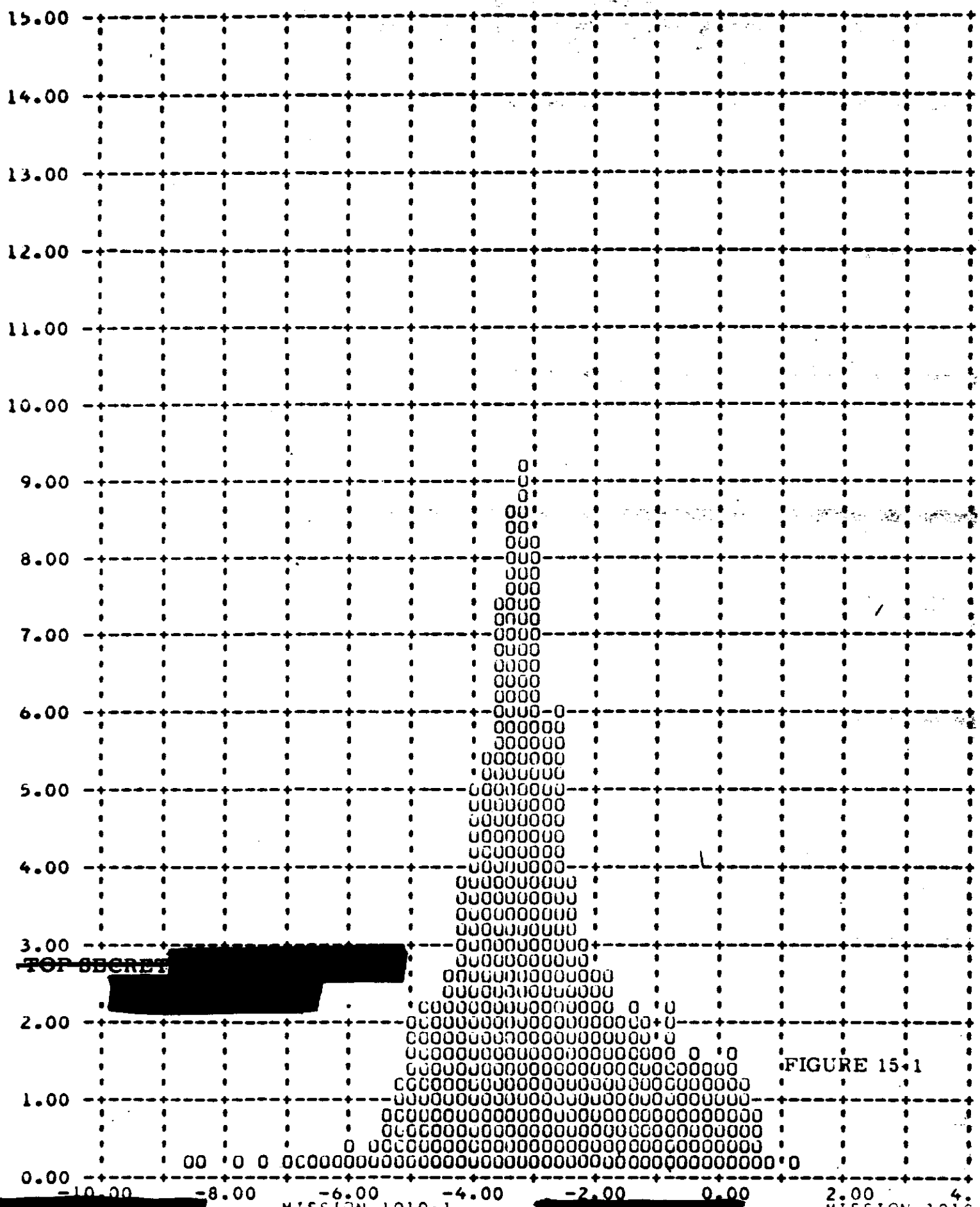
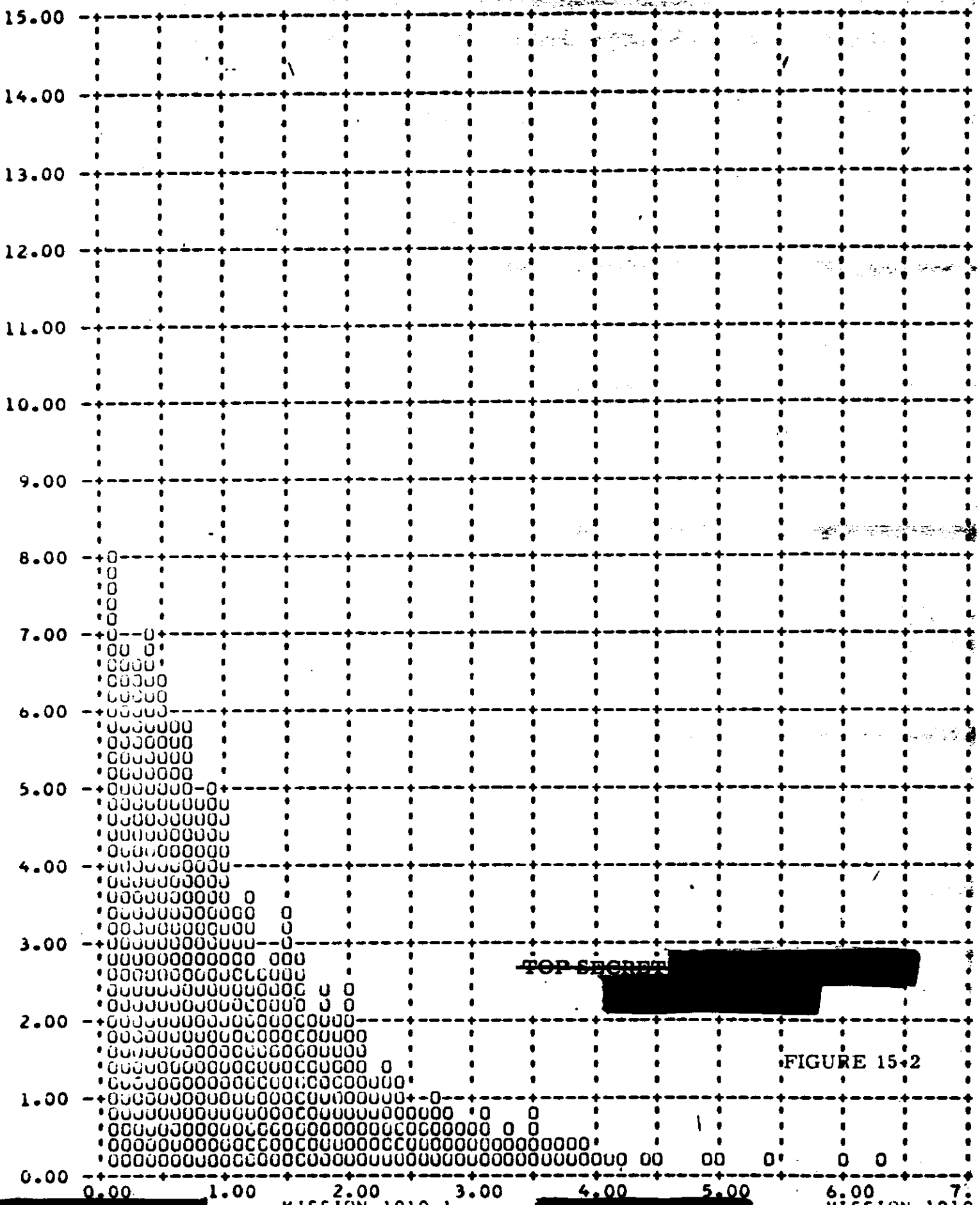


FIGURE 15-1

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INST 1 J11A V1178 L 9-14-64, FRAMES 1-6 OF EACH OF LIMITED 90 PERCENT = 2.2E

Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)



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FIGURE 15-2

INST 1 J11A V1178 L 9-14-64 FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 4.3

Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

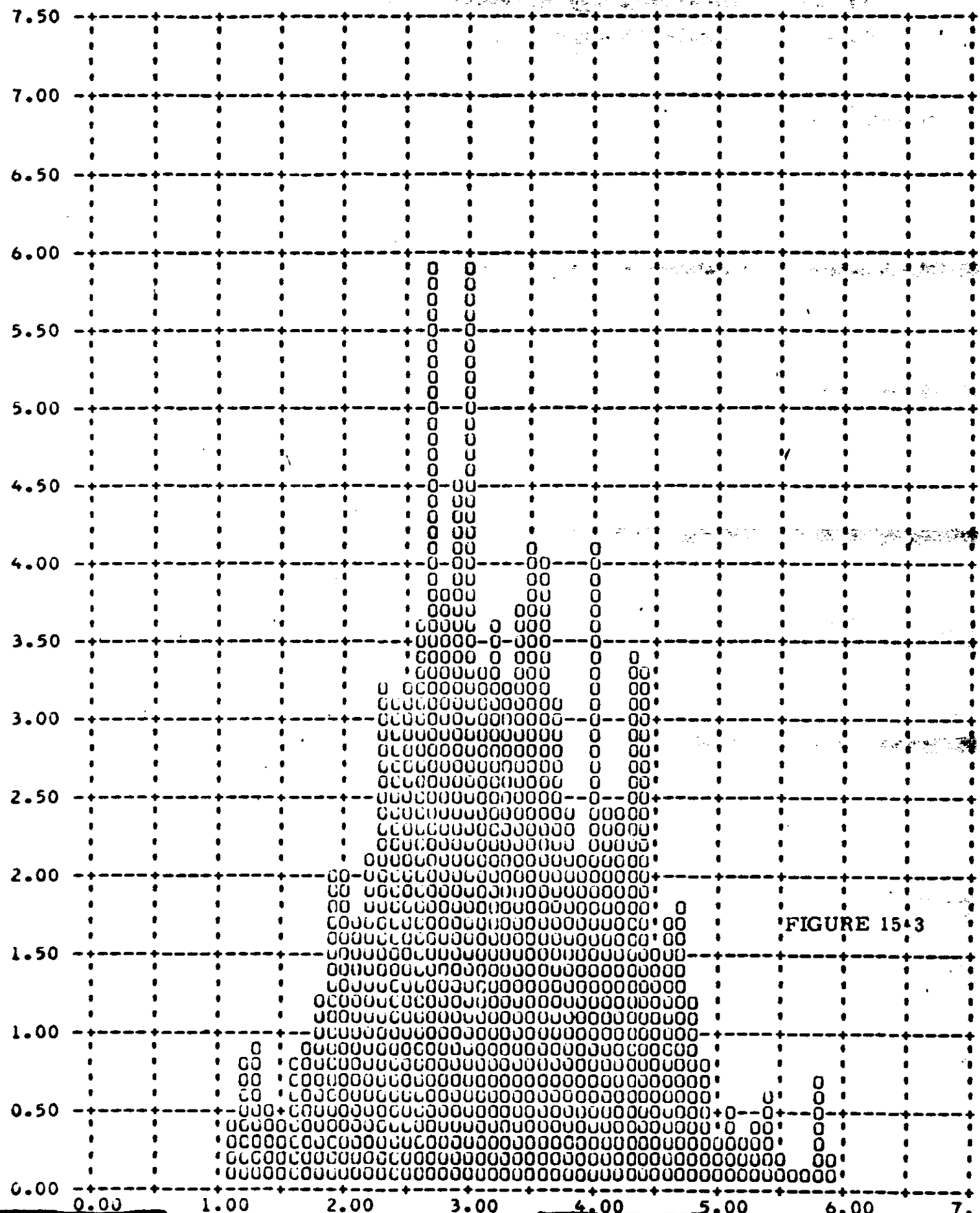


FIGURE 15-3

INST 1 J118 V1178 L 9-14-64 FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 4.63

Y V/H RATIO ERROR - PERCENT (X) VERSUS FREQUENCY - PERCENT (Y)

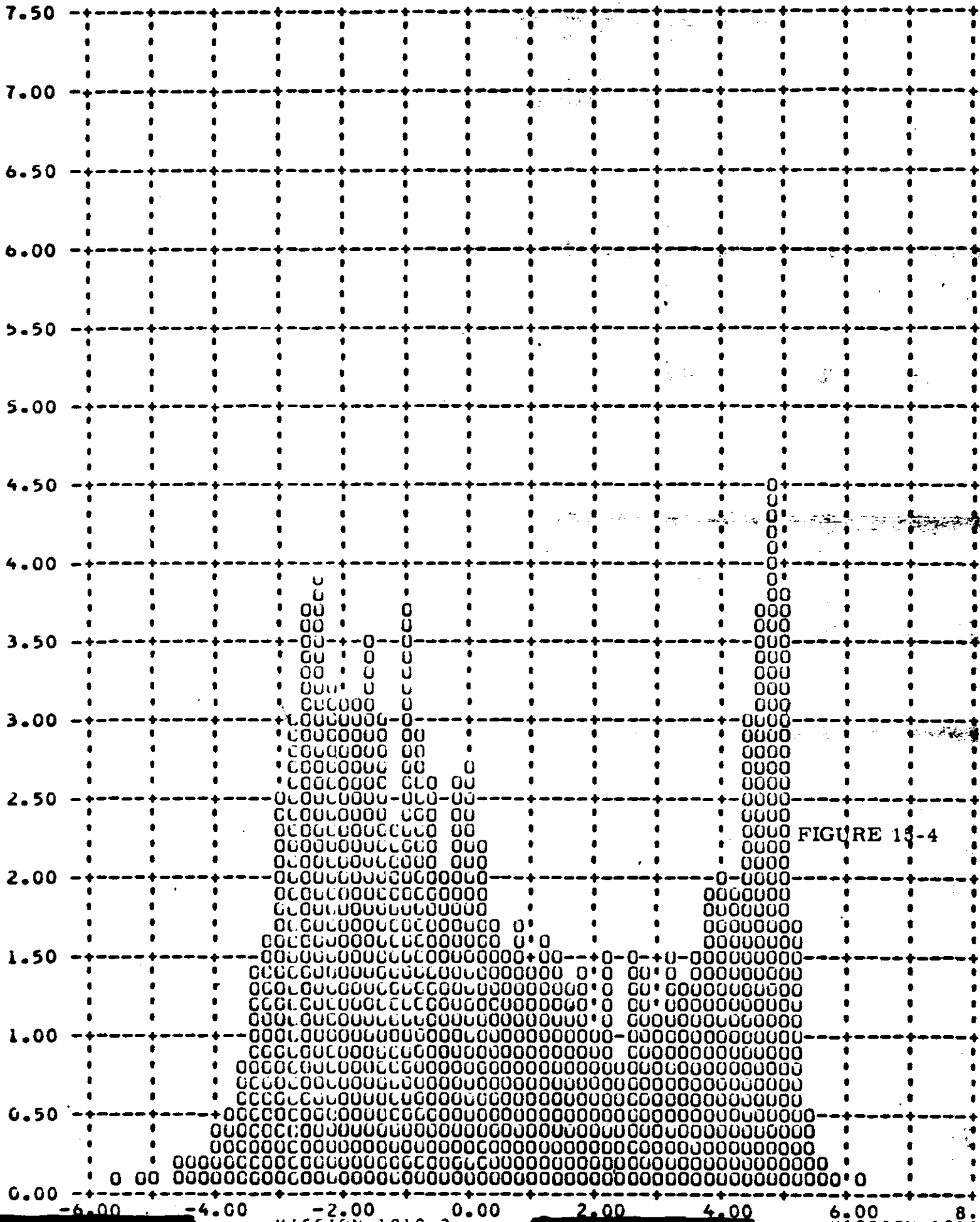


FIGURE 13-4

INST 1 J118 V1178 L 9-14-64 FRAMES 1-6 OF EACH UP OMITTED 90 PERCENT = 7.50

Y ALONG TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)

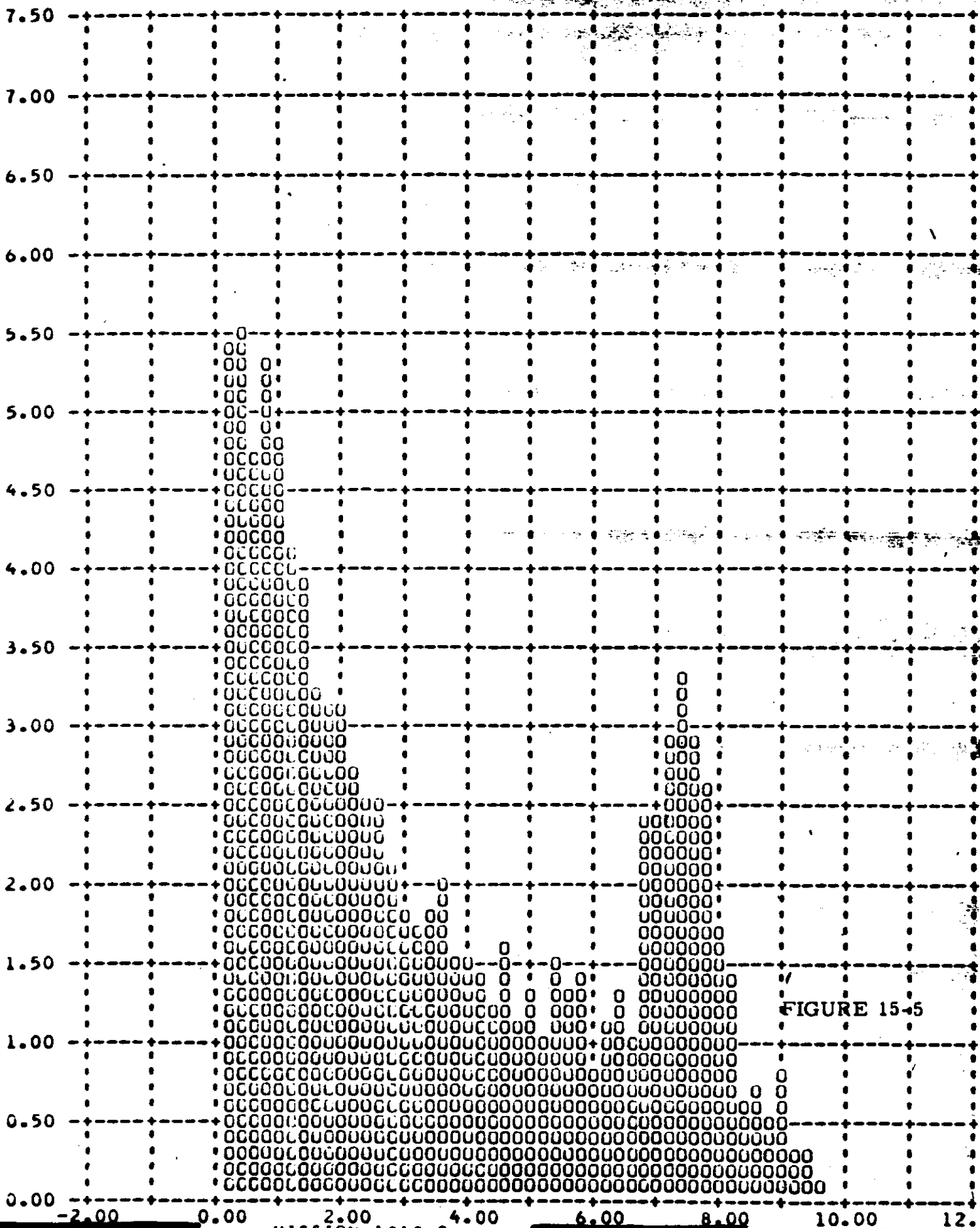
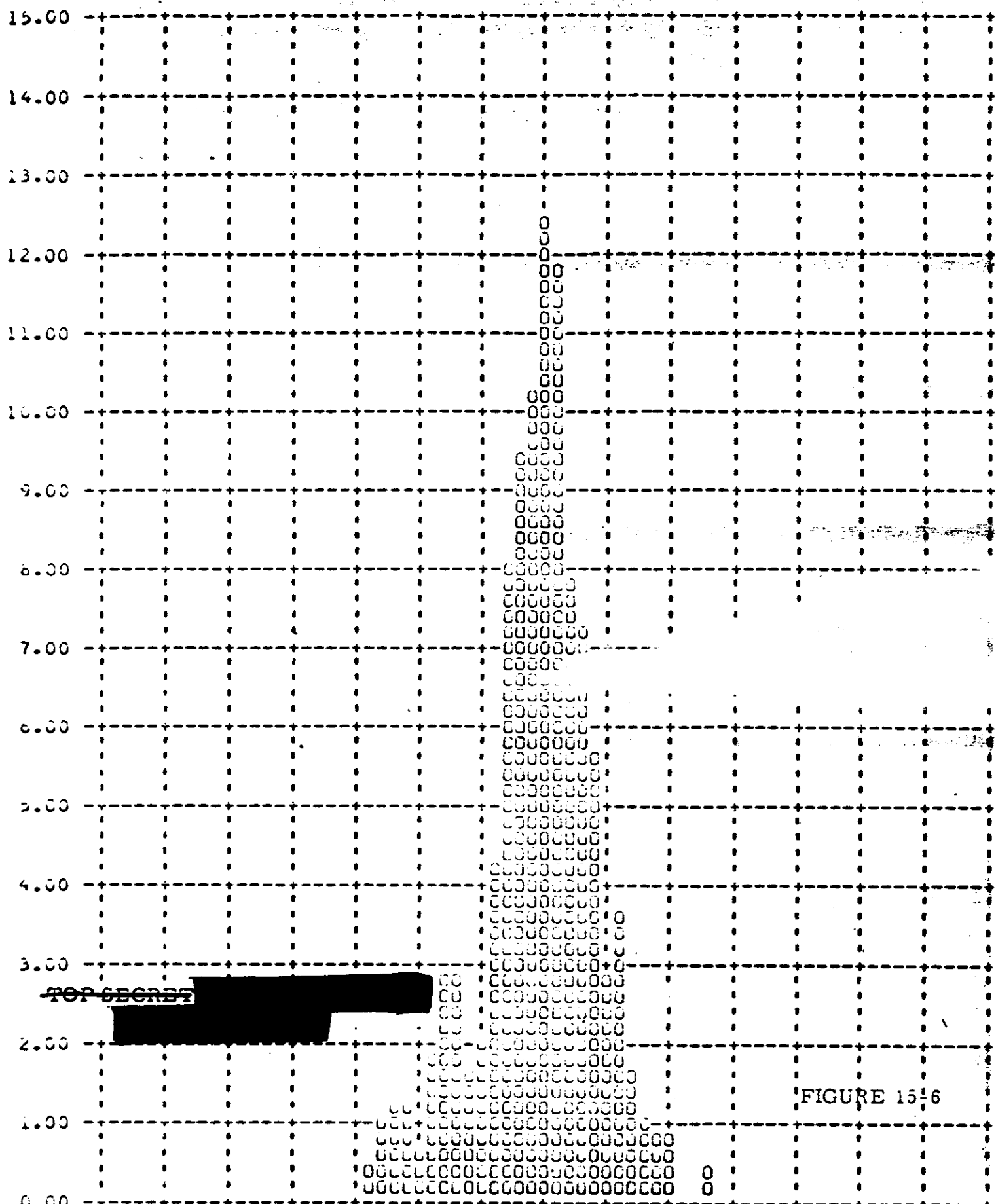


FIGURE 15-5

INST 1 J118 V1178 L 9-14-64 FRAMES 1-6 OF EACH OP OMITTED 90 PERCENT = 3.8

Y CROSS TRACK RESOLUTION LIMIT - FEET (X) VERSUS FREQUENCY - PERCENT (Y)



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FIGURE 15.6

SECTION 16

RADIATION DOSAGE

Each recovery system flown on a Corona mission contains a sealed packet of Eastman Type 3401 and Royal X Pan emulsions to determine the total radiation received at the take-up cassette. Both film types have been irradiated by LMSC at various levels and the base plus fog densities recorded after controlled processing.

Following recovery the film dosimeter packets are removed at A/P and processed with a pre-flight sample of the same film type and sensitometric control film. The resulting base plus fog density measurement of the dosimeter strips is used to ascertain the total radiation level. The table below presents the base plus fog readings for the dosimeter strips and the radiation level equivalents.

<u>Emulsion</u>	<u>Mission 1010-1</u>		<u>Mission 1010-2</u>	
	<u>B + F Density</u>	<u>Radiation</u>	<u>B + F Density</u>	<u>Radiation</u>
Type 3401	0.20	0.8 R	0.19	0.7 R
Royal X Pan	0.31	0.6 R	0.27	0.5 R

The mean total radiation seen by the take-up cassettes during both missions was approximately 0.6 roentgens. This level is somewhat less than received during recent missions and is below the level that would degrade the panoramic photography.

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SECTION 17

SYSTEM RELIABILITY

Reliability calculations for the payload are based on a sample beginning with M-7. Hence both the major part of the Mural Program and the "J" Program are covered in the calculation. For certain auxiliaries, i. e., the stellar-index camera and the horizon cameras, the sample size is changed to recognize incorporation of modified equipment or new designs where reliability was one of the principal reasons for the modification. However, for primary mission function, the sample size is consistent with reliability reporting for the vehicle.

The reliability estimates of this section deal exclusively with the payload. Failures to achieve orbit or vehicle induced failures are thereby excluded. Recoveries before a complete mission has been completed are considered as full missions providing that early termination was caused by reasons not connected with payload operation. Film quality is not considered in the reliability estimate calculation. Hence, only electrical and mechanical functioning are considered.

The reliability estimate is also divided into primary and secondary functions. The primary functions are operation of the panoramic cameras, main camera door operation, operation of the payload clock, and recovery operations. The secondary mission functions are horizon camera operation excluding catastrophic open shutter failure mode, auxiliary data recording, and stellar-index camera operation.

Panoramic Camera Reliability

Sample Size - 64 opportunities to operate.

One failure - capping shutter on slave instrument on system M-7.

Assume - 3000 cycles per camera per mission.

Estimated Reliability = 98.5% at 50% confidence level.

Main Camera Door Reliability

Sample Size - 32 vehicles x 2 doors = 64 opportunities to operate

1 major malfunction, door failed to eject for 7 passes, Mission 9048.

1 minor malfunction, door failed to eject for 2 passes, Mission 1006.

Estimated Reliability = 97.6% at 50% confidence level.

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Payload Clock Reliability

Sample Size - 36 completed missions in sample.

No failures.

Estimated Reliability = 98.1% at 50% confidence level.

Estimated Reliability of Payload Functioning on orbit

98.5 x 97.6 x 98.1 = 94.3

Recovery System Reliability

32 opportunities to recover

1 failure - improper separation due to water seal - cutter failure.

Estimated Reliability = 94.8% at 50% confidence level.

Stellar-Index Camera Reliability

Sample begins with M-13

Sample size = 24

Number of failures = 7

Estimated Reliability = 74.8% at 50% confidence.

Horizon Camera Reliability

Sample includes M27, J5A, J5B, J9A, J9B, and up; 13 samples

1 failure - center of format switch, Mission 1006

Estimated Reliability of Single Camera = 92.6% at 50% confidence level.

Estimated Reliability of Four Horizon Cameras at a Parallel

Redundant System = 99.4% at 50% confidence level

Horizon Camera Door Reliability

Sample size = 32 x 4 = 128 opportunities to operate

No failures have occurred.

Estimated Reliability = 99.5% reliability at 50% confidence level.

Stellar-Index Camera Door Reliability

Terrain Door, Stellar Door, and deployment of Stellar Baffle are functions considered.

Sample size = 21 x 3 = 63 chances to operate.

One failure - stellar baffle failed to deploy.

Estimated Reliability = 97.7% at 50% confidence level.

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SECTION 18

SUMMARY DATA

The comparison of the operating parameters and the performance achieved by previous missions has been difficult due to the large volume of data that results from each mission. Some of the pertinent characteristics from prior missions have been summarized in Tables 18-1 through 18-3.

The summary data was started with Mission 1004 as the J-05 camera system was the first to incorporate the major modifications of the titanium drum and scan arm, four roller scan head and Corona J capabilities. Only those missions that culminated in the recovery of some photography have been listed, therefore Missions 1003 and 1005 are deleted.

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PERFORMANCE SUMMARY

MISSE:	M/NR:	SERIAL NUMBER	M/T/P	VISUAL RES	SPLIT ALTITUDE	M/EEZ M	SPLIT ALTITUDE	90% ATTITUDE ERROR (°)		90% ATTITUDE EPRES (VHR)	90% V/M EP/DOR (D)	90% RESOLUTION (M Y LINE)
								PITCH	ROLL			
1004-1	FWD	124	85	78	97	109	115	0.45	1.08	25.0	5.1	7.7
	AFT	125	85	86	80	96	117	0.74	0.91	30.0	4.9	6.8
	AFT	125	85	76	88	113	90	0.41	1.14	28.5	15.4	13.8
	AFT	125	85	73	85	106	95	0.49	1.08	27.9	11.6	10.1
1006-1	FWD	148	90	78	65	88	84	0.58	1.43	23.9	3.6	8.4
	AFT	149	90	74	71	90	87	0.64	0.47	43.0	4.6	7.6
	AFT	149	90	85	64	81	84	0.59	0.94	23.9	2.9	5.9
	AFT	149	90	83	72	90	87	0.63	0.71	24.0	2.8	5.4
1007-1	FWD	144	85	80	80	95	81	0.65	0.71	22.7	3.3	5.8
	AFT	145	85	86	63	83	86	0.48	0.59	23.9	2.6	5.9
	AFT	145	85	79	72	81	83	0.93	0.87	23.6	4.5	4.4
	AFT	145	85	91	77	92	74	0.59	0.70	23.6	4.6	3.8
1009-1	FWD	150	85	80	80	95	81	0.65	0.71	22.7	3.3	5.8
	AFT	151	85	76	73	89	85	0.65	0.71	22.7	3.3	5.8
	AFT	151	85	82	84	96	83	0.65	0.71	22.7	3.3	5.8
	AFT	151	85	79	91	83	85	0.65	0.71	22.7	3.3	5.8
1009-2	FWD	154	85	92	80	95	81	0.65	0.71	22.7	3.3	5.8
	AFT	155	85	88	85	83	86	0.65	0.71	22.7	3.3	5.8
	AFT	155	85	94	85	84	84	0.65	0.71	22.7	3.3	5.8
	AFT	155	85	87	87	87	72	0.65	0.71	22.7	3.3	5.8
1010-1	FWD	152	85	90	90	88	87	0.65	0.71	22.7	3.3	5.8
	AFT	153	85	88	86	80	92	0.65	0.71	22.7	3.3	5.8
	AFT	153	85	92	81	82	82	0.65	0.71	22.7	3.3	5.8
	AFT	153	85	90	82	85	87	0.65	0.71	22.7	3.3	5.8

EXPOSURE - PROCESSING SUMMARY

MISSION NUMBER	CAMERA	SOLAR ELEVATION RANGE (°)		SOLAR AZIMUTH RANGE (°)		PREDICTED PROCESSING			REPORTED PROCESSING			COMPUTED PROCESSING			TERRAIN D-MIN			TERRAIN D-MAX			CLOUD RANGE			UNDER EXPOSED (N)	UNDER PROCESSED (N)	NOMINAL EXP & PROC (N)	OVER PROCESSED (N)	OVER EXPOSED (N)	CLOUD COVER (N)				
		LOW	HIGH	LOW	HIGH	P	F	T	P	F	T	P	F	T	LOW	HIGH	MEAN	LOW	HIGH	MEAN	LOW	HIGH	MEAN										
8004-1	PWD	3	61	23	124	5	74	19	4	79	17	0	79	21	0	28	1.89	0.83	0.78	0.43	2.43	1.97	2.02	1.00	2.43	2.04	2.08	0	4	60	31	0	35
	APT	-3	61	23	124	5	74	21	4	79	17	0	80	20	0	22	1.58	0.76	0.70	0.53	2.43	1.92	1.94	1.08	2.43	1.98	2.03	0	4	67	26	0	35
	AFT	-4	66	10	131	7	78	17	37	50	13	4	83	13	0	29	1.80	0.83	0.78	0.36	2.30	1.84	1.90	0.41	2.37	1.87	1.93	0	4	59	27	0	35
8004-2	PWD	-4	66	10	131	7	78	17	37	50	13	4	77	19	0	29	1.91	0.81	0.73	0.36	2.39	1.89	1.99	0.43	2.46	1.89	1.98	0	4	67	20	0	35
	APT	-4	66	10	131	7	78	17	37	50	13	4	77	19	0	29	1.91	0.81	0.73	0.36	2.39	1.89	1.99	0.43	2.46	1.89	1.98	0	4	67	20	0	35
	AFT	-4	66	10	131	7	78	17	37	50	13	4	77	19	0	29	1.91	0.81	0.73	0.36	2.39	1.89	1.99	0.43	2.46	1.89	1.98	0	4	67	20	0	35
8006-1	PWD	38	96	32	140	1	99	0	1	31	48	0	91	49	0	23	1.81	0.71	0.68	0.80	2.31	1.58	1.52	1.31	2.40	2.20	2.24	0	5	72	21	1	80
	APT	38	96	32	140	1	99	0	0	23	77	0	24	76	0	36	1.66	0.87	0.84	0.96	2.35	1.72	1.72	1.41	2.40	2.24	2.28	0	1	58	40	1	80
	AFT	32	84	36	147	2	98	0	30	41	29	11	59	30	0	21	1.14	0.53	0.50	0.56	2.28	1.49	1.50	1.50	2.33	2.11	2.16	2	21	72	4	0	45
8006-2	PWD	32	84	36	147	2	98	0	35	40	23	21	54	28	0	26	1.34	0.82	0.58	0.65	2.19	1.48	1.47	1.58	2.30	2.12	2.18	0	11	77	9	0	45
	APT	32	84	36	147	2	98	0	35	40	23	21	54	28	0	26	1.34	0.82	0.58	0.65	2.19	1.48	1.47	1.58	2.30	2.12	2.18	0	11	77	9	0	45
	AFT	32	84	36	147	2	98	0	35	40	23	21	54	28	0	26	1.34	0.82	0.58	0.65	2.19	1.48	1.47	1.58	2.30	2.12	2.18	0	11	77	9	0	45
8007-1	PWD	12	49	50	103	0	5	95	1	20	79	0	25	73	0	26	1.22	0.92	0.47	0.62	2.20	1.44	1.40	1.22	1.36	2.17	2.21	2	2	86	6	0	60
	APT	11	49	48	102	0	100	0	10	42	48	6	77	17	0	26	1.76	0.58	0.55	0.78	2.31	1.52	1.52	1.54	2.39	2.20	2.24	1	13	80	8	1	60
	AFT	32	37	43	112	0	23	73	3	28	89	0	28	74	0	26	1.23	0.81	0.48	0.70	2.32	1.44	1.40	0.90	2.37	2.15	2.20	18	9	71	2	0	68
8007-2	PWD	31	87	39	111	0	100	0	19	41	40	3	88	9	0	24	1.56	0.80	0.56	0.44	2.27	1.52	1.52	0.84	2.41	2.17	2.25	1	16	74	9	1	68
	APT	31	87	39	111	0	100	0	19	41	40	3	88	9	0	24	1.56	0.80	0.56	0.44	2.27	1.52	1.52	0.84	2.41	2.17	2.25	1	16	74	9	1	68
	AFT	31	87	39	111	0	100	0	19	41	40	3	88	9	0	24	1.56	0.80	0.56	0.44	2.27	1.52	1.52	0.84	2.41	2.17	2.25	1	16	74	9	1	68
8008-1	PWD	30	81	30	102	0	100	0	4	32	64	1	33	64	0	32	1.48	0.86	0.62	0.78	2.24	1.55	1.54	1.46	2.35	2.21	2.24	2	2	86	8	1	45
	APT	30	81	30	102	0	100	0	4	27	69	0	34	66	0	32	1.57	0.71	0.69	0.81	2.21	1.57	1.58	1.08	2.37	2.21	2.24	1	1	84	13	0	45
	AFT	29	56	42	105	0	100	0	3	31	66	0	27	73	0	14	1.81	0.78	0.72	0.57	2.10	1.54	1.55	1.09	2.40	2.50	2.25	2	1	73	23	1	68
8008-2	PWD	29	56	42	105	0	100	0	3	30	67	2	29	71	0	32	1.64	0.77	0.76	0.73	2.10	1.55	1.55	1.10	2.35	2.18	2.22	1	3	69	27	0	68
	APT	29	56	42	105	0	100	0	3	30	67	2	29	71	0	32	1.64	0.77	0.76	0.73	2.10	1.55	1.55	1.10	2.35	2.18	2.22	1	3	69	27	0	68
	AFT	29	56	42	105	0	100	0	3	30	67	2	29	71	0	32	1.64	0.77	0.76	0.73	2.10	1.55	1.55	1.10	2.35	2.18	2.22	1	3	69	27	0	68
8009-1	PWD	12	49	42	132	0	100	0	1	28	73	0	34	66	0	32	1.40	0.63	0.62	0.85	2.41	1.53	1.52	0.83	2.31	2.30	2.36	5	4	77	14	0	60
	APT	12	49	42	132	0	100	0	0	40	60	0	45	55	0	28	1.42	0.70	0.64	0.92	2.28	1.58	1.55	0.63	2.31	2.32	2.36	1	5	73	20	0	60
	AFT	23	58	35	136	2	98	0	40	60	29	1	40	60	0	29	1.55	0.69	0.64	0.73	2.37	1.53	1.53	0.62	2.45	2.23	2.30	4	4	74	17	0	60
8009-2	PWD	23	58	35	136	2	98	0	4	47	49	0	56	44	0	26	1.47	0.69	0.64	0.44	2.42	1.61	1.60	1.81	2.50	2.31	2.34	1	4	77	16	0	60
	APT	23	58	35	136	2	98	0	4	47	49	0	56	44	0	26	1.47	0.69	0.64	0.44	2.42	1.61	1.60	1.81	2.50	2.31	2.34	1	4	77	16	0	60
	AFT	23	58	35	136	2	98	0	4	47	49	0	56	44	0	26	1.47	0.69	0.64	0.44	2.42	1.61	1.60	1.81	2.50	2.31	2.34	1	4	77	16	0	60
8010-1	PWD	18	47	45	83	0	21	79	0	13	87	0	9	91	0	28	1.14	0.92	0.47	0.43	2.32	1.38	1.32	1.11	2.42	2.16	2.20	18	3	75	4	0	48
	APT	18	47	45	83	0	21	79	0	13	87	0	9	91	0	28	1.14	0.92	0.47	0.43	2.32	1.38	1.32	1.11	2.42	2.16	2.20	18	3	81	6	0	48
	AFT	18	47	45	83	0	21	79	0	13	87	0	9	91	0	28	1.14	0.92	0.47	0.43	2.32	1.38	1.32	1.11	2.42	2.16	2.20	18	3	81	6	0	48
8010-2	PWD	18	47	45	83	0	21	79	0	13	87	0	9	91	0	28	1.14	0.92	0.47	0.43	2.32	1.38	1.32	1.11	2.42	2.16	2.20	18	3	81	6	0	48
	APT	18	47	45	83	0	21	79	0	13	87	0	9	91	0	28	1.14	0.92	0.47	0.43	2.32	1.38	1.32	1.11	2.42	2.16	2.20	18	3	81	6	0	48
	AFT	18	47	45	83	0	21	79	0	13	87	0	9	91	0	28	1.14	0.92	0.47	0.43	2.32	1.38	1.32	1.11	2.42	2.16	2.20	18	3	81	6	0	48

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